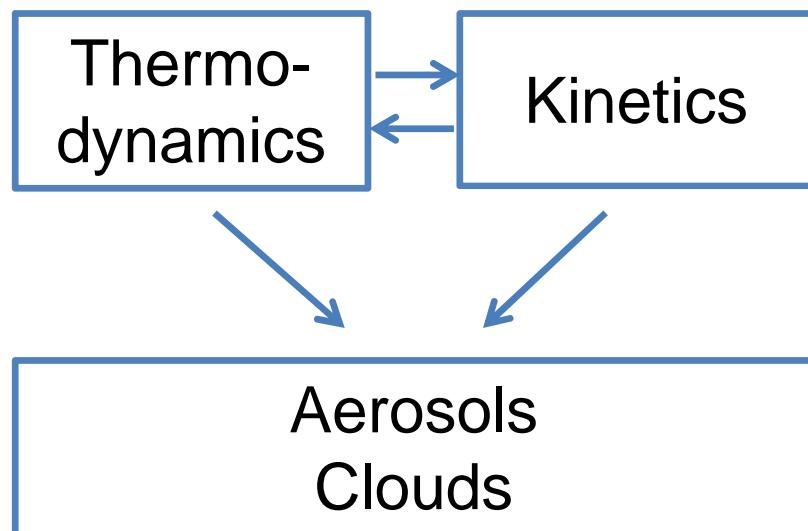


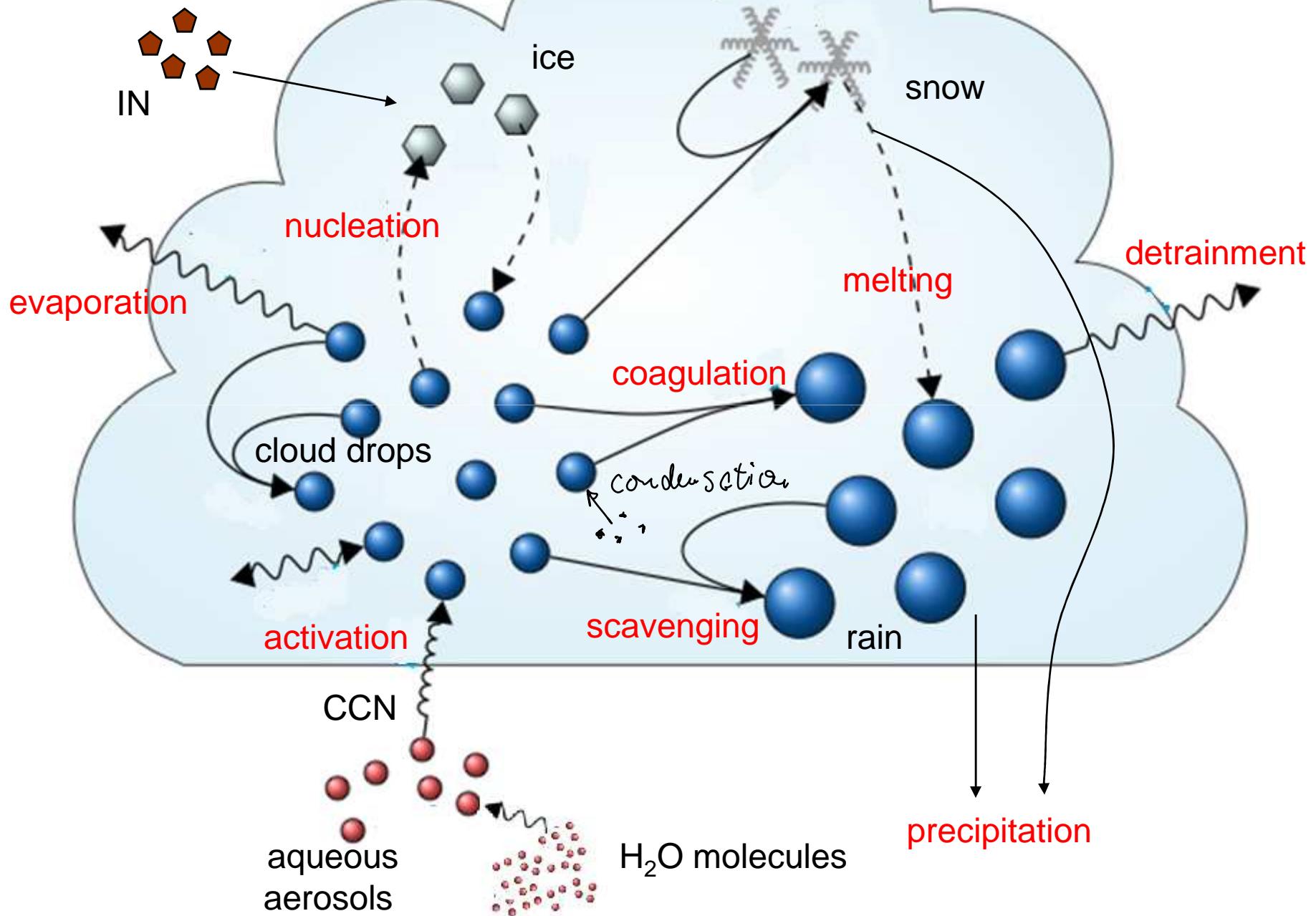
## Microphysics

Tom Peter, ETH Zurich

- Observations
- Modelling



# Aerosol and Cloud Processes

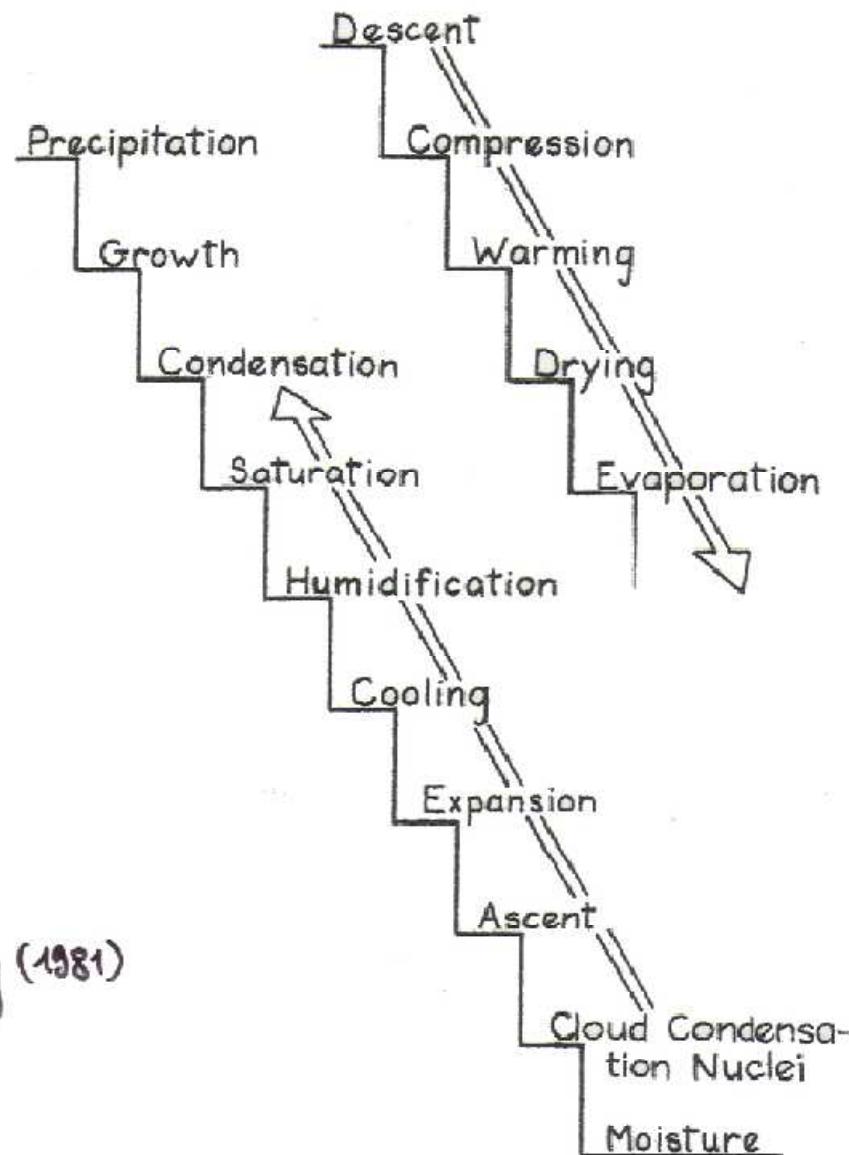


# Precipitation staircase

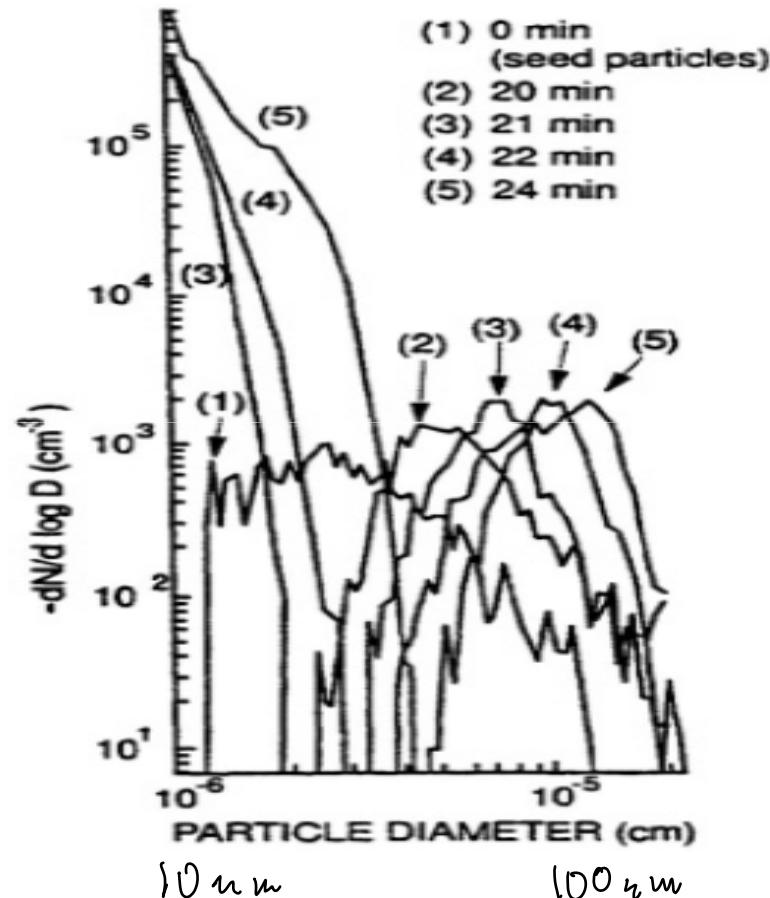
Prerequisites for cloud formation:

- water
- low T
- supersaturation
- Cloud Condensation Nuclei (CCN) or Ice Nuclei (IN)

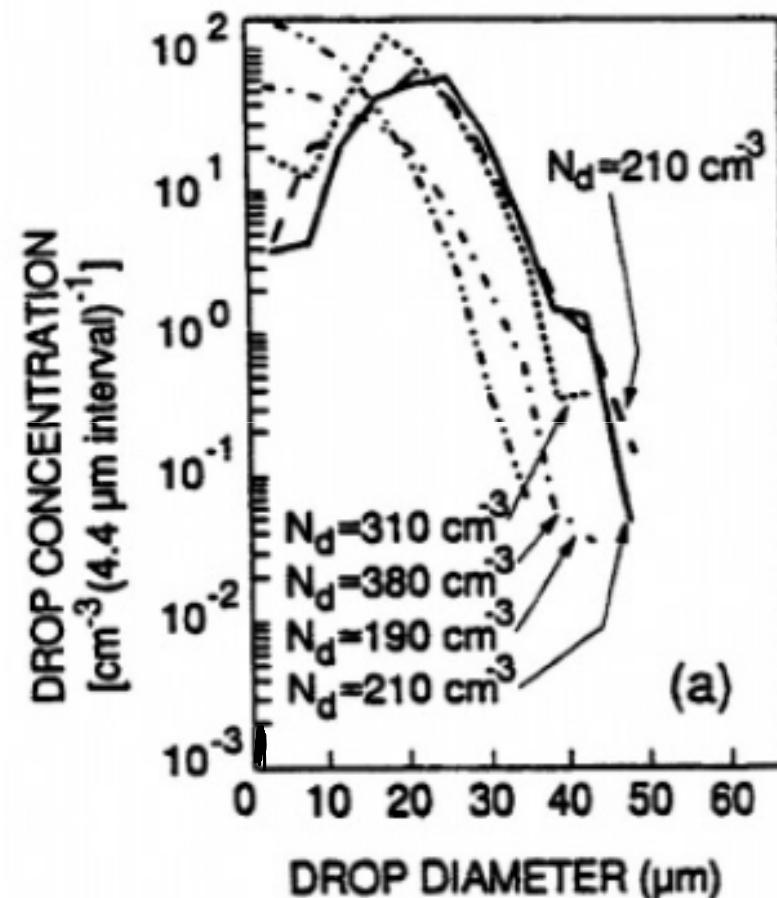
Schoefer & Day (1981)



# Particle size distributions: The result of the interplay of thermodynamics and kinetics in response to outer forcings ( $T$ , $h\nu$ , $g$ )



Size distribution of aerosol particles from photooxidation of a methylcyclohexane-propane- $\text{NO}_x$  mixture (Seinfeld, 1994)

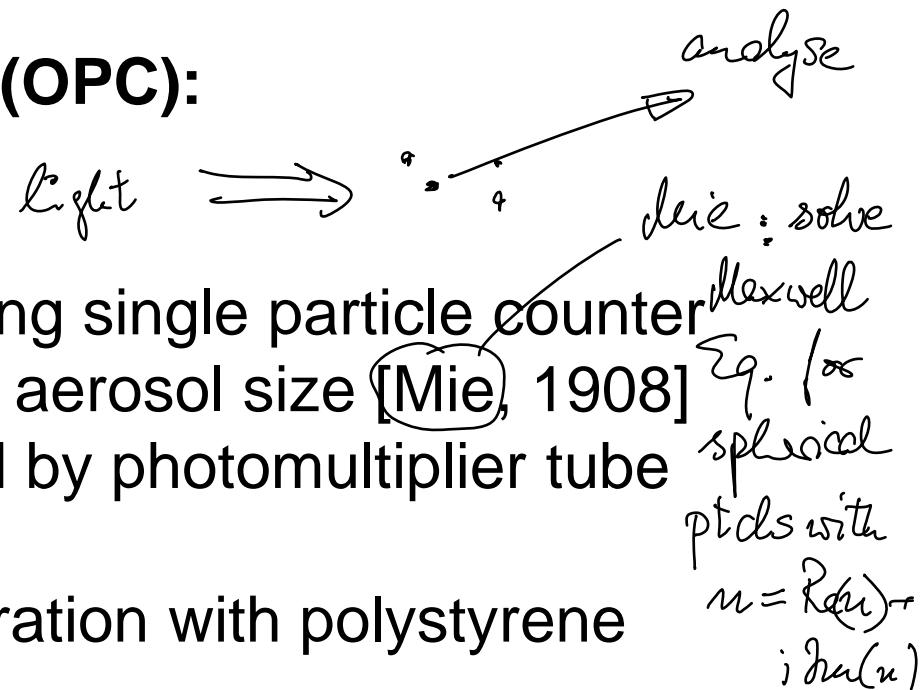


Size distribution of cloud particles near the top of young continental cumuli (Hobbs et al., 1980)

Example of instrument:

## Optical particle counter (OPC):

- “White light counter”
- Aerosol forward scattering single particle counter
- Mie theory to determine aerosol size [Mie, 1908]
- Scattered light amplified by photomultiplier tube
- Pulse height detection
- Prior to each flight calibration with polystyrene latex spheres



All OPC channels measure particles larger than a certain size

# The differential particle size distribution

$$\frac{dn}{d \log D}(\vec{x}, \vec{D}, t) = \frac{dn}{d \log r}(\vec{x}, r, t) = r \underbrace{\frac{dn}{dr}(\vec{x}, r, t)}_{\substack{\# \text{ ptcls} \\ \text{cm}^{-3} \mu\text{m}}} \equiv r n_r(\vec{x}, r, t)$$

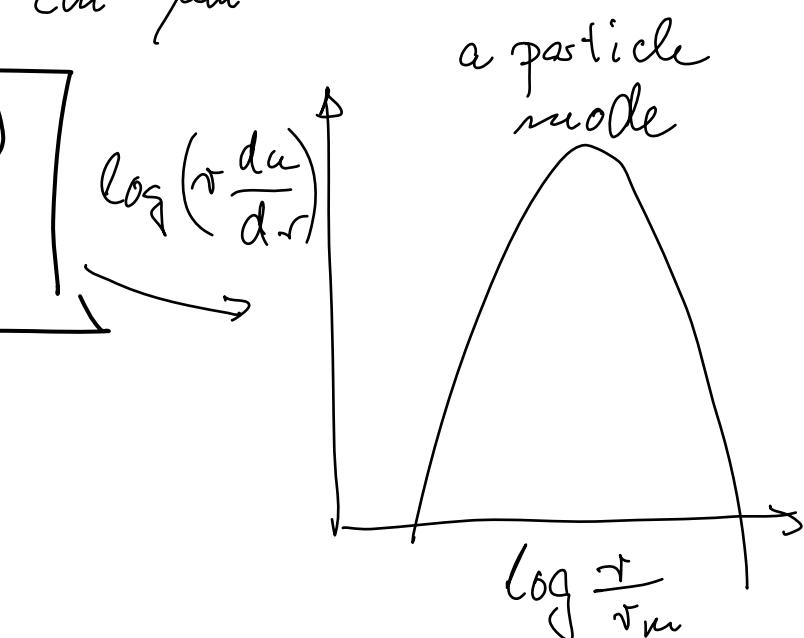
diameter                          radius

Lognormal distribution :

$$\frac{dn}{dr} = \frac{n_t}{\sqrt{2\pi} + \ln \sigma} e^{-\frac{\ln^2(r/r_m)}{2\ln^2 \sigma}}$$

$r_m$  = mode radius

$\sigma$  = width



Lognormal distribution :

$$\frac{dn}{dr} = \frac{n_t}{\sqrt{2\pi} + \ln \sigma} e^{-\frac{\ln^2(r/r_m)}{2\ln^2 \sigma}}$$

$r_m$  = mode radius

$\alpha$ -th moment :

$$\langle r^\alpha \rangle = \frac{1}{n_t} \int_0^\infty dr \frac{dn}{dr} r^\alpha = r_m^\alpha \exp\left(\frac{\alpha^2}{2} \ln^2 \sigma\right)$$

Thus:

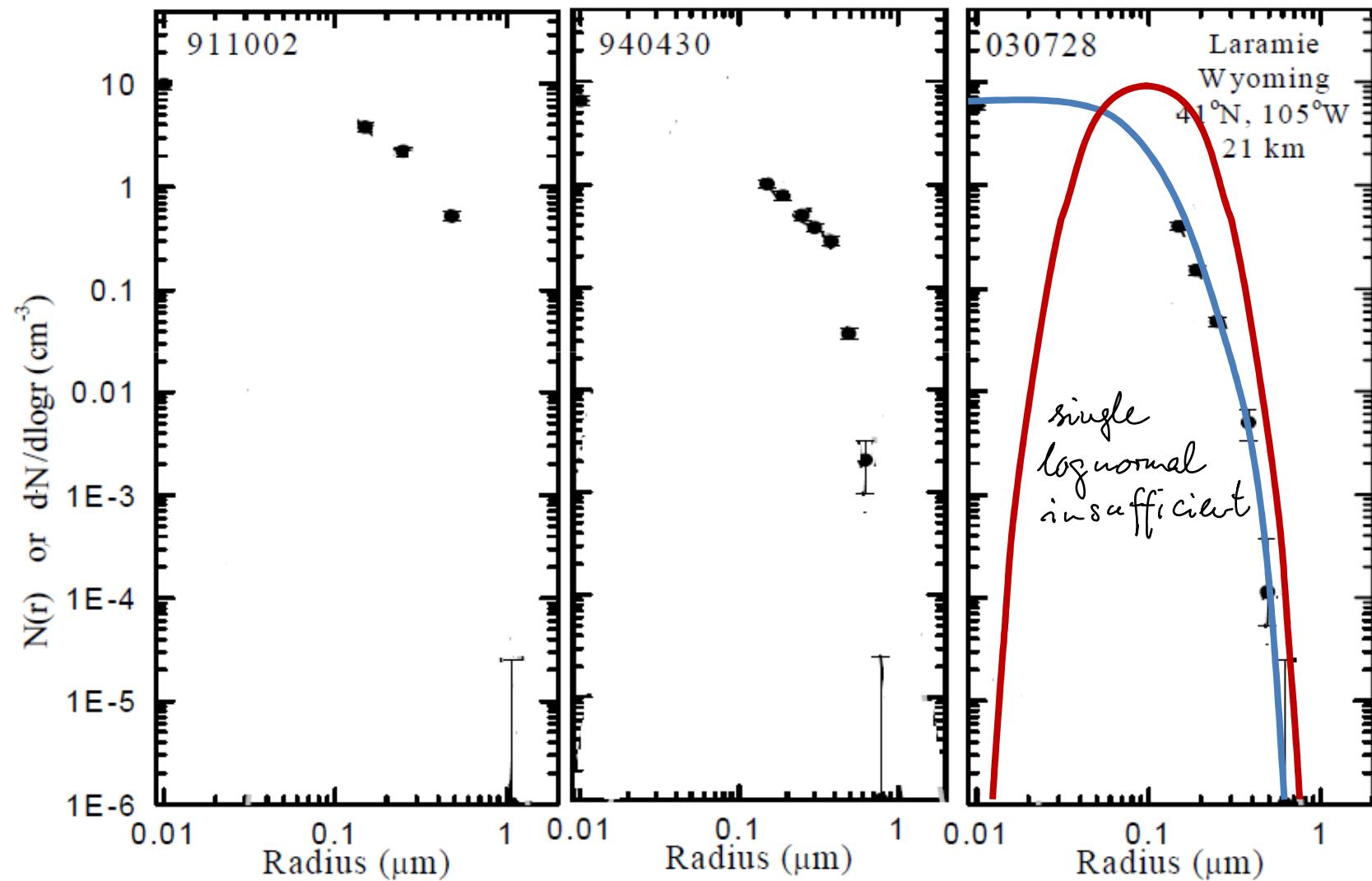
$$\int_0^\infty dr \frac{dn}{dr} = n_t = \text{total number density}$$

$$\langle r \rangle = r_m \exp\left(\frac{1}{2} \ln^2 \sigma\right) = \text{mean radius}$$

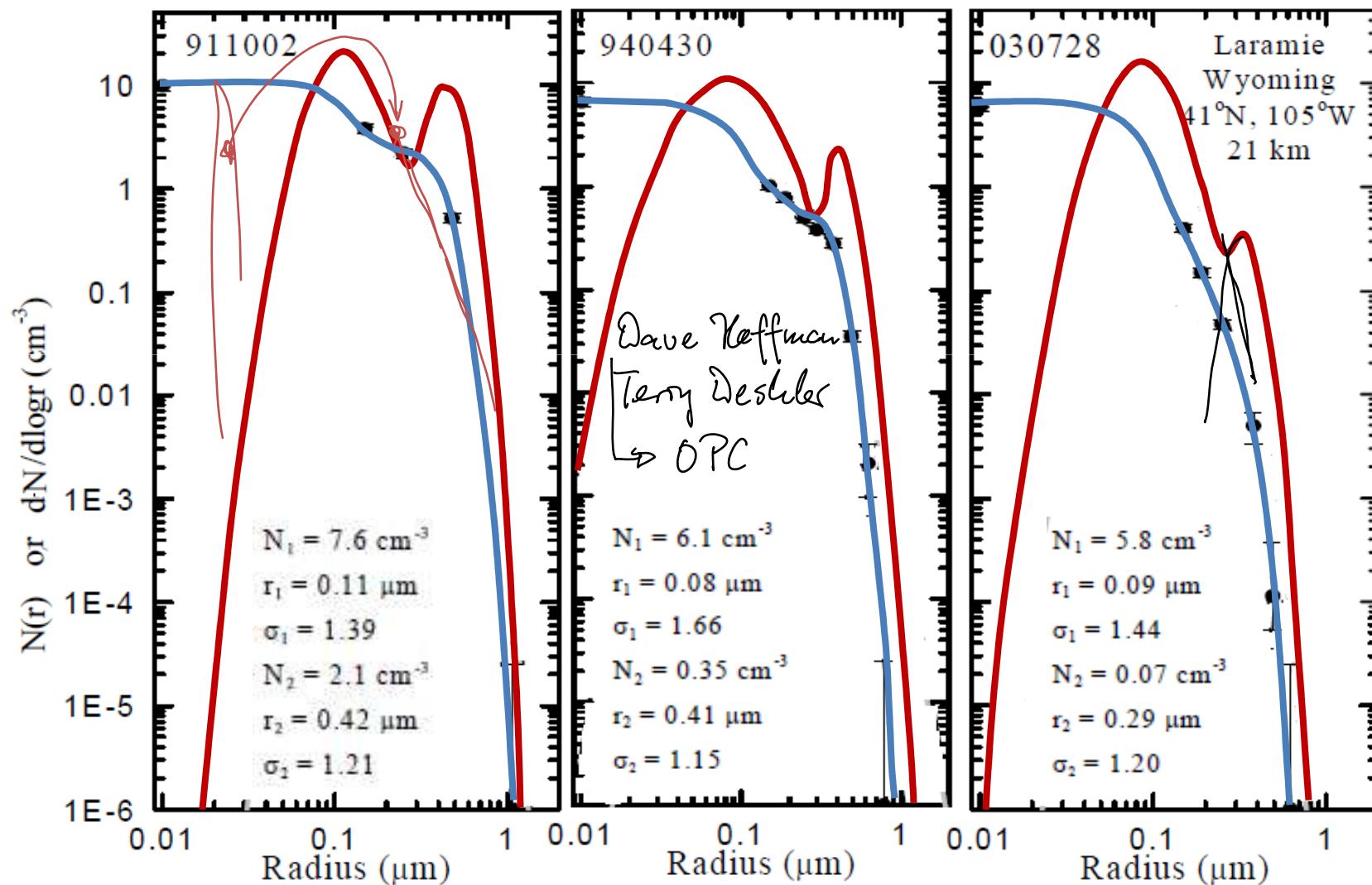
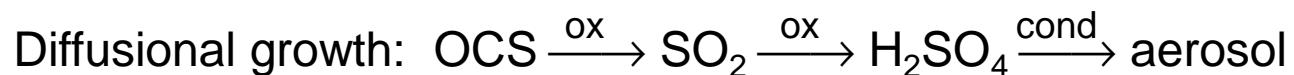
# Size distribution of stratospheric aerosols

Diffusional growth:  $\text{OCS} \xrightarrow{\text{ox}} \text{SO}_2 \xrightarrow{\text{ox}} \text{H}_2\text{SO}_4 \xrightarrow{\text{cond}} \text{aerosol}$

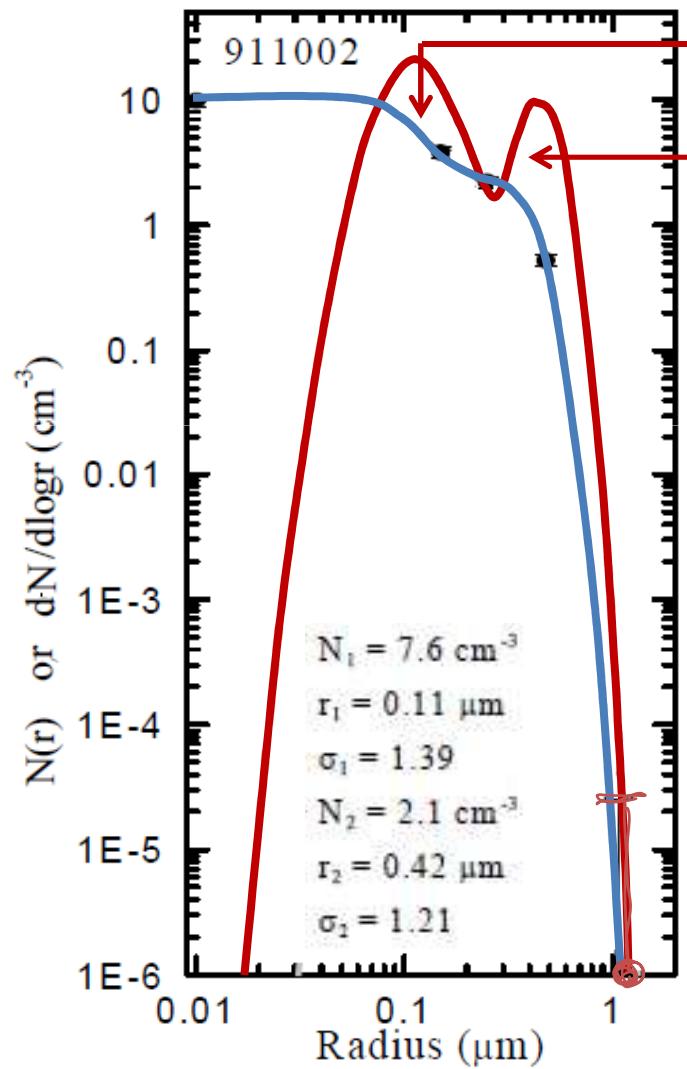
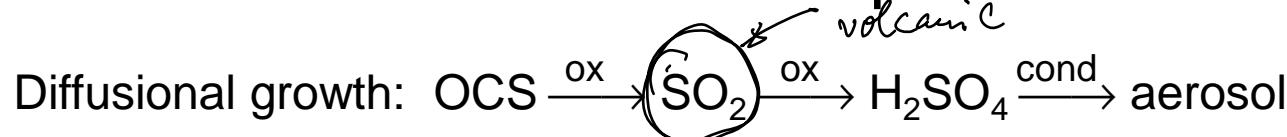
OPC measured  
in strat.



# Size distribution of stratospheric aerosols



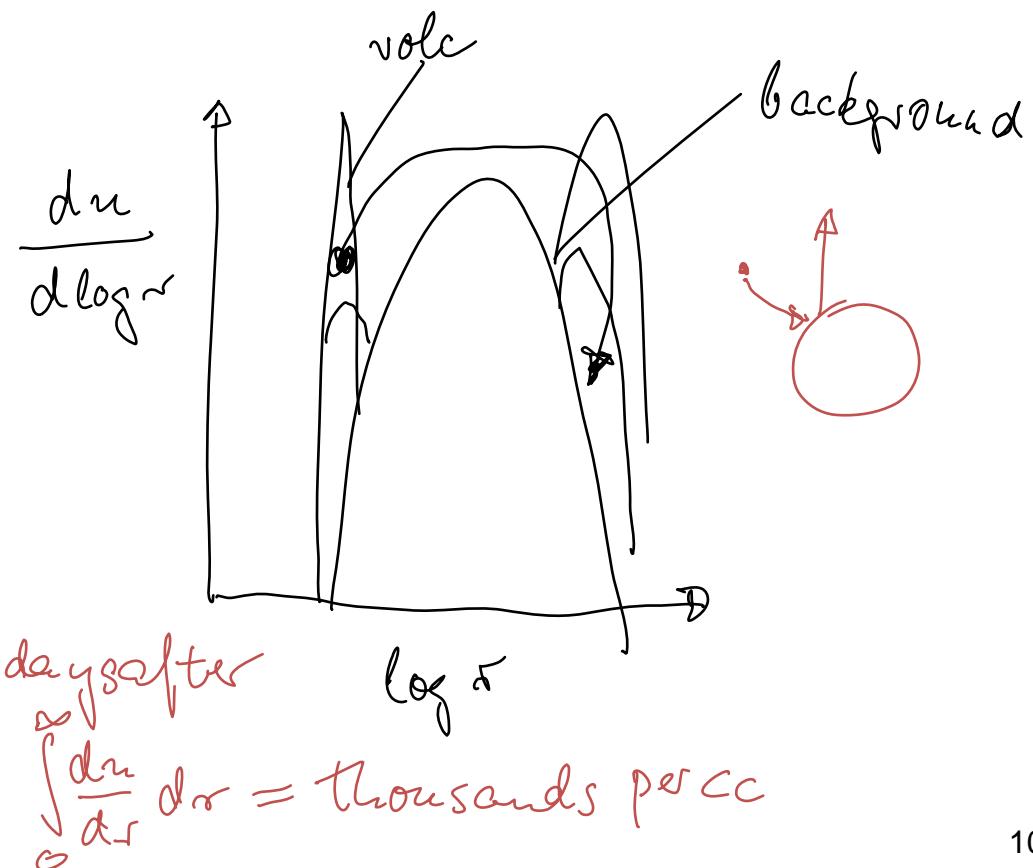
# Size distribution of stratospheric aerosols



Background mode

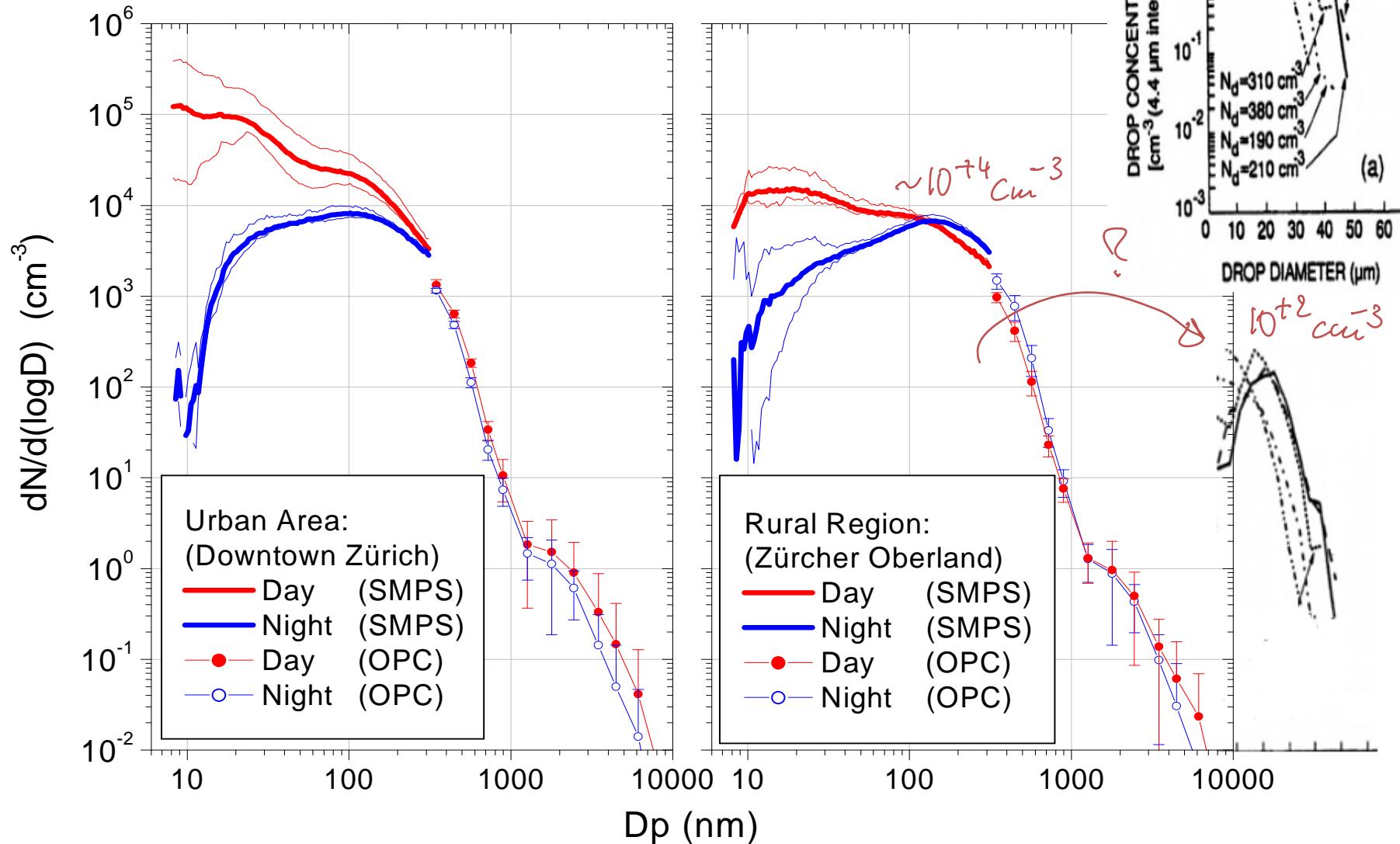
Volcanic mode:

Pinatubo, 15°N, June 1991: coagulation of freshly nucleated with largest background particles

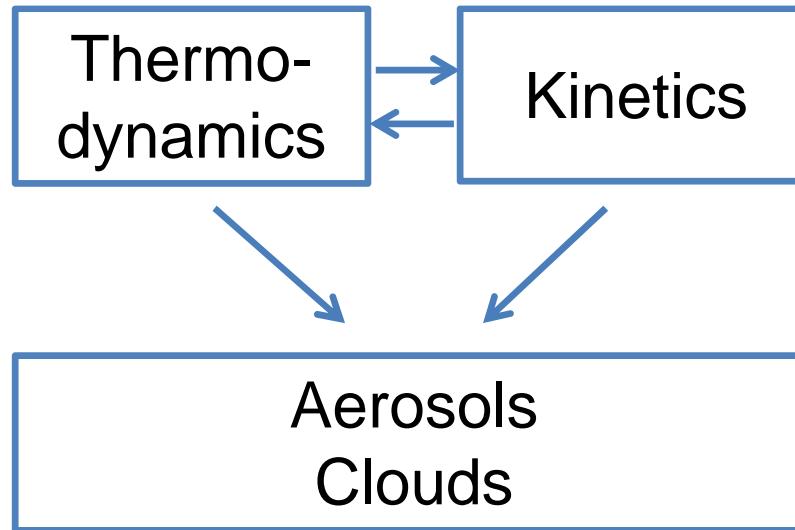


# Size distribution in and around Zürich:

smallest particles are 10 times more abundant in the city compared to the country side and 100 times more abundant during the day than in the night



## Formation of water clouds



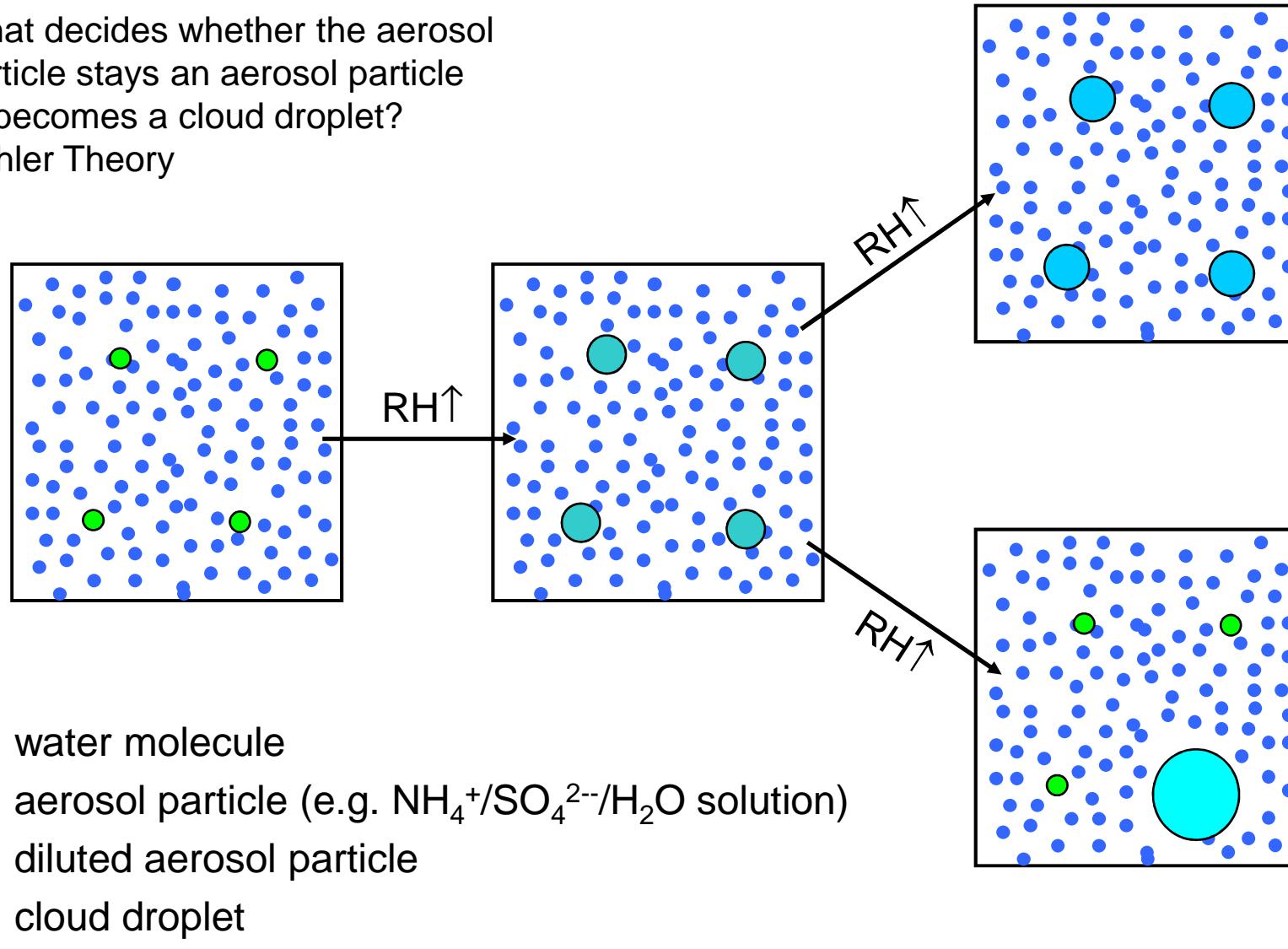
*How far do we get with  
thermodynamics in explaining  
cloud formation?*

# Cloud droplet formation

A fierce competition without which precipitation would be massively impeded!

What decides whether the aerosol particle stays an aerosol particle or becomes a cloud droplet?

Köhler Theory



# 3 big names: Raoult, Kelvin, Köhler

- Raoult's law (1870)

- small droplets have higher solute concentrations (salts, acids) and this reduces the H<sub>2</sub>O vapor pressure
  - advantage for small droplets

- Kelvin effect (1879)

- small droplets have a higher H<sub>2</sub>O vapor pressure (curvature effect)
  - disadvantage for small droplets

- Köhler equation (1921)

- balance between Kelvin and Raoult terms
  - quantitative understanding

## Clapeyron's equation

(applies to any phase transition of a pure substance)

$$\Delta V_m \, dp = \Delta S_m \, dT$$

$\Delta S_m$  = change of molar entropy during phase transition

$\Delta V_m$  = change of molar volume during phase transition

## Clausius-Clapeyron equation

(valid for solid-gas and liquid-gas phase transitions)

$$\text{Gibbs free energy: } \Delta G_{vap} = \mu dn = \Delta H_{vap} - T\Delta S_{vap} = 0$$

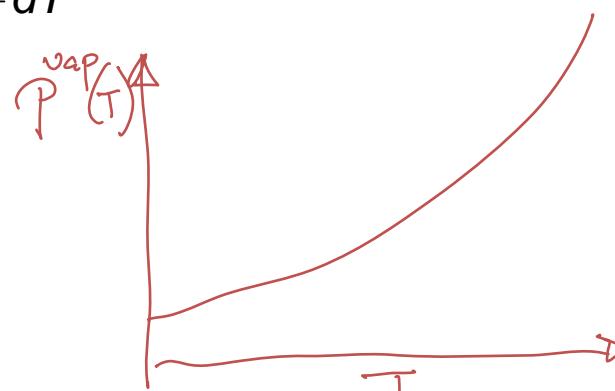
$\Delta H_{vap}$ : molar enthalpy change during vaporization

→  $\Delta S_{vap} = \Delta H_{vap}/T$  at equilibrium of two phases

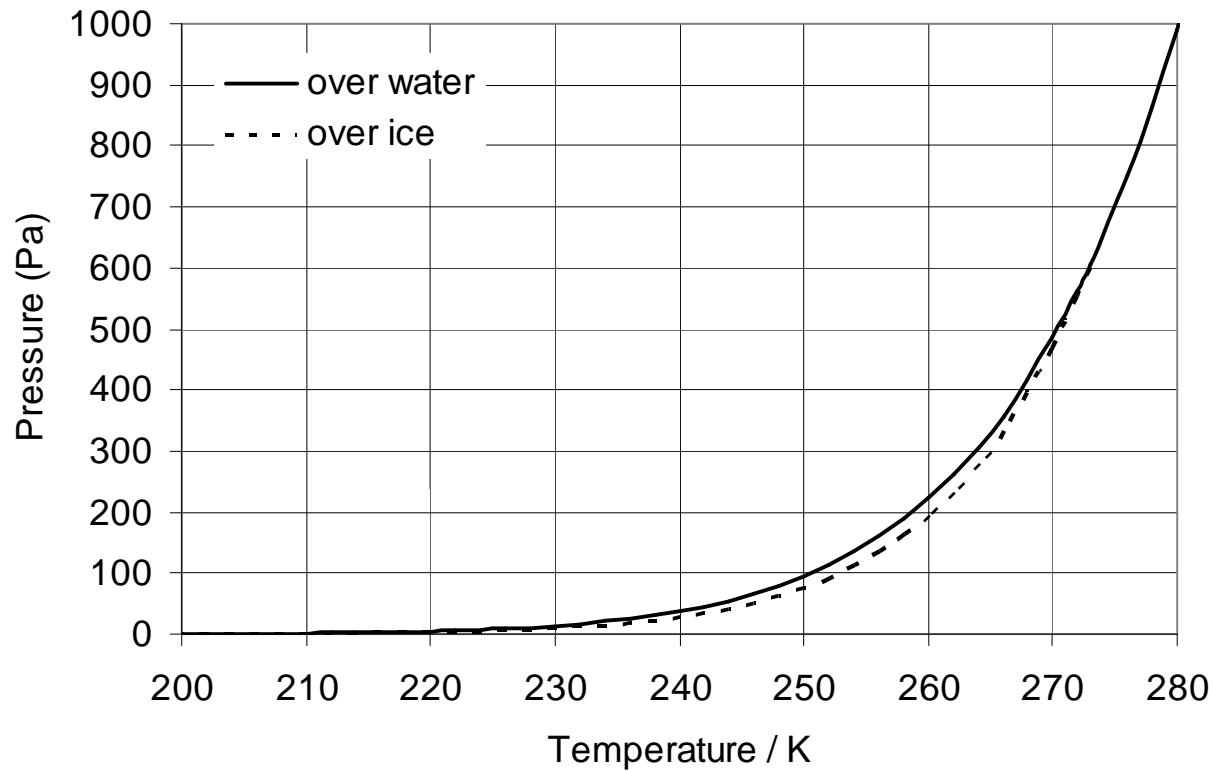
$$\rightarrow \frac{dp}{dT} = \frac{\Delta H_{vap}}{\Delta V_{vap} T} = \frac{\Delta H_{vap} p}{RT^2} \quad \rightarrow \quad \frac{dp}{p} = d \ln p = \frac{\Delta H_{vap}}{RT^2} dT$$

$$\rightarrow \boxed{\ln \frac{p(T)}{p_0} = -\frac{\Delta H_{vap}}{R} \left( \frac{1}{T_1} - \frac{1}{T_0} \right)}$$

assumes  $\Delta H_{vap}$  to be  $T$ -independent



## Vapor pressure of liquid water and ice



Murphy & Koop 2005, Q. J. R. Meteorol. Soc. 131, 1539–1565:

$p$  over water in Pa:

$$\begin{aligned}\ln(p_{\text{water}}) \approx & 54.842763 - 6763.22/T - 4.210 \ln(T) + 0.000367 T + \tanh\{0.0415(T - 218.8)\} \\ & \times (53.878 - 1331.22/T - 9.44523 \ln(T) + 0.014025 T)\end{aligned}$$

$p$  over ice in Pa:

$$\ln(p_{\text{ice}}) = 9.550426 - 5723.265/T + 3.53068 \ln(T) - 0.00728332T; \quad T > 110 \text{ K}$$

# Vapor pressure of liquid mixtures: Raoult's law

Mixture of two liquids A und B:

$$p_A = x_A p_A^*, \quad p_B = x_B p_B^*$$

$$P = p_A + p_B$$

$P$  = total pressure

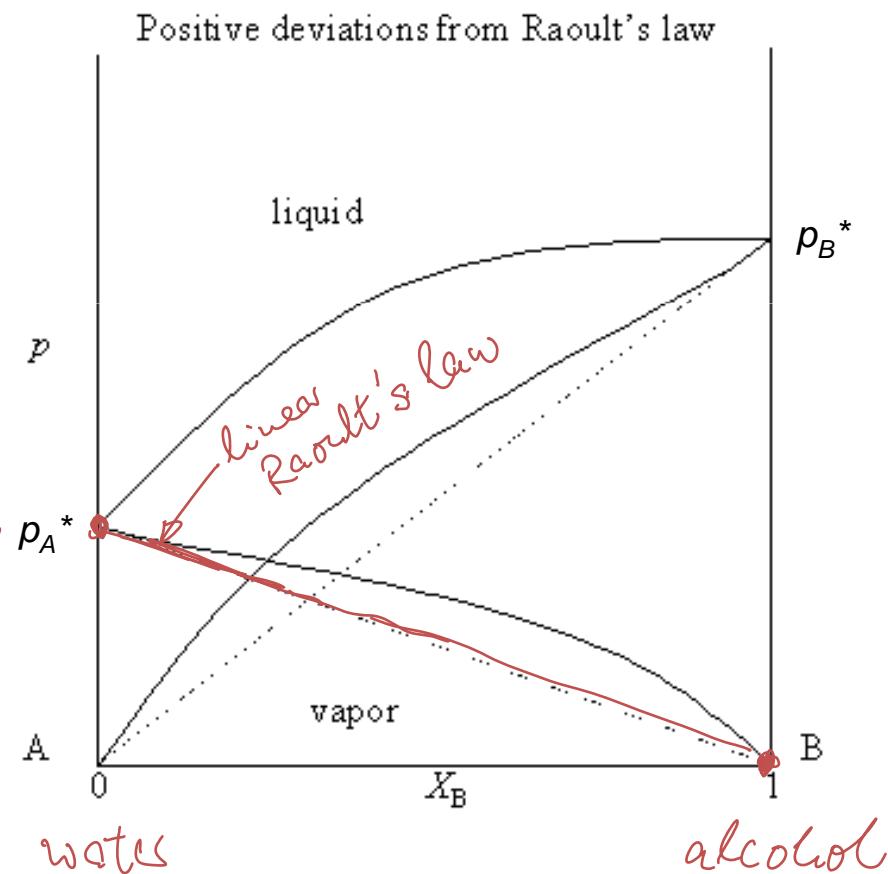
$p$  = partial pressure

$p^*$  = pressure of pure substance

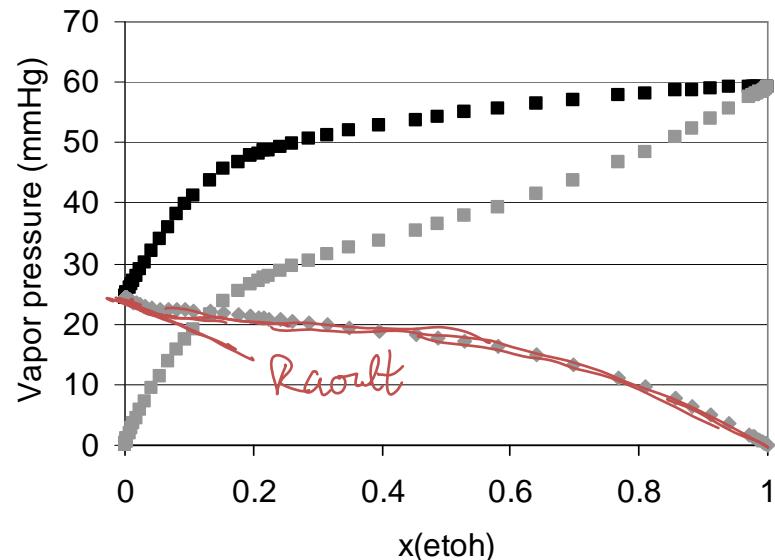
$$x_i = \text{mole fraction: } x_i = \frac{n_i}{\sum n_i}$$

$n$  = mole number

Pure H<sub>2</sub>O vapor

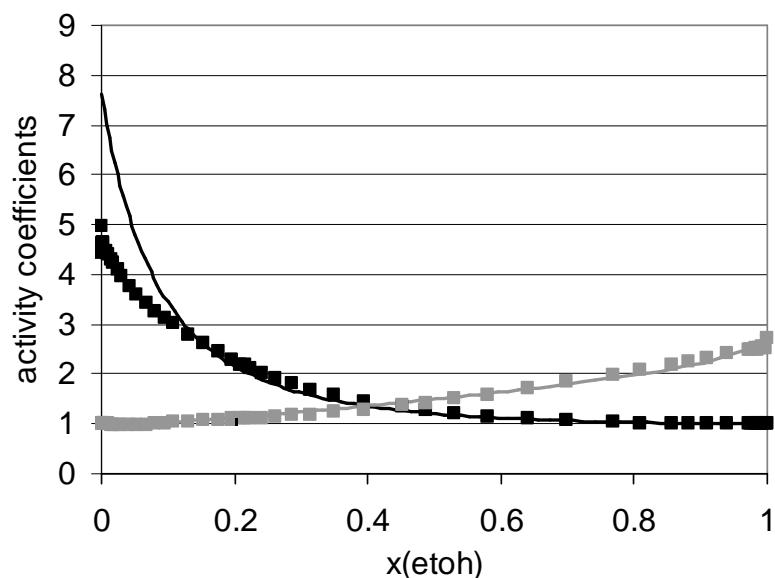


## Water / ethanol – mixtures at 25.13°C



Measurement of the vapor-liquid-equilibrium (VLE) of ethanol (etOH) / water mixtures

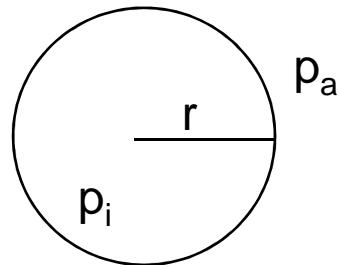
- total vapor pressure  $P$
- partial vapor pressure of etOH =  $\text{C}_2\text{H}_5\text{OH}$
- ◆ partial vapor pressure of  $\text{H}_2\text{O}$



Activity coefficients  $\gamma$  of ethanol / water mixtures

- $\gamma(\text{etOH})$  from UNIFAC model calculation
- $\gamma(\text{H}_2\text{O})$  from UNIFAC model calculation
- $\gamma(\text{etOH})$  from VLE data
- $\gamma(\text{H}_2\text{O})$  from VLE data

## Kelvin effect



Work required to increase the surface area  $A$  of the liquid-vapor interface:

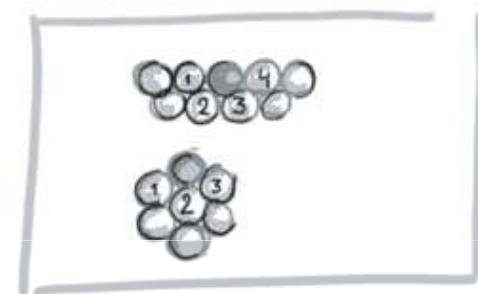
$$dW = \sigma dA$$

$\sigma$  = surface tension

$$A = 4\pi r^2 = \text{surface area}$$

$$dW = \sigma dA$$

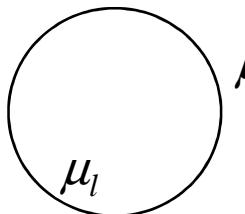
$$4\pi r^2 (p_i - p_a) = A dp = \sigma d(4\pi r^2) = 8\pi r \sigma dr$$



$$\rightarrow p_i = p_a + 2 \sigma / r \quad \text{Laplace equation (valid for bubble or droplet)}$$

*important  
for  $r < 50 \mu m$   
 $\hookrightarrow 5-10\%$  effect*

## What is the influence of the higher pressure inside a curved surface on the vapor pressure of a droplet?



In equilibrium:  $\mu_g = \mu_l$  and  $d\mu_g = d\mu_l$

Chemical potential depends on pressure:  $(\partial\mu/\partial p)_T = V_m$ ,

$V_m$ : molar volume

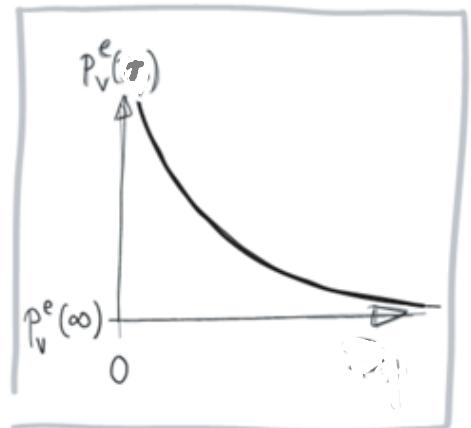
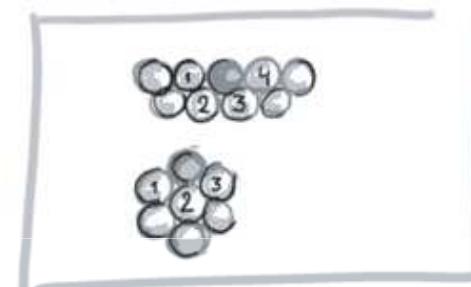
$$\rightarrow V_{m,l} dp_l = V_{m,g} dp_g = \frac{RT}{p_g} dp_g$$

$$\Rightarrow \int_{p(\infty)}^p \frac{1}{p_g} dp_g = \frac{1}{RT} \int_{p(\infty)}^{p^* + \Delta p} V_{m,l} dp_l \approx \frac{V_{m,l}}{RT} \Delta p$$

$$\Rightarrow \ln\left(\frac{p(r)}{p(\infty)}\right) = \frac{V_{m,l} \Delta p}{RT}$$

For curved surfaces:  $\Delta p = 2\sigma / r$

$$p(r) = p(\infty) \times e^{2\sigma V_{m,l} / r RT} \quad \text{Kelvin Equation}$$

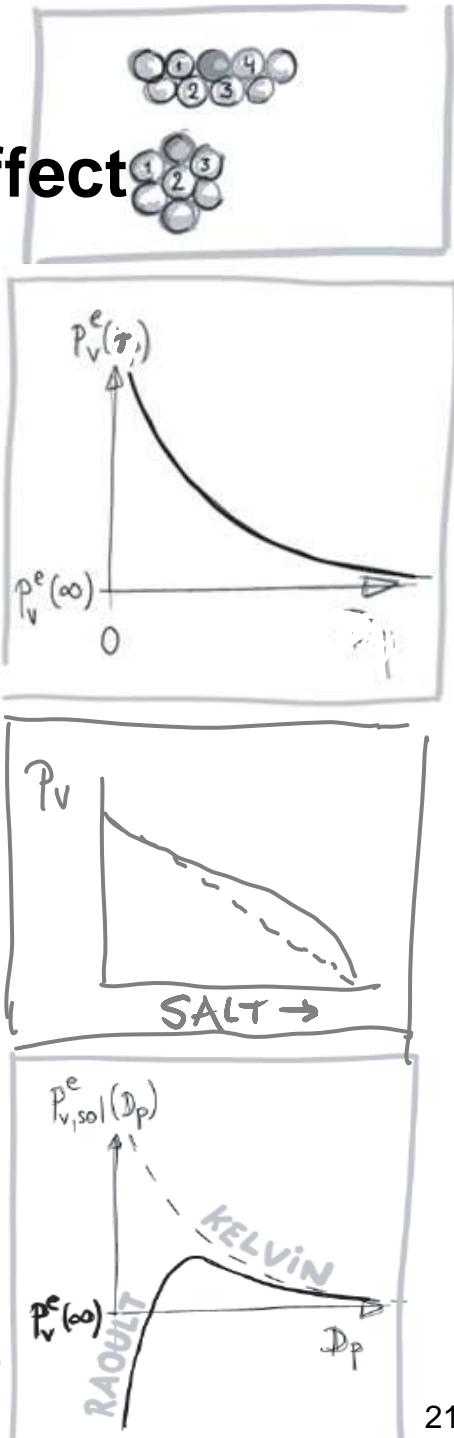


$p(\infty)$  = vapor pressure over flat surface,  $r$  = ptcl radius,  $R$  = gas constant,  
 $V_{m,l}$  = liquid molar volume, e.g. of H<sub>2</sub>O,  $\sigma$  = surface tension

# Köhler theory = Raoult's law + Kelvin Effect

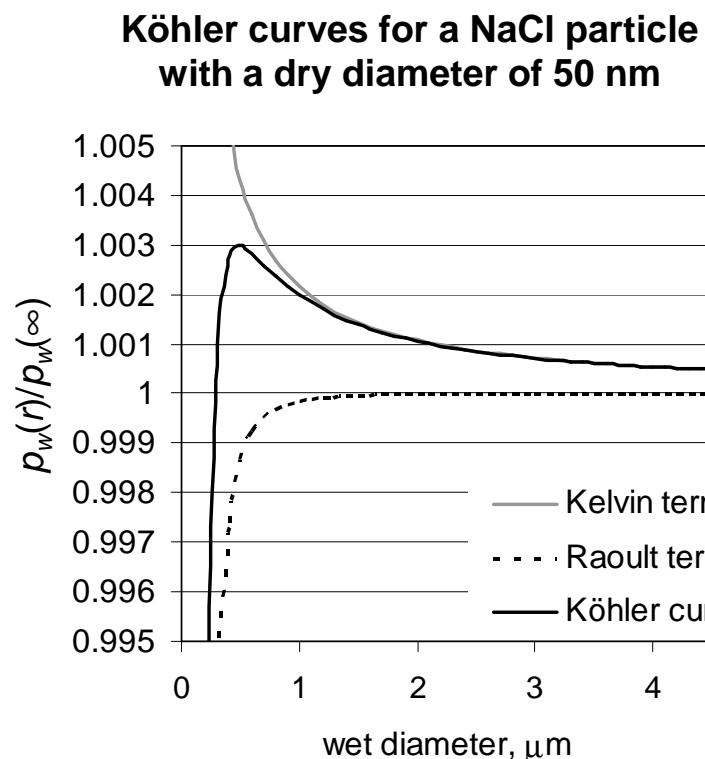
$$\begin{aligned}
 p_w(r) &= p(\infty) \times e^{2\sigma V_{m,w}/rRT} \\
 &= x_w p_w(\infty) \times e^{2\sigma V_{m,w}/rRT} \\
 &= \frac{n_w}{n_w + n_s} p_w(\infty) \times e^{2\sigma V_{m,l}/rRT} \\
 &= \frac{1}{1 + n_s V_{m,w} / (4\pi r^3 / 3 - n_s V_s)} p_w(\infty) \times e^{2\sigma V_{m,l}/rRT} \\
 &\approx \frac{1}{1 + 3n_s V_{m,w} / (4\pi r^3)} p_w(\infty) \times e^{2\sigma V_{m,w}/rRT} \\
 &\approx p_w(\infty) \times \exp\left(\frac{2\sigma V_{m,w}}{rRT} - \frac{3n_s V_{m,w}}{4\pi r^3}\right)
 \end{aligned}$$

The last two steps assume the solution to be dilute, and make a Taylor expansion;  
 $p_w(\infty)$  = H<sub>2</sub>O vapor pressure over pure liquid bulk water,  $\sigma$  = surface tension of solution,  
 $r$  = particle radius,  $V_{m,w}$  = liquid molar volume of H<sub>2</sub>O,  $n_s$  = molar density of solute

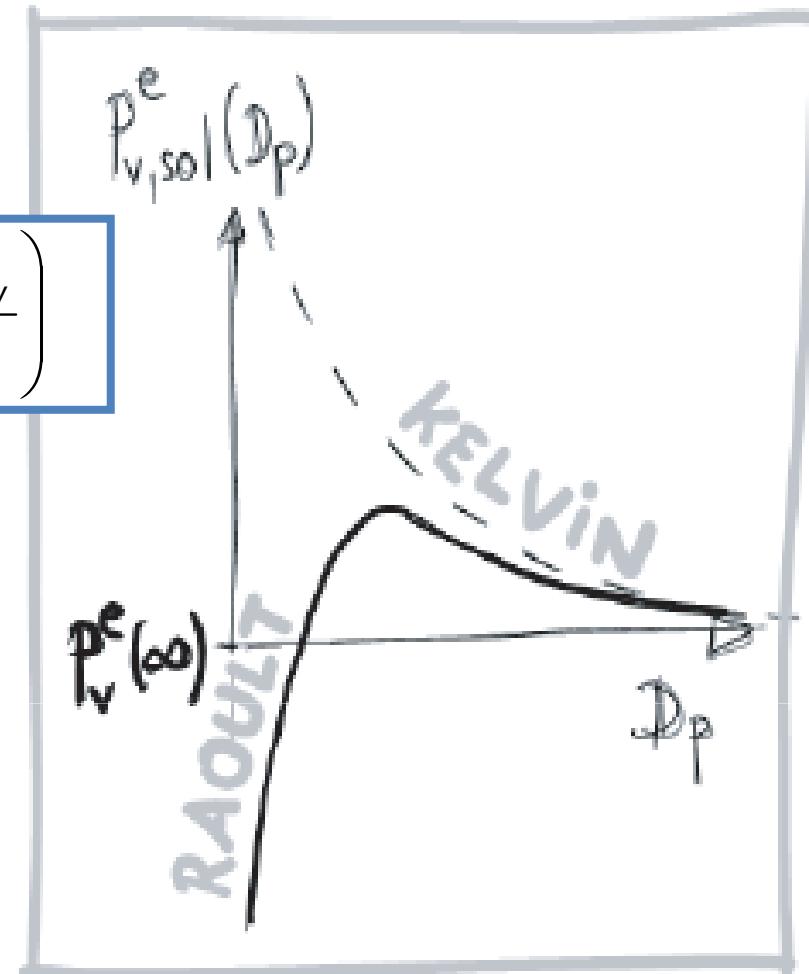


# Köhler theory

$$p_w(D_p) \approx p_w(\infty) \times \exp \left( \frac{4\sigma V_{m,w}}{D_p RT} - \frac{6n_s V_{m,w}}{\pi D_p^3} \right)$$

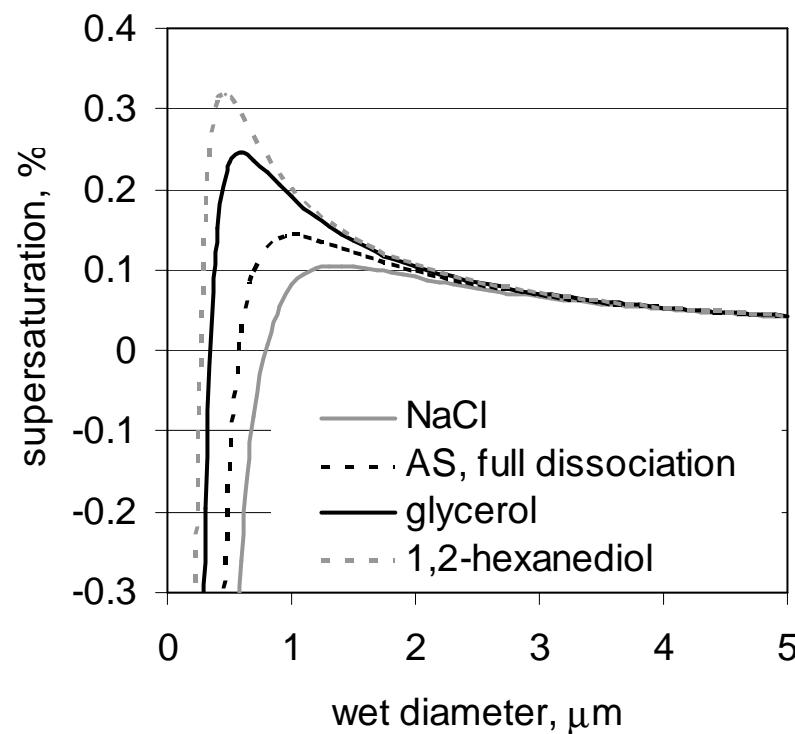


$p_w(\infty)$  =  $\text{H}_2\text{O}$  vapor pressure over pure liquid bulk water,  $\sigma$  = surface tension of solution,  
 $D_p$  = particle radius,  $V_{m,w}$  = liquid molar volume of  $\text{H}_2\text{O}$ ,  $n_s$  = molar density of solute

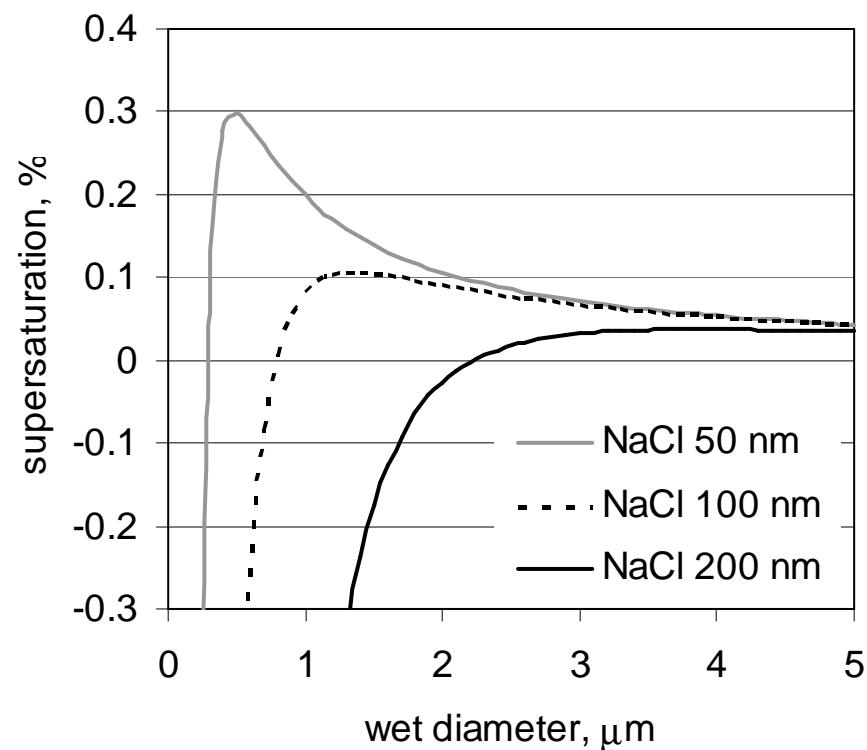


$$S_w = \frac{p_w(D_p)}{p_w(\infty)} \approx \exp\left( \frac{4\sigma V_{m,w}}{D_p RT} - \frac{6n_s V_{m,w}}{\pi D_p^3} \right)$$

**Köhler curves for particles (with dry diameters of 100 nm) of different compositions**



**Köhler curves for NaCl particles of different dry diameters**



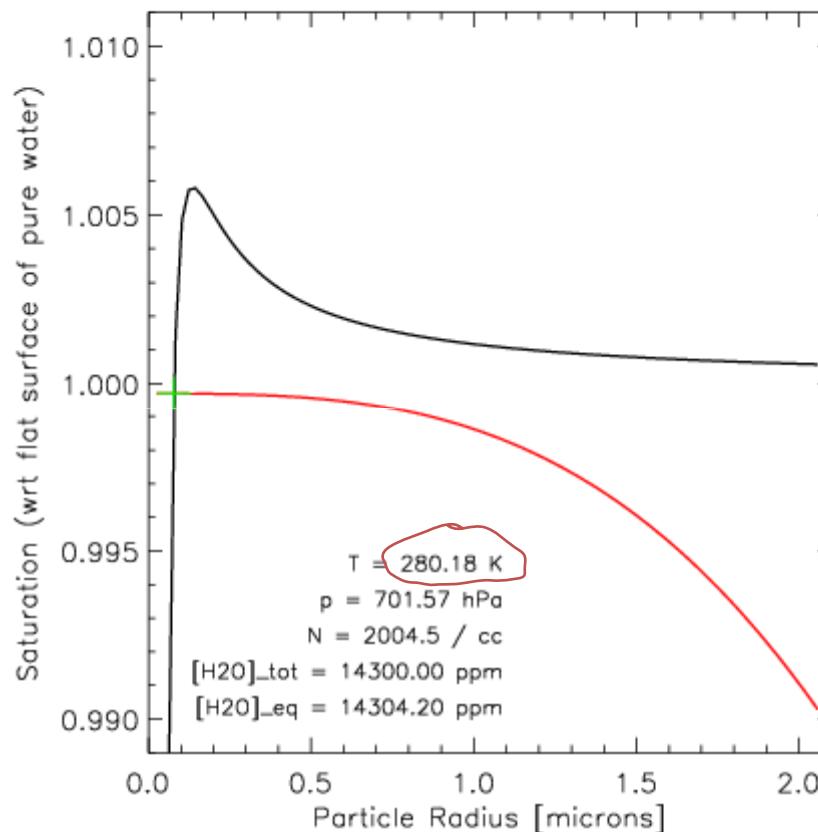
**The Köhler curve describes the equilibrium vapor pressure of a droplet with a specified dry diameter as it takes up or loses water.**

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

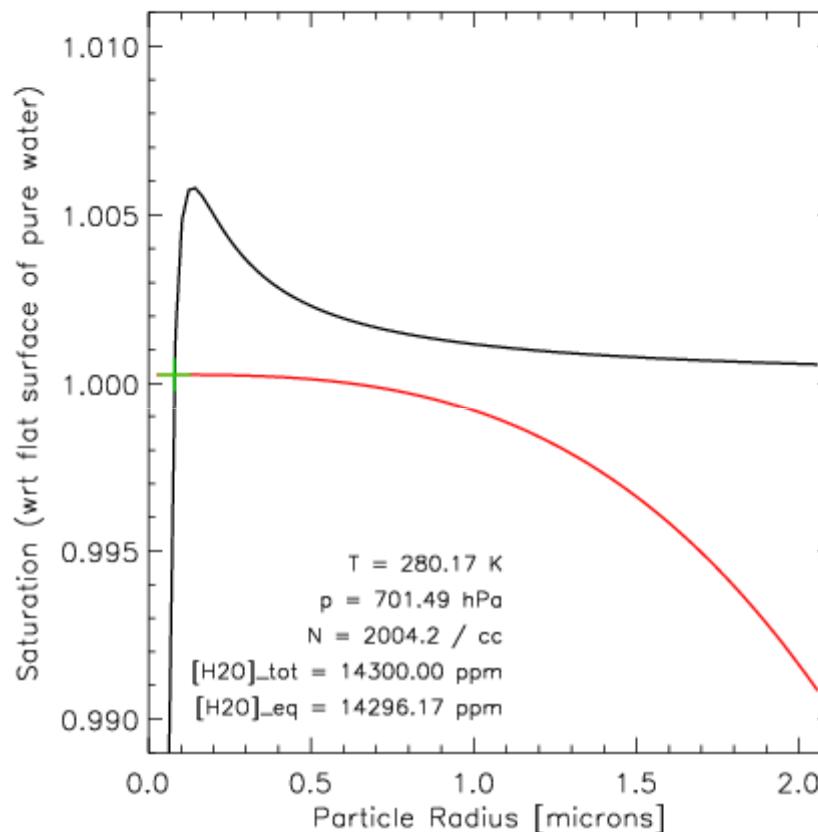
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

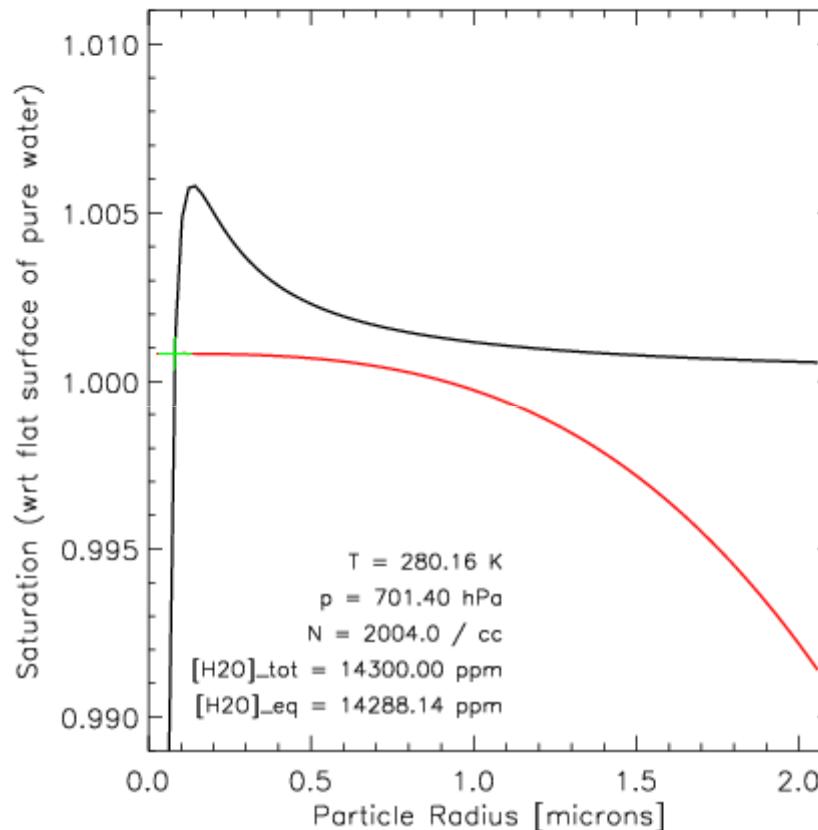
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

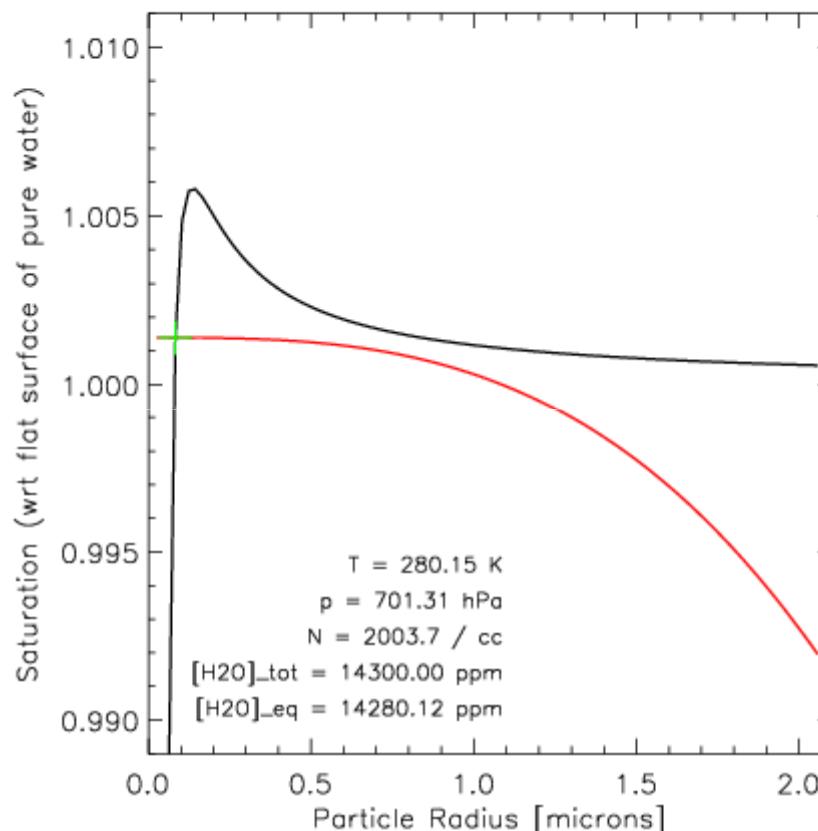
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

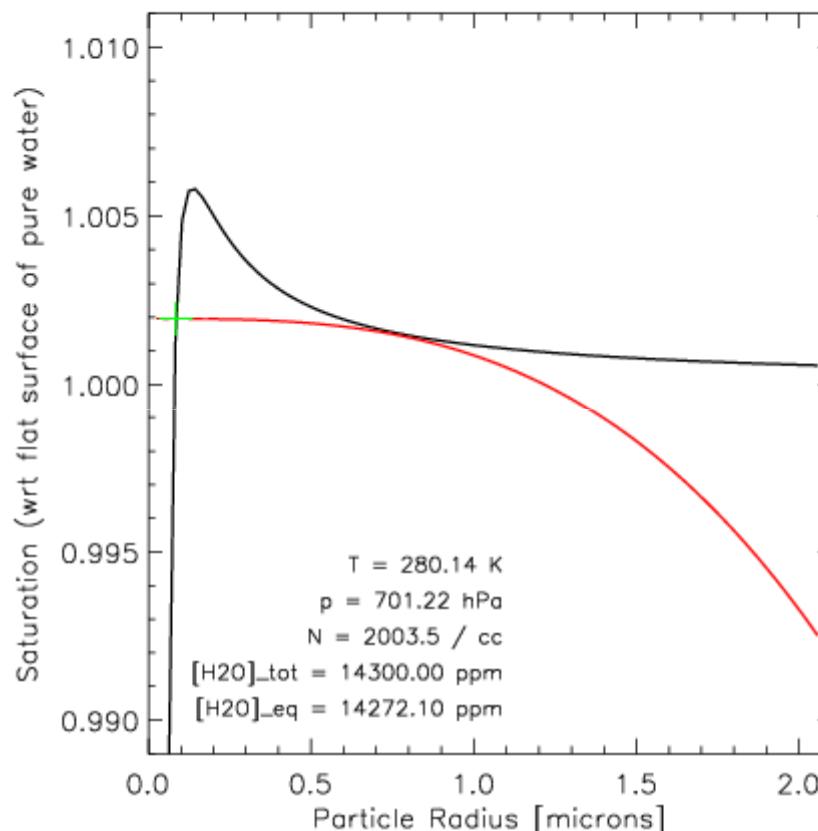
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

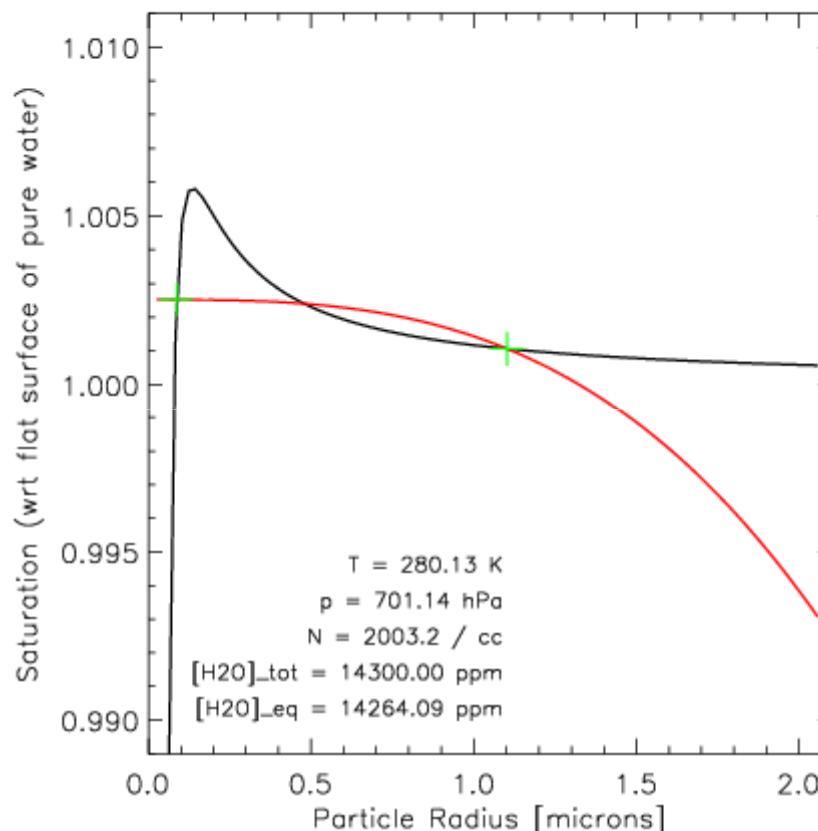
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

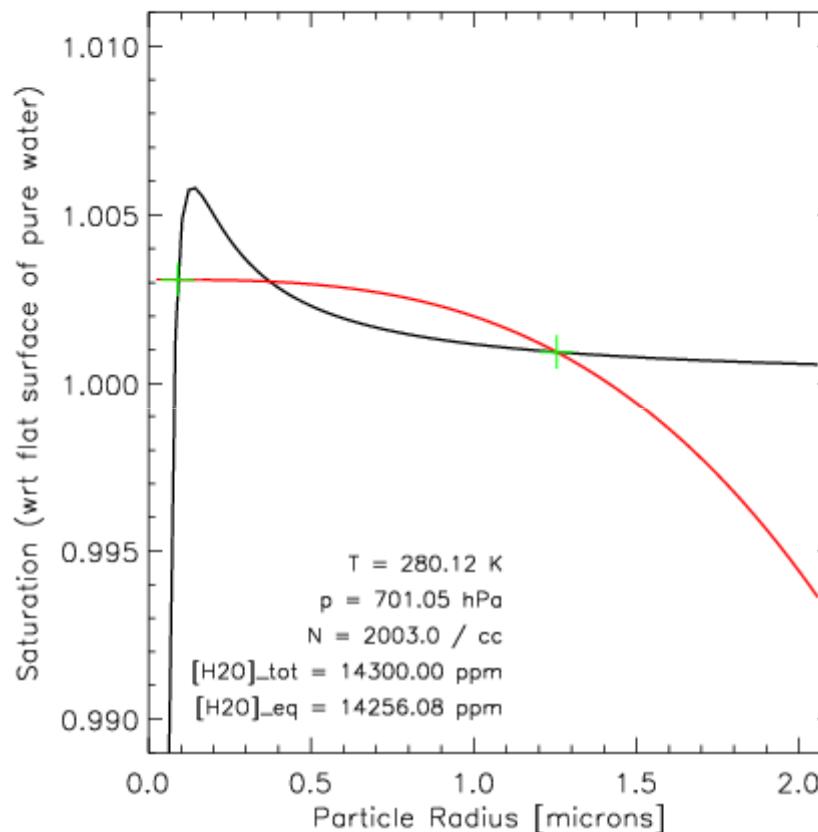
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

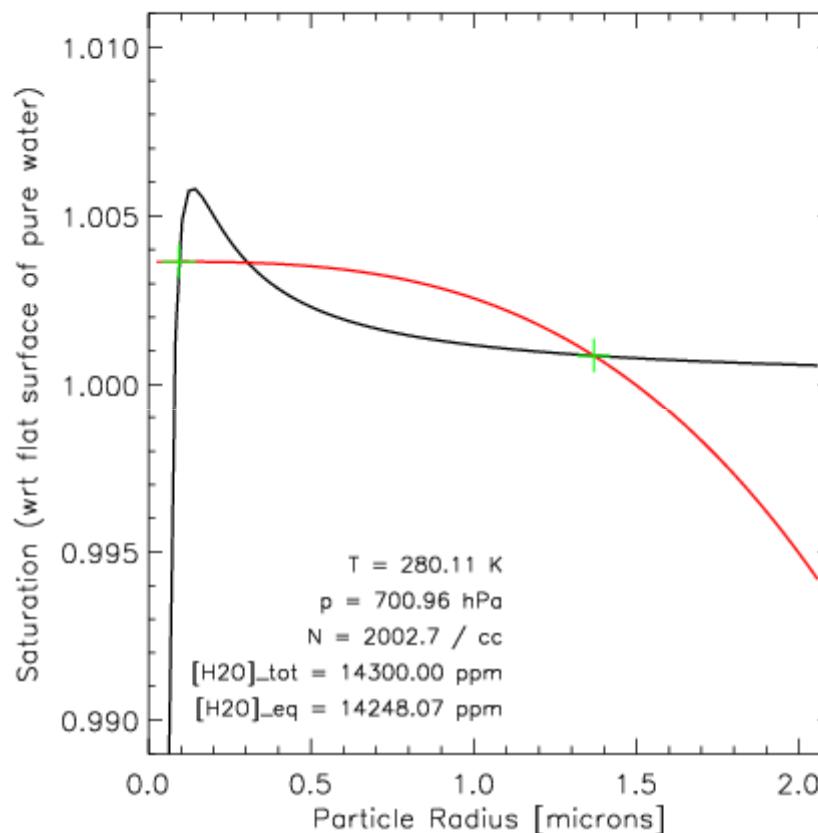
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

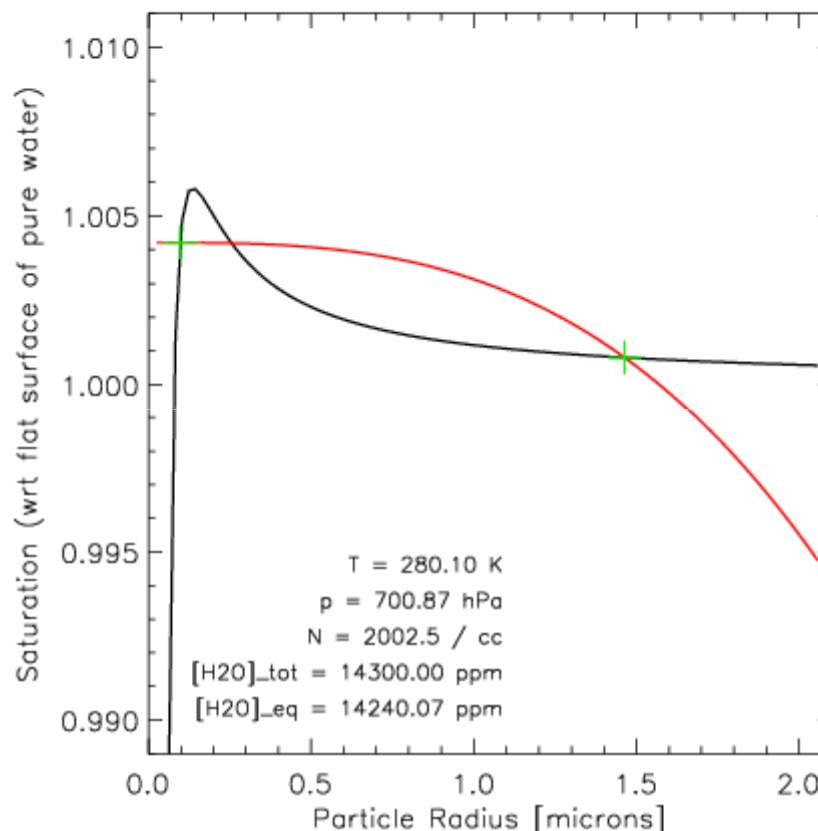
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

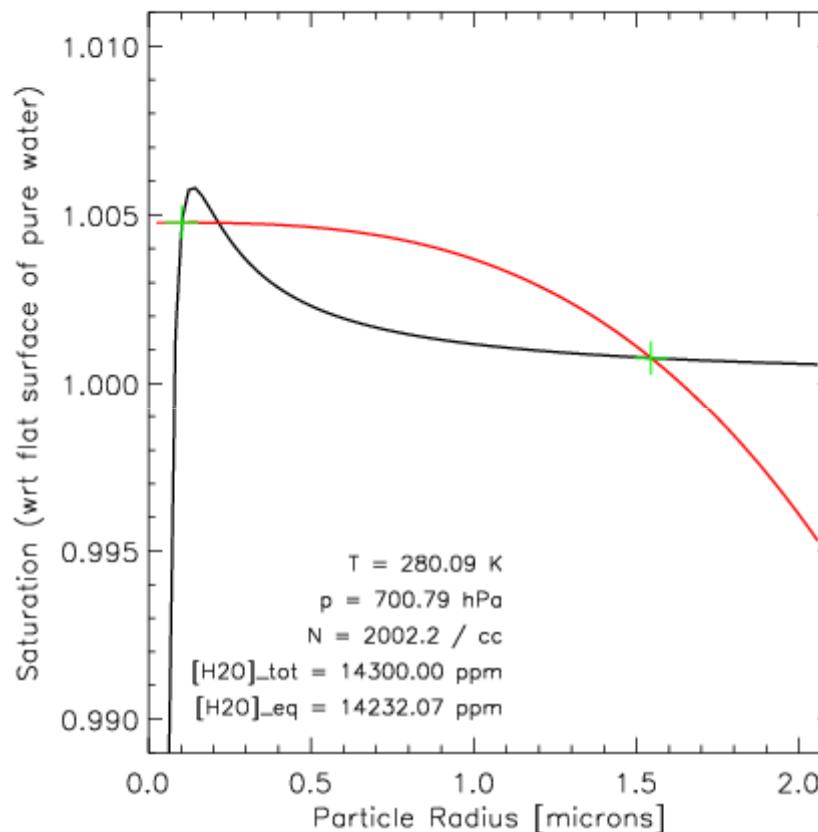
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

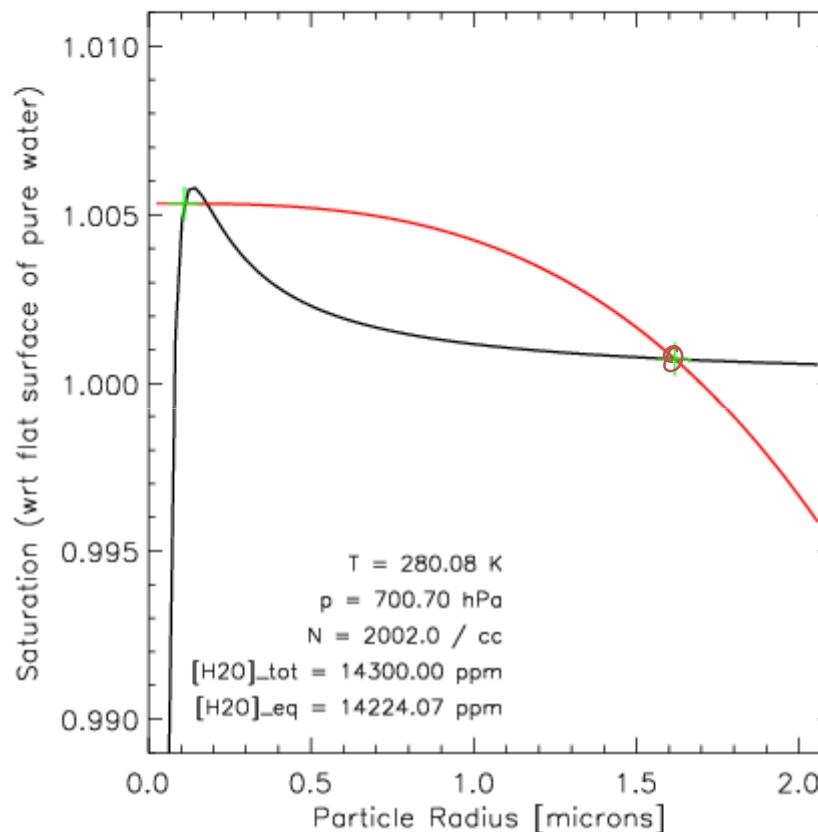
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 $2000 \text{ cm}^{-3}$

**Salt mass:**  
 $2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$

**Mass balance:**

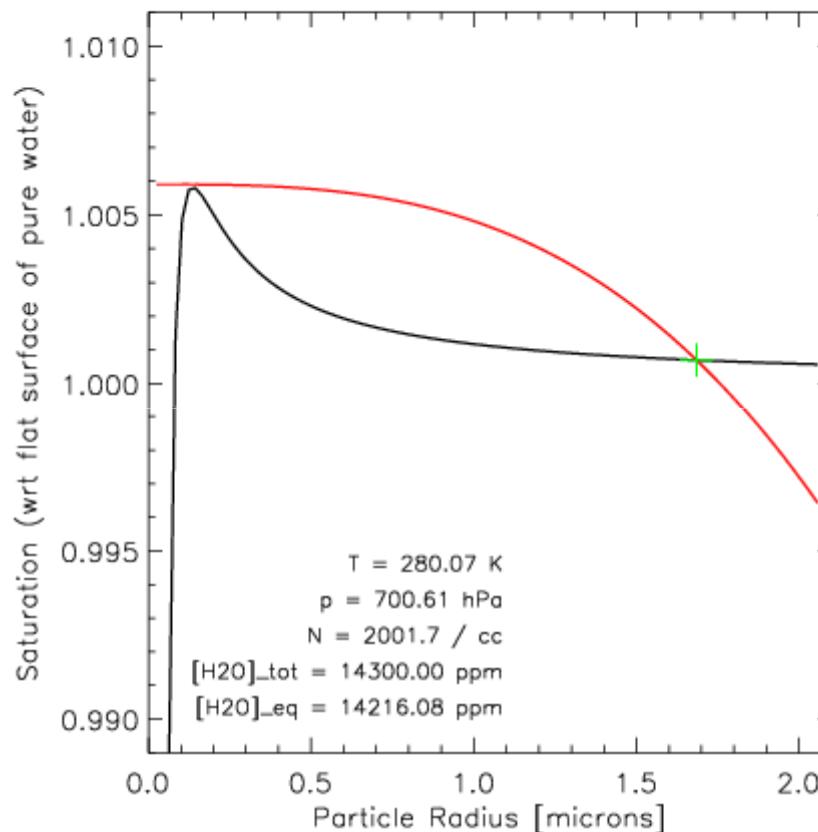
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

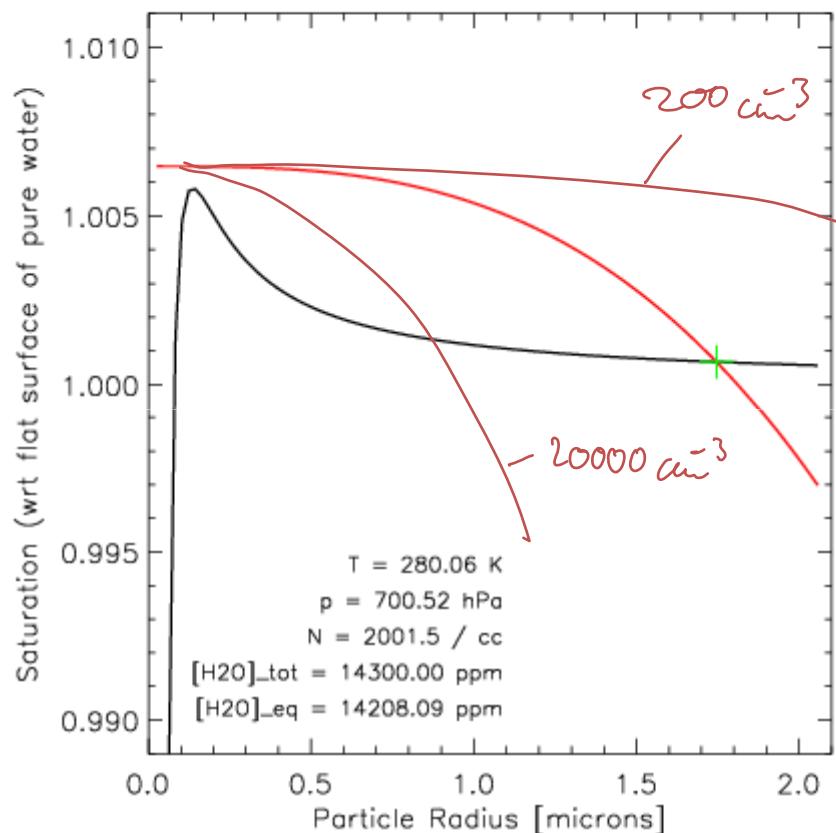
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

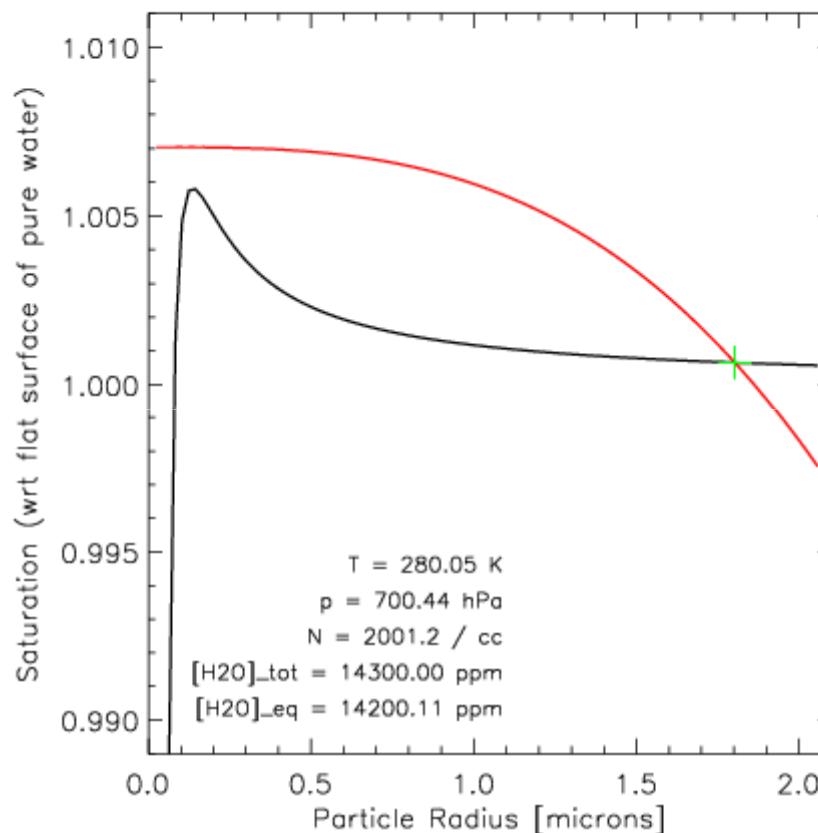
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

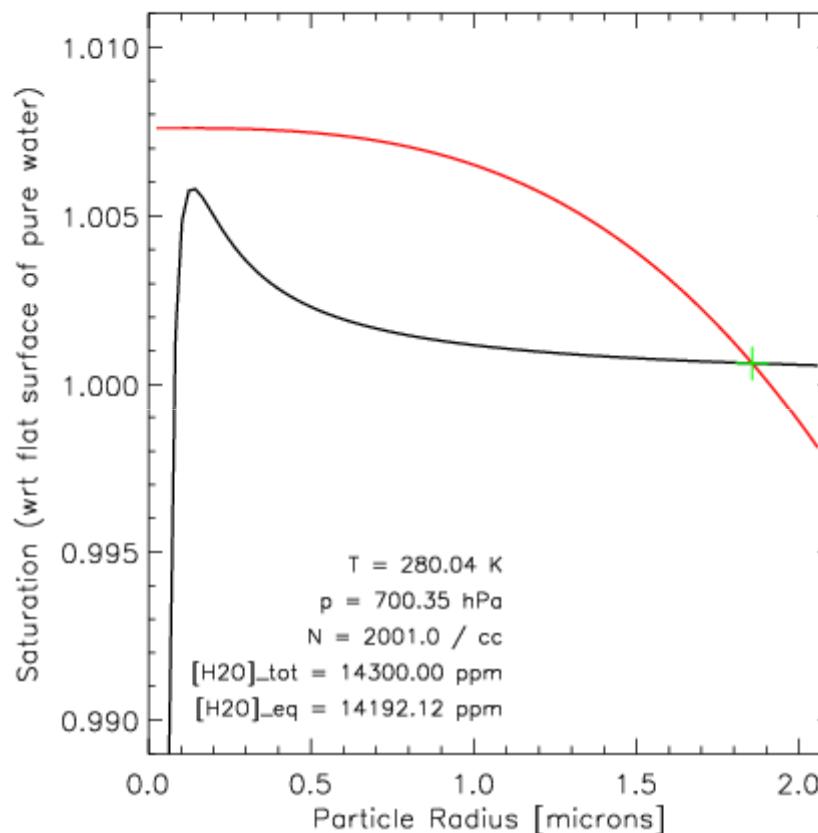
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

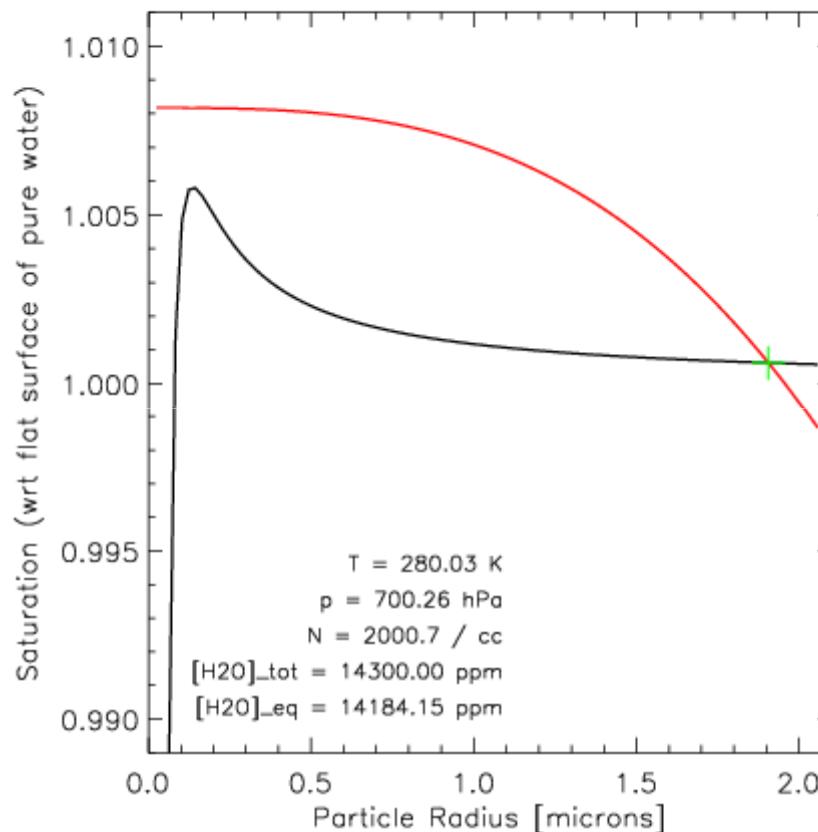
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

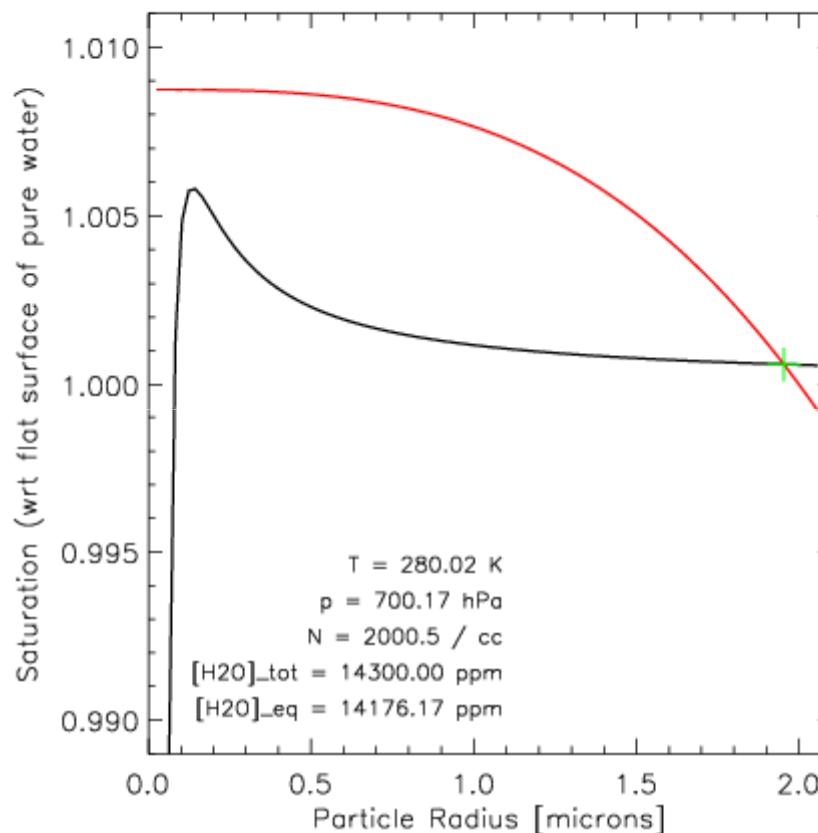
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 **$2000 \text{ cm}^{-3}$**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

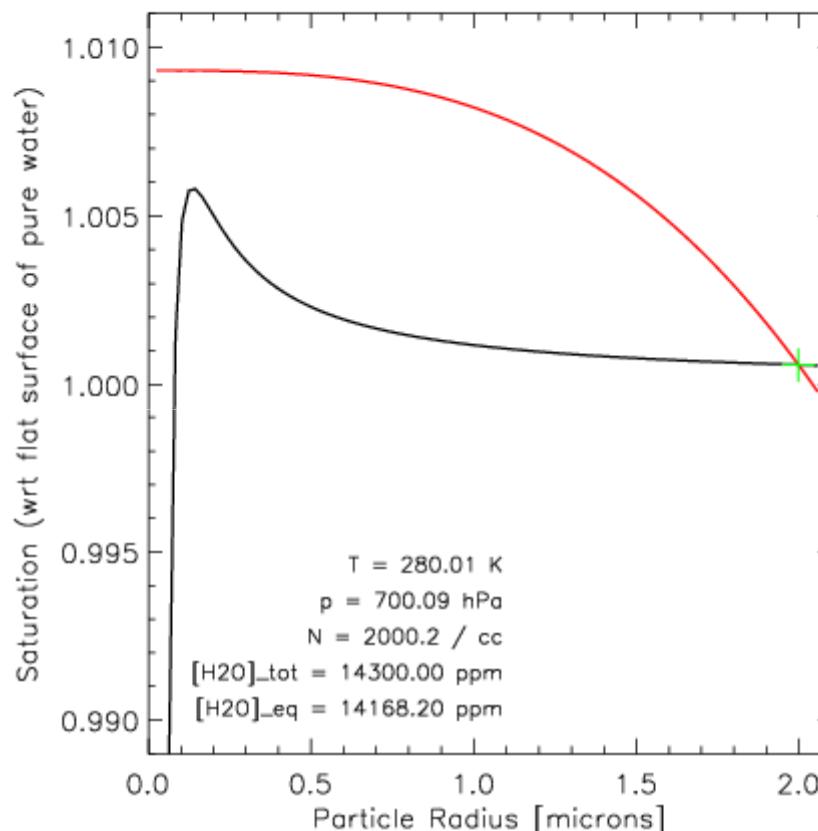
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
 **$2000 \text{ cm}^{-3}$**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

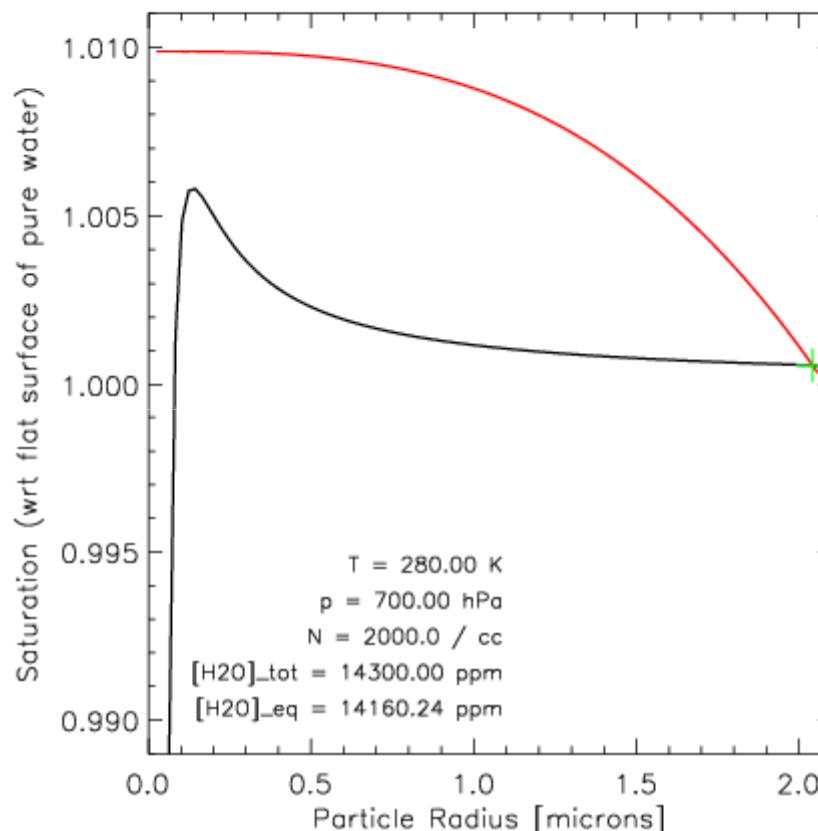
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

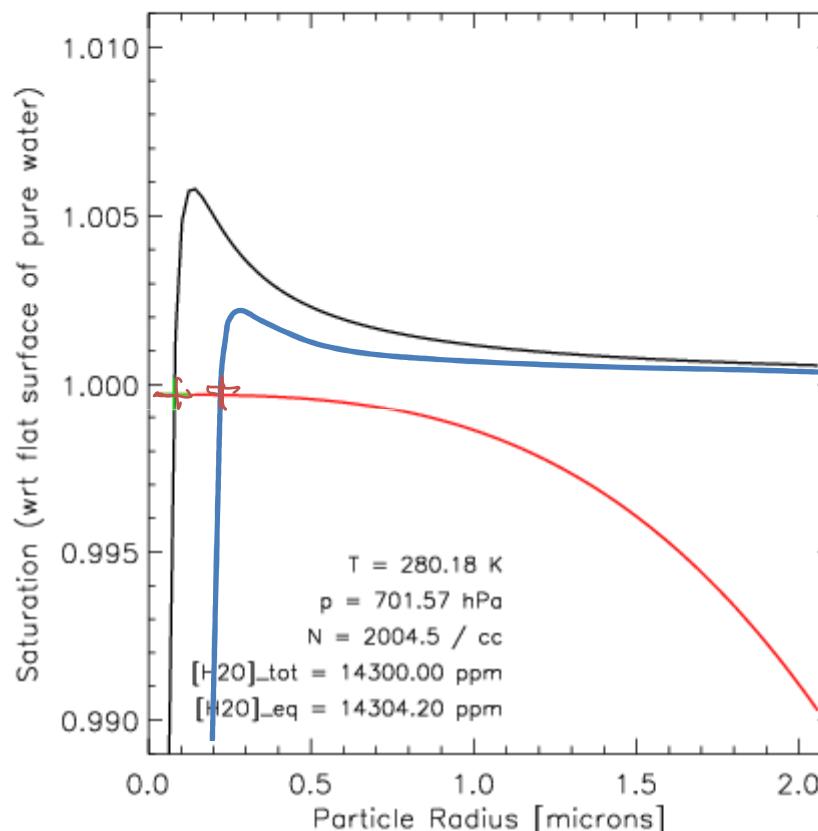
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

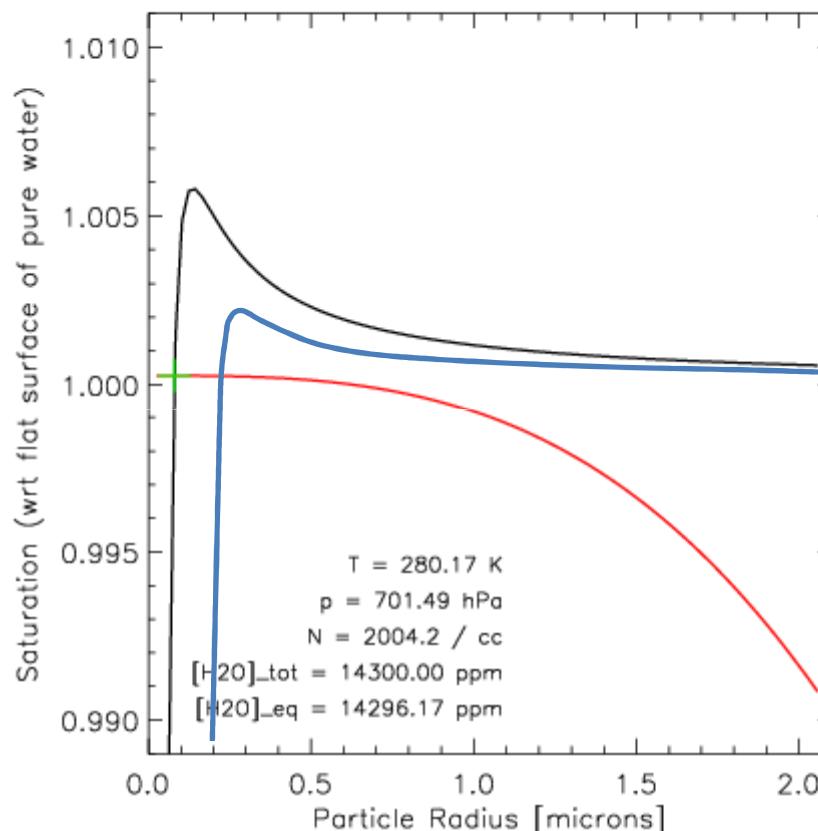
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

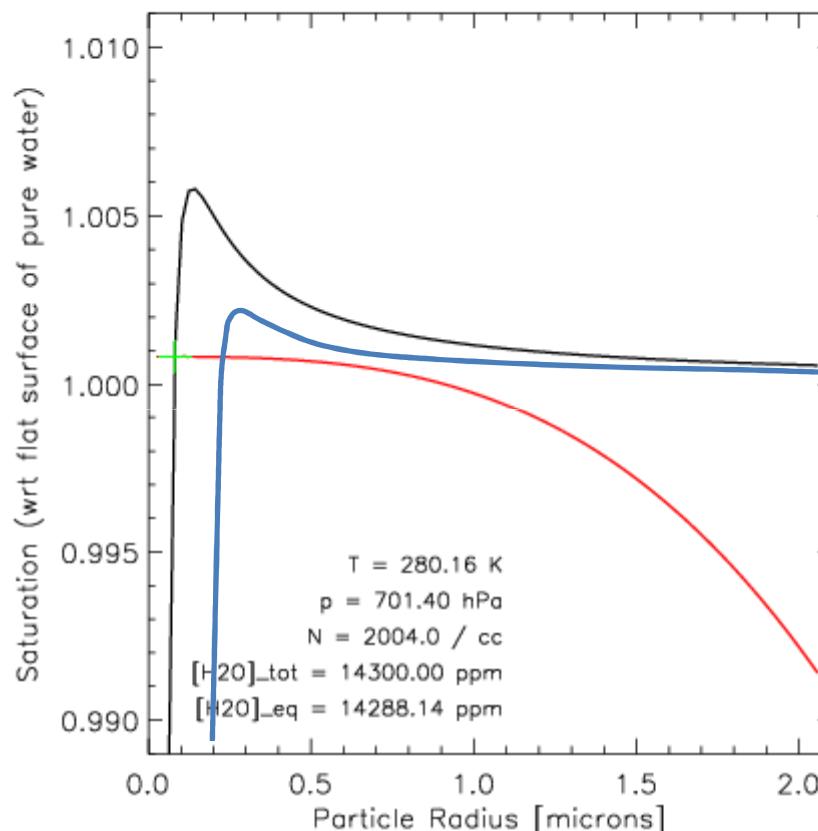
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

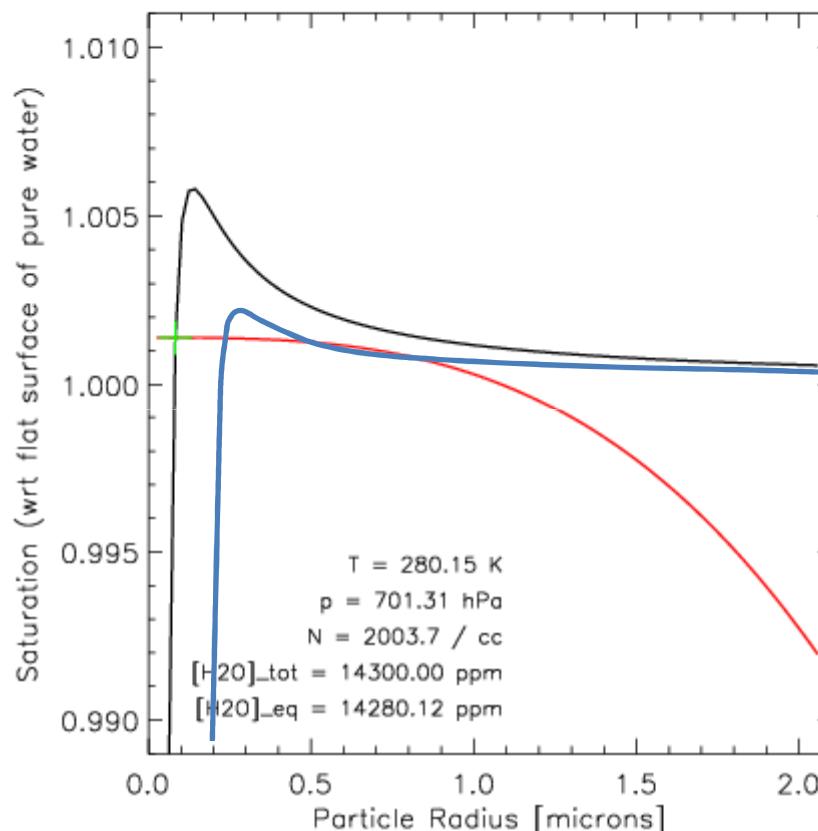
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**  
**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

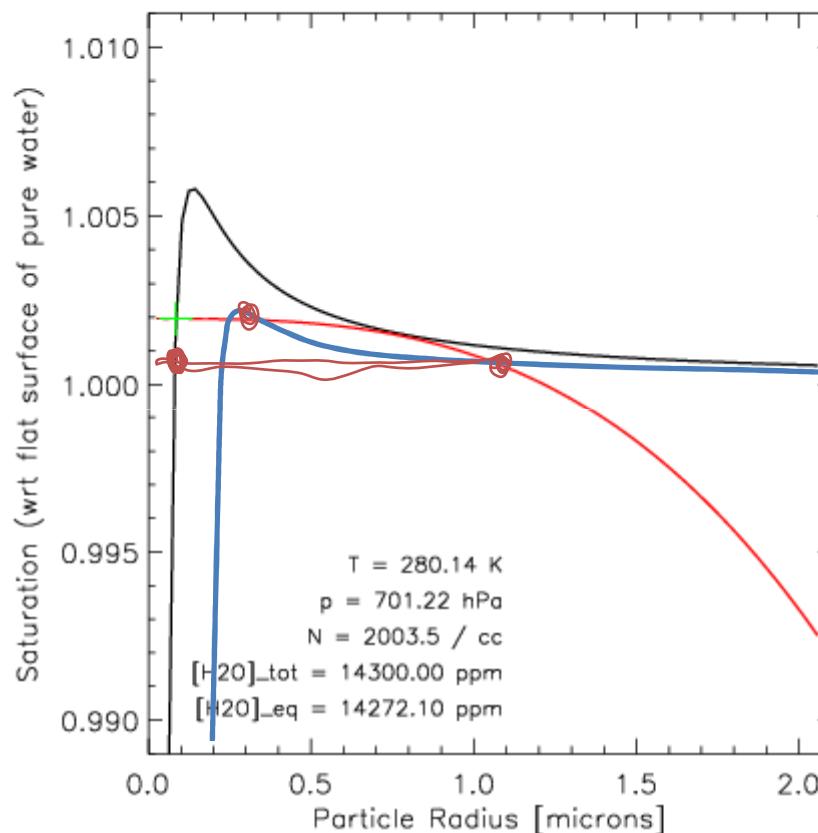
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

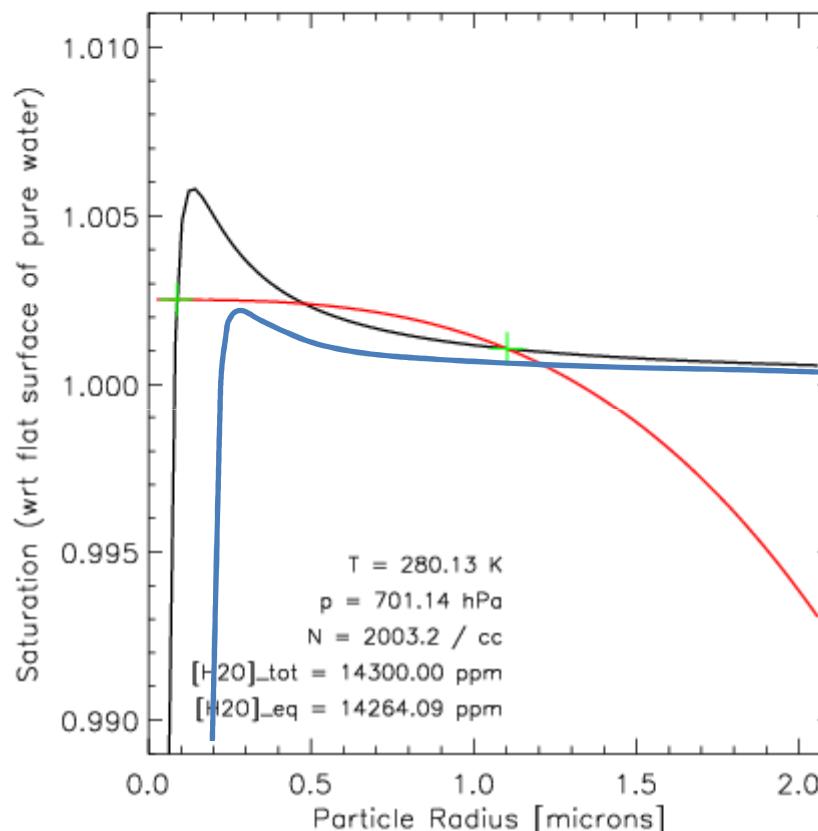
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

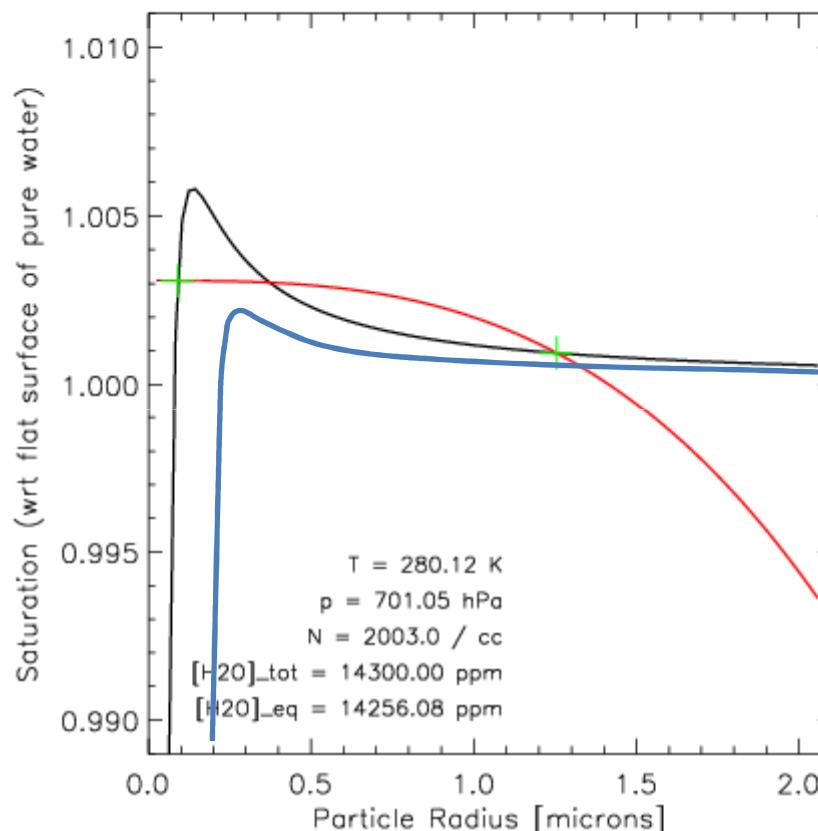
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

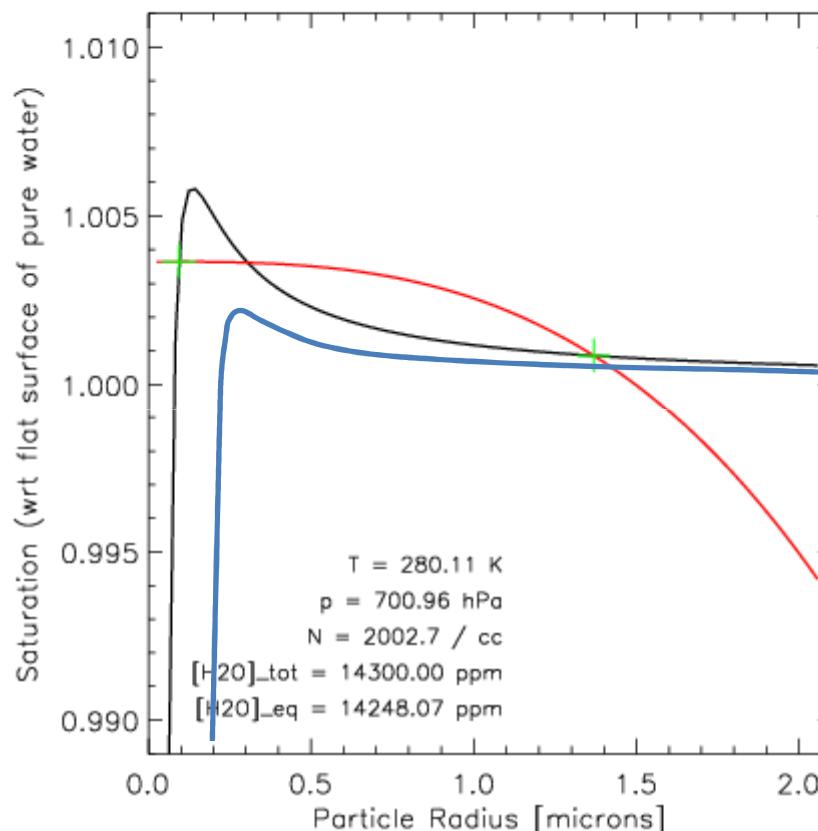
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

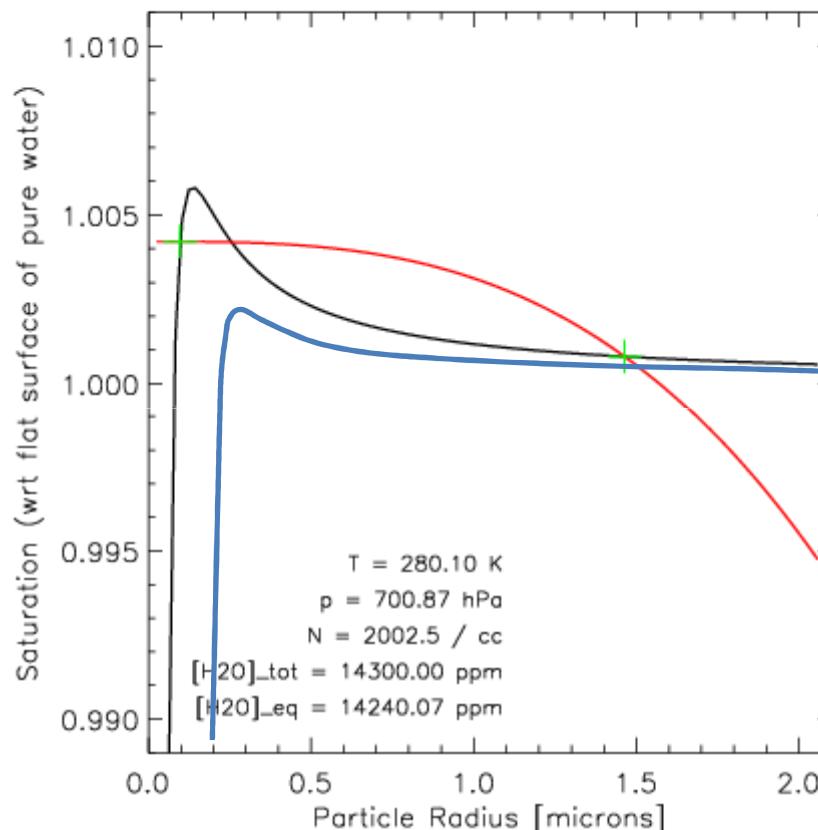
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

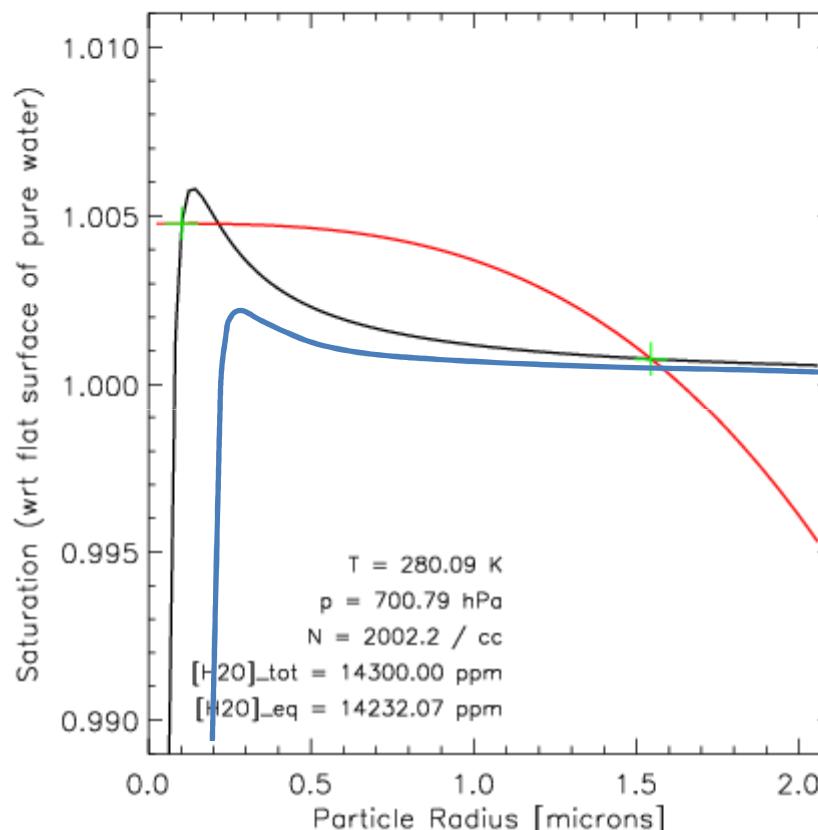
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**   
**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

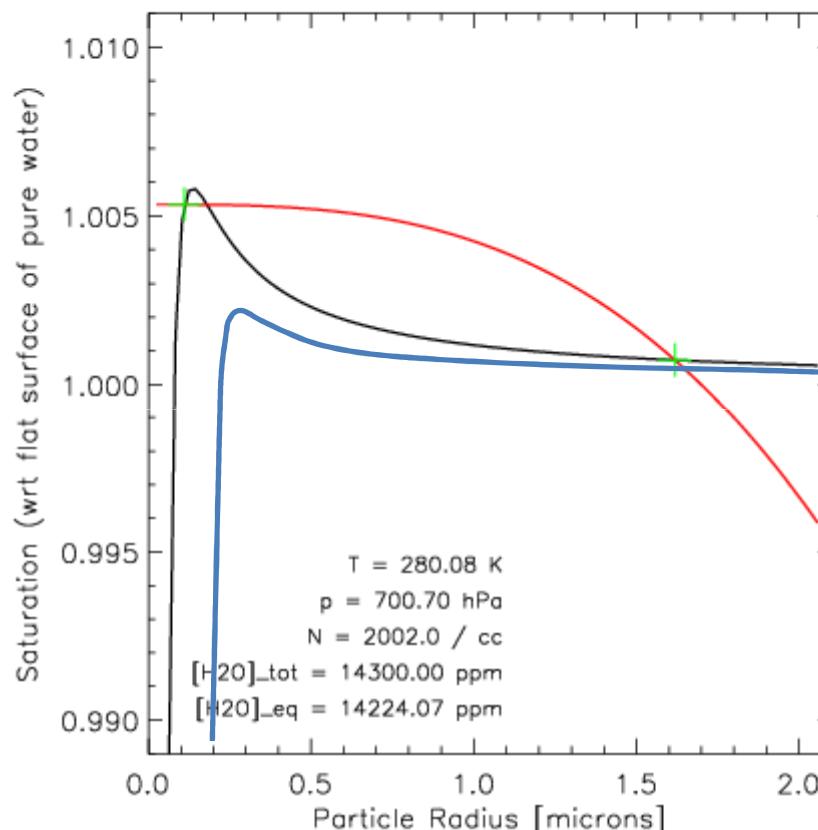
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

$701.57 \text{ hPa} \rightarrow 700.00 \text{ hPa}$

$280.18 \text{ K} \rightarrow 280.00 \text{ K}$

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

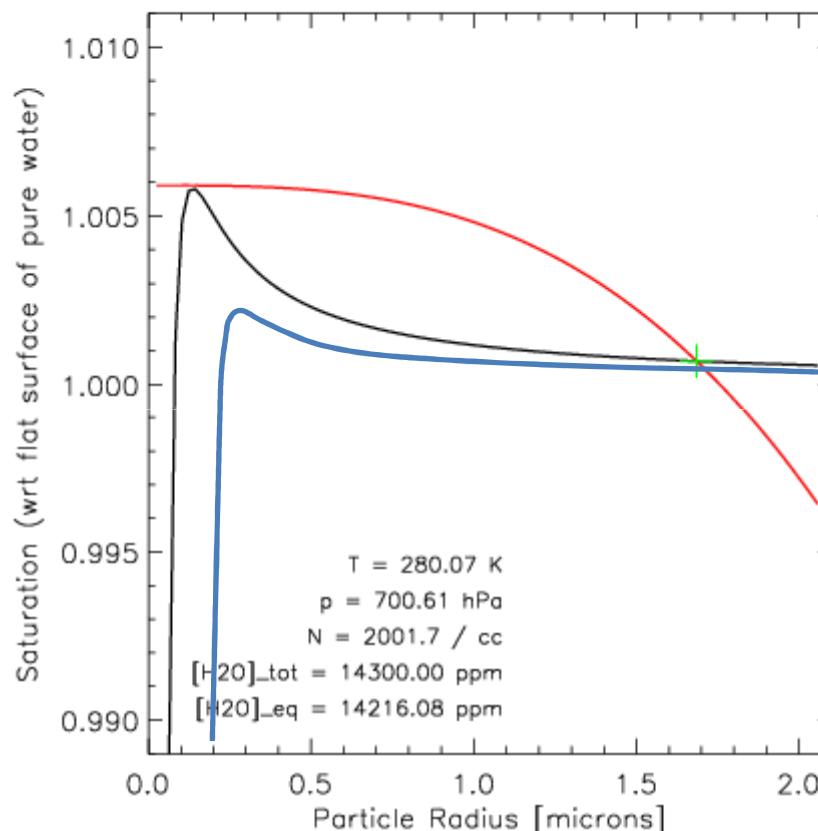
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

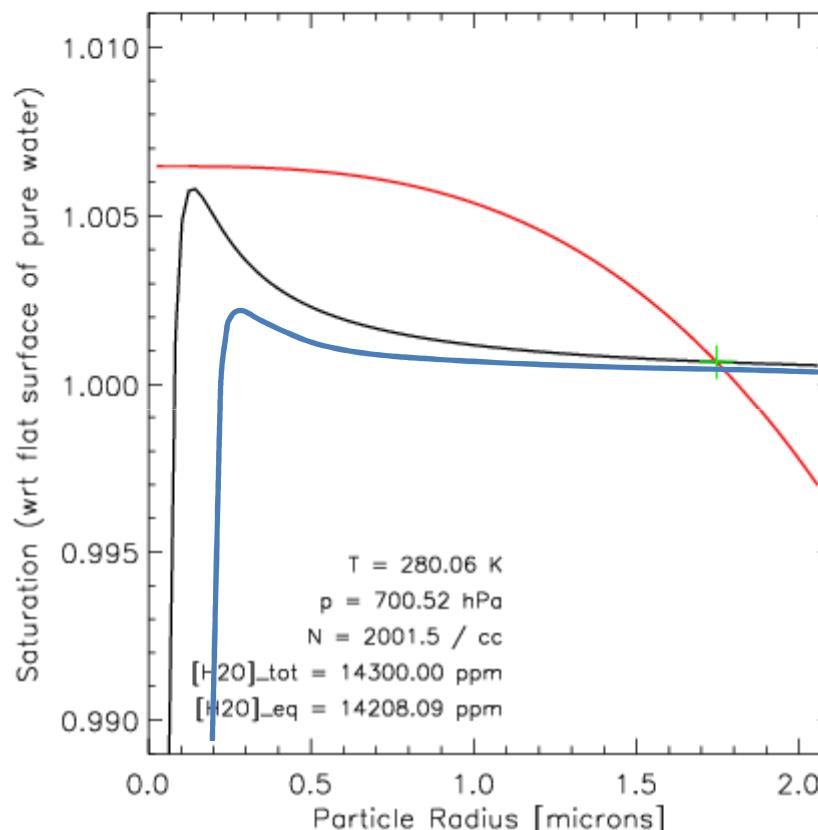
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

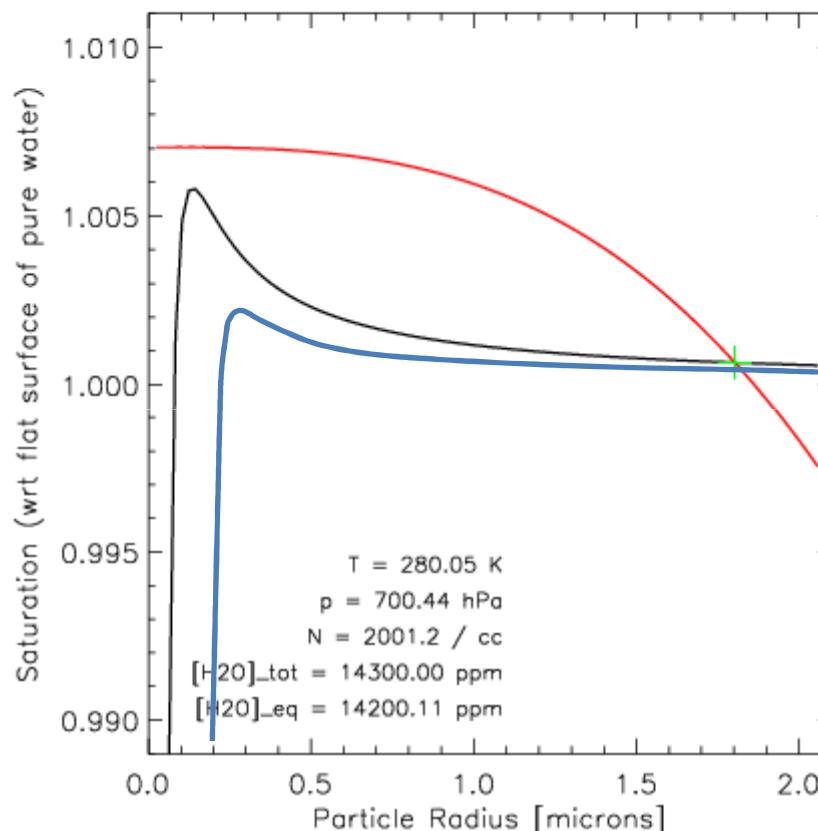
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

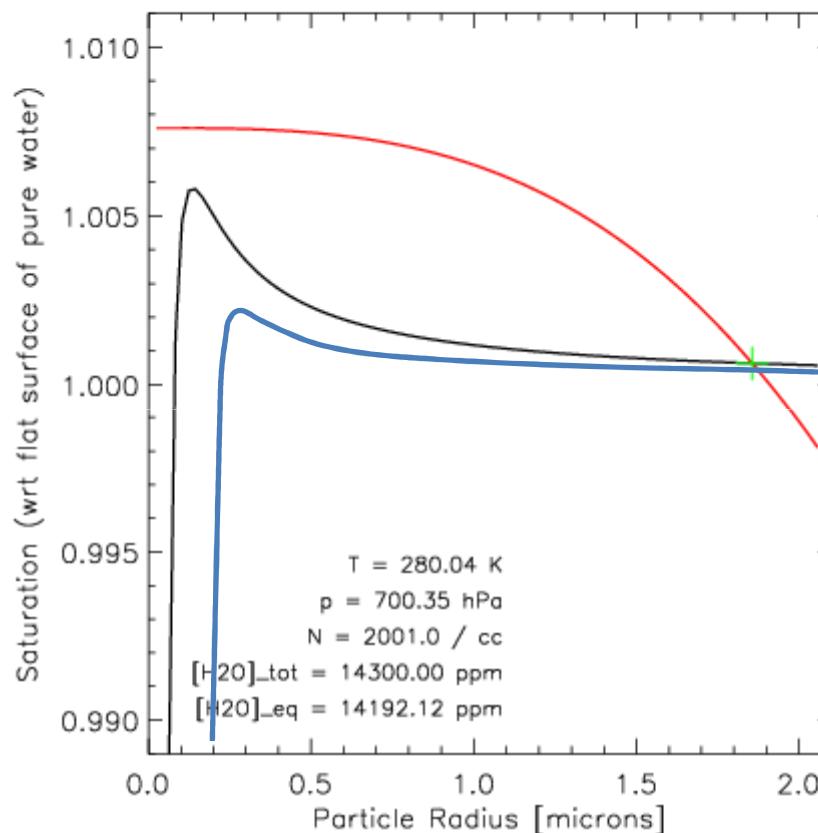
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**  
**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

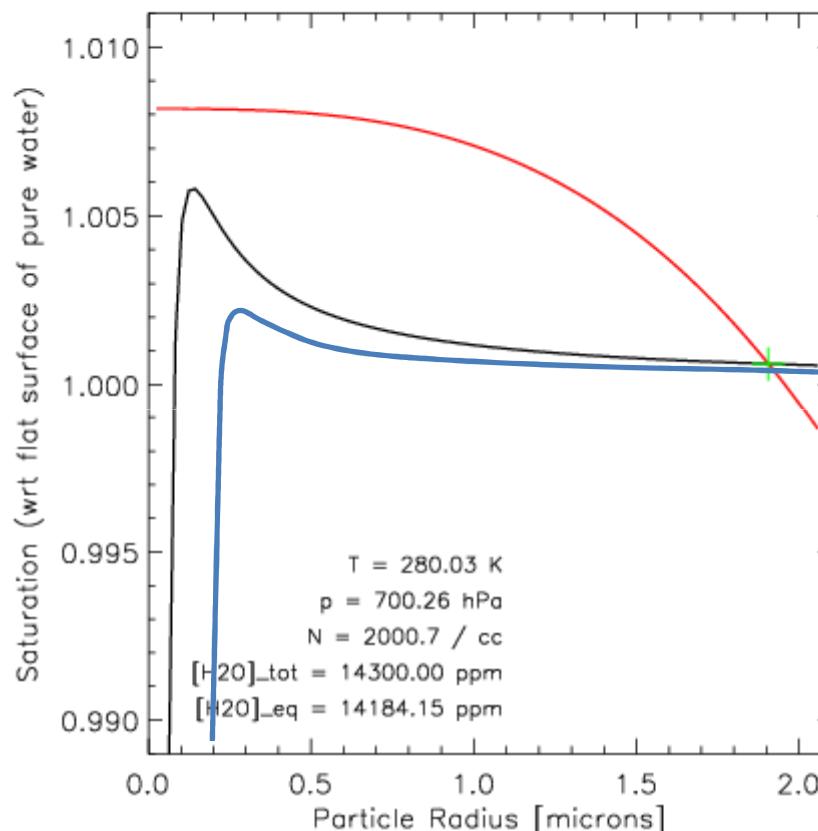
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
 **$2 \times 10^{-16} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Minority with**  
 **$2 \times 10^{-15} \text{ g } (\text{NH}_4)_2\text{SO}_4$**

**Mass balance:**

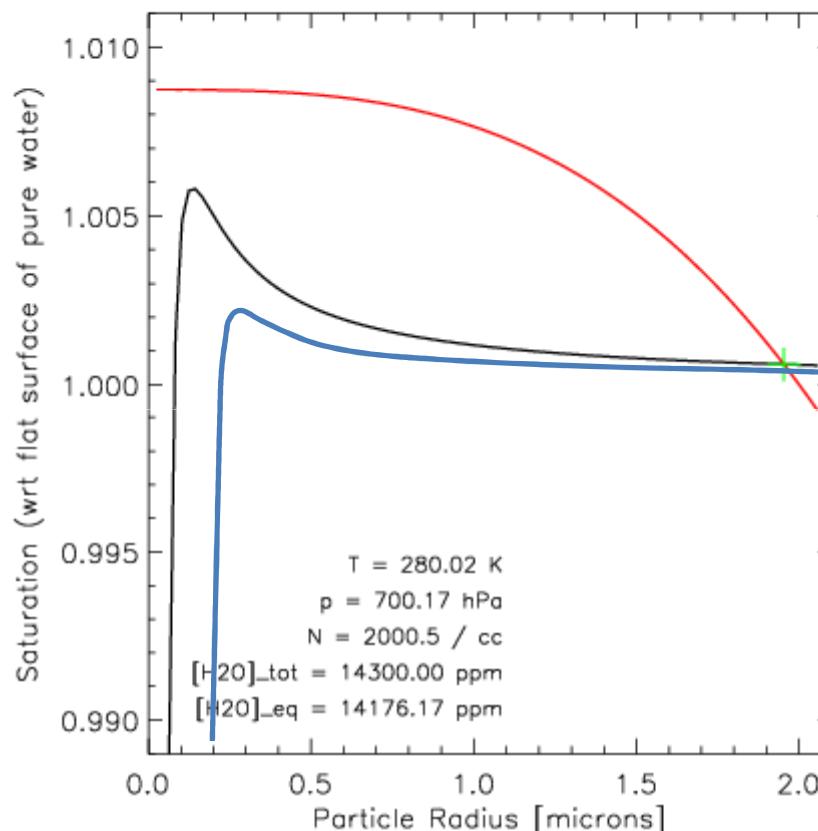
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**  
**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

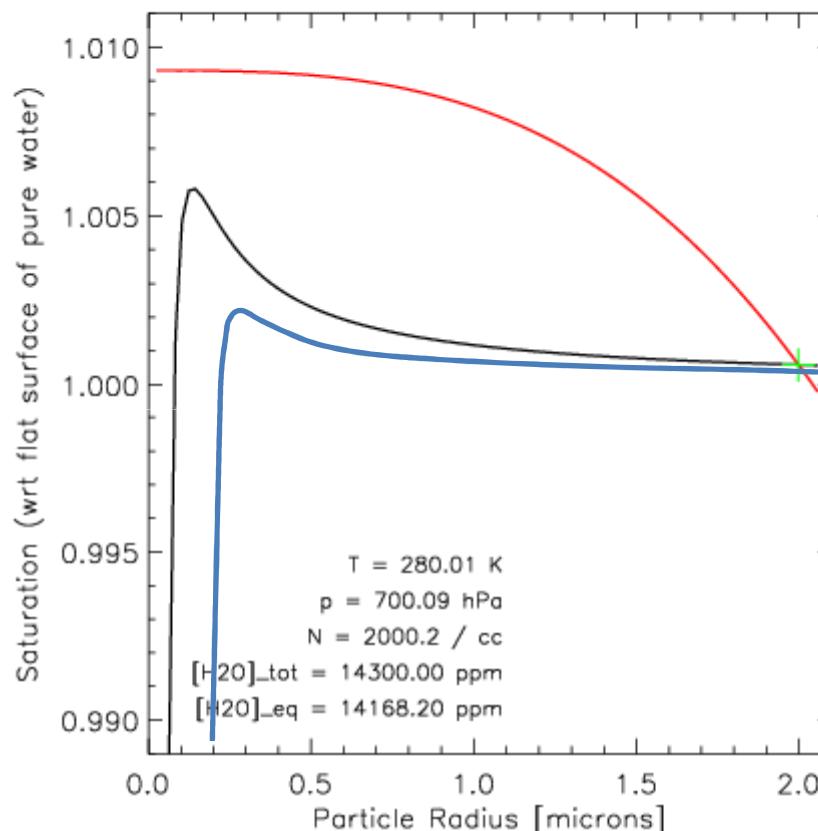
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

701.57 hPa → 700.00 hPa

280.18 K → 280.00 K

(Lift of ~17 m)



$$\chi^{tot} = 14300 \text{ ppm} \\ = 1.43 \%$$

**Monodisperse salt particles:**

**Number density:**  
**2000 cm<sup>-3</sup>**

**Salt mass:**  
**2×10<sup>-16</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Minority with**  
**2×10<sup>-15</sup>g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>**

**Mass balance:**

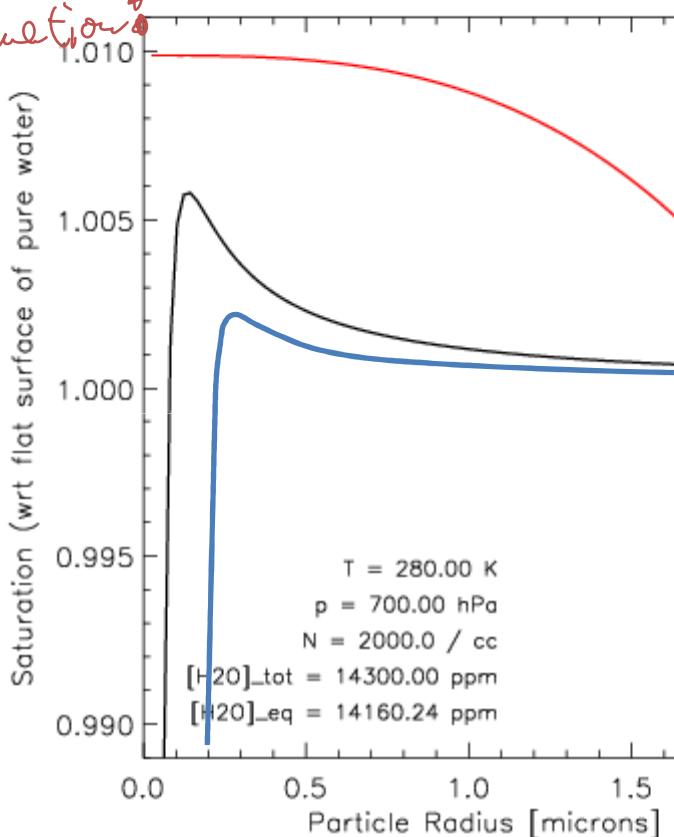
$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \quad \Rightarrow \quad S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w^{tot}}{p_w^{vap}(T)} - \frac{NkT}{p_w^{vap}(T)} \left( \frac{r}{r_w} \right)^3$$

# Adiabatic cooling of an air parcel

Note: other processes, e.g. coalescence, also lead to large particle formation.

→ The minority has the “size advantage”. But whether it loses or wins the battle depends on the cooling rate, i.e. on kinetics.

701.57 hPa → 700.00 hPa  
280.18 K → 280.00 K  
(Lift of ~17 m)



For everyone who has will be given more, and he will have an abundance. Whoever does not have, even what he has will be taken from him.

Denn wer hat, dem wird gegeben, und er wird im Überfluss haben; wer aber nicht hat, dem wird auch noch weggenommen, was er hat.

Car à celui qui a, on donnera, et il aura encore davantage; mais à celui qui n'a pas, on ôtera même ce qu'il a.

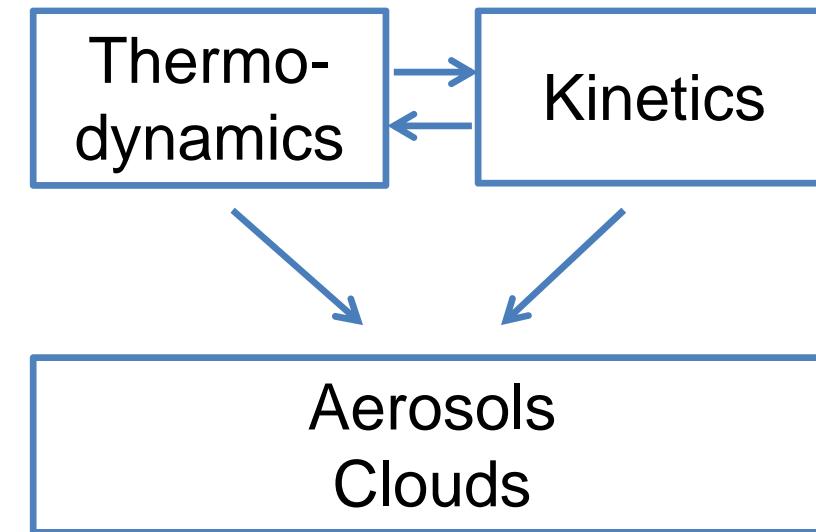
**Mass balance:**

$$p_w = n_w kT = \left( n_w^{tot} - N \frac{4\pi}{3} \frac{r^3}{v_w} \right) kT \Rightarrow S = \frac{p_w}{p_w^{vap}(T)} = \frac{p_w(T)}{p_w(T) - p_w(T) \frac{r^3}{v_w}}$$

(Mt 25,29)

**Formation of water clouds**

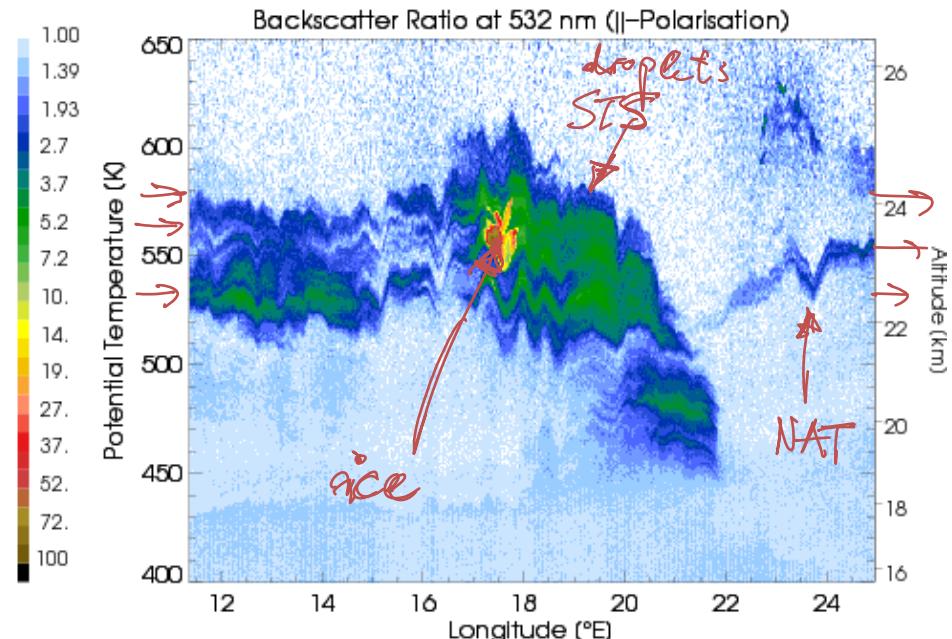
**Formation of Polar Stratospheric Clouds**



*How far do we get with thermodynamics in explaining cloud formation?*

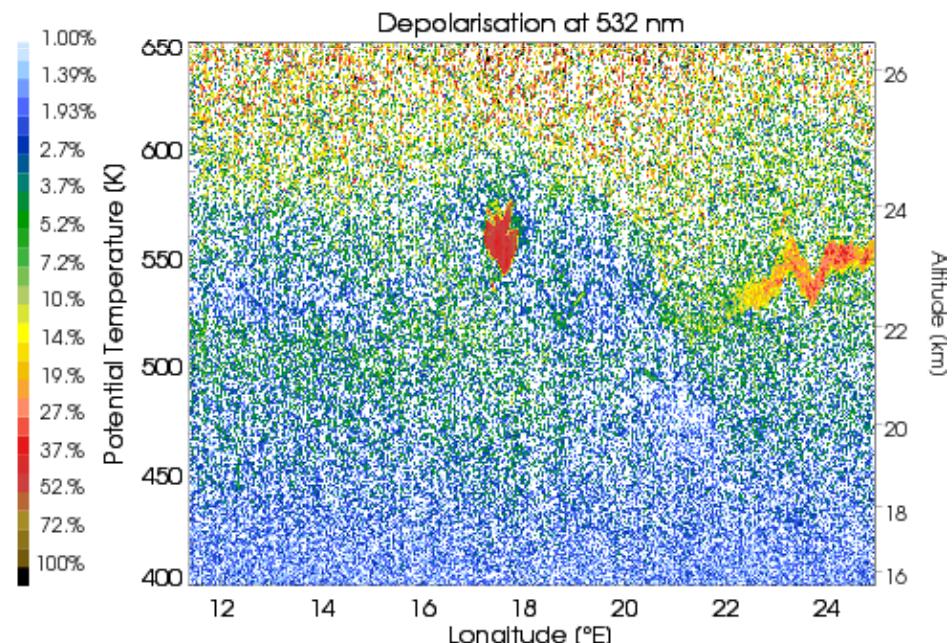
## 3 Types of Polar Stratospheric Clouds (PSCs)

- (1) Ice
- (2) NAT (nitric acid trihydrate  
=  $\text{HNO}_3 \cdot 3\text{H}_2\text{O}$ , crystalline)
- (3) STS (supercooled ternary  
solutions,  $\text{H}_2\text{SO}_4/\text{HNO}_3/\text{H}_2\text{O}$ )



Lidar observations  
PSCs over the Norwegian Alps  
Wirth et al. (1994)

sphericity  
of scatterers



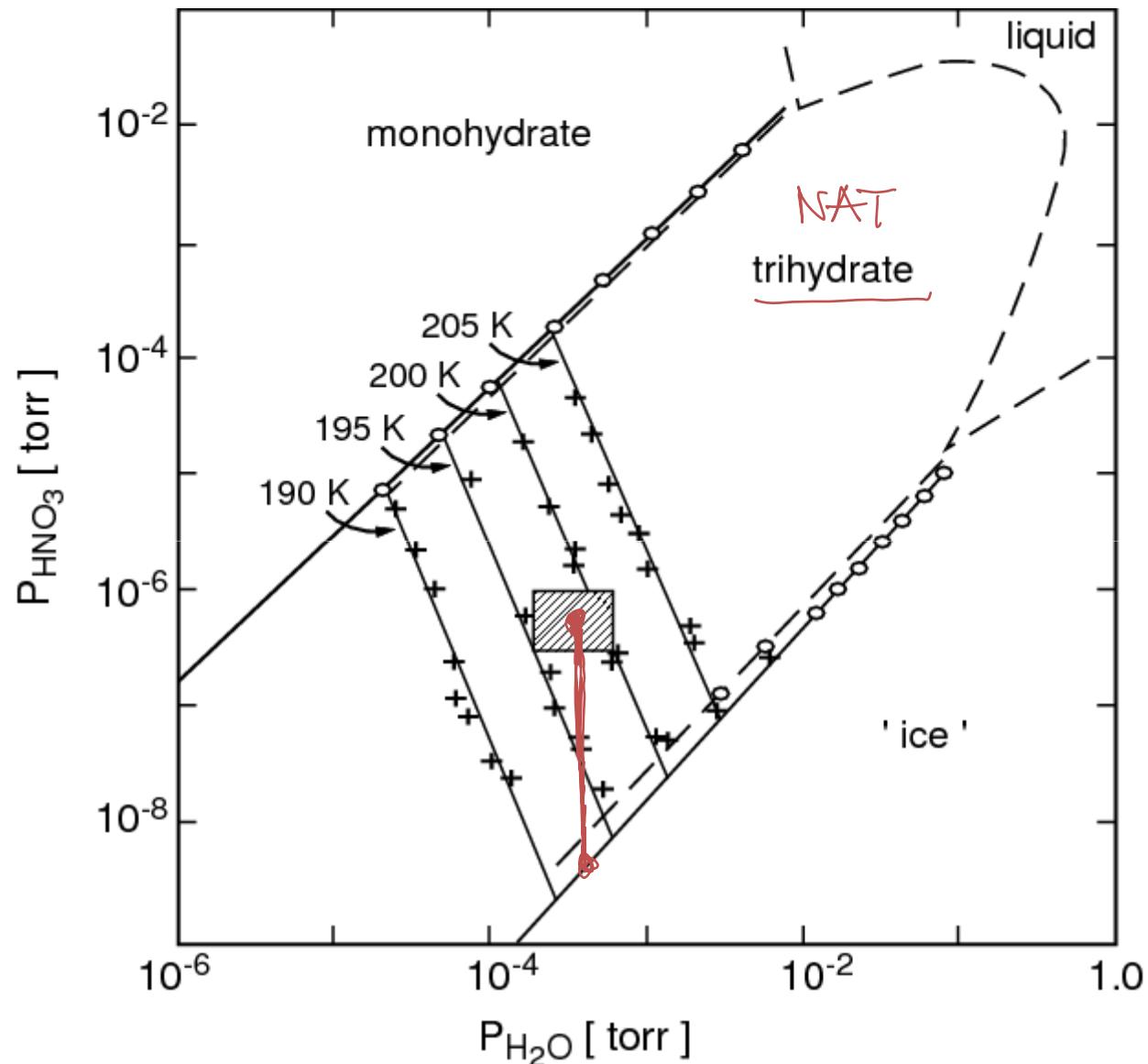
Scandinavian Alps

Hanson and  
Mauersberger (1986):

Mass spectrometric  
measurements  
Formation of NAT  
PSCs

$$T_{\text{ice}} \approx 188 \text{ K}$$

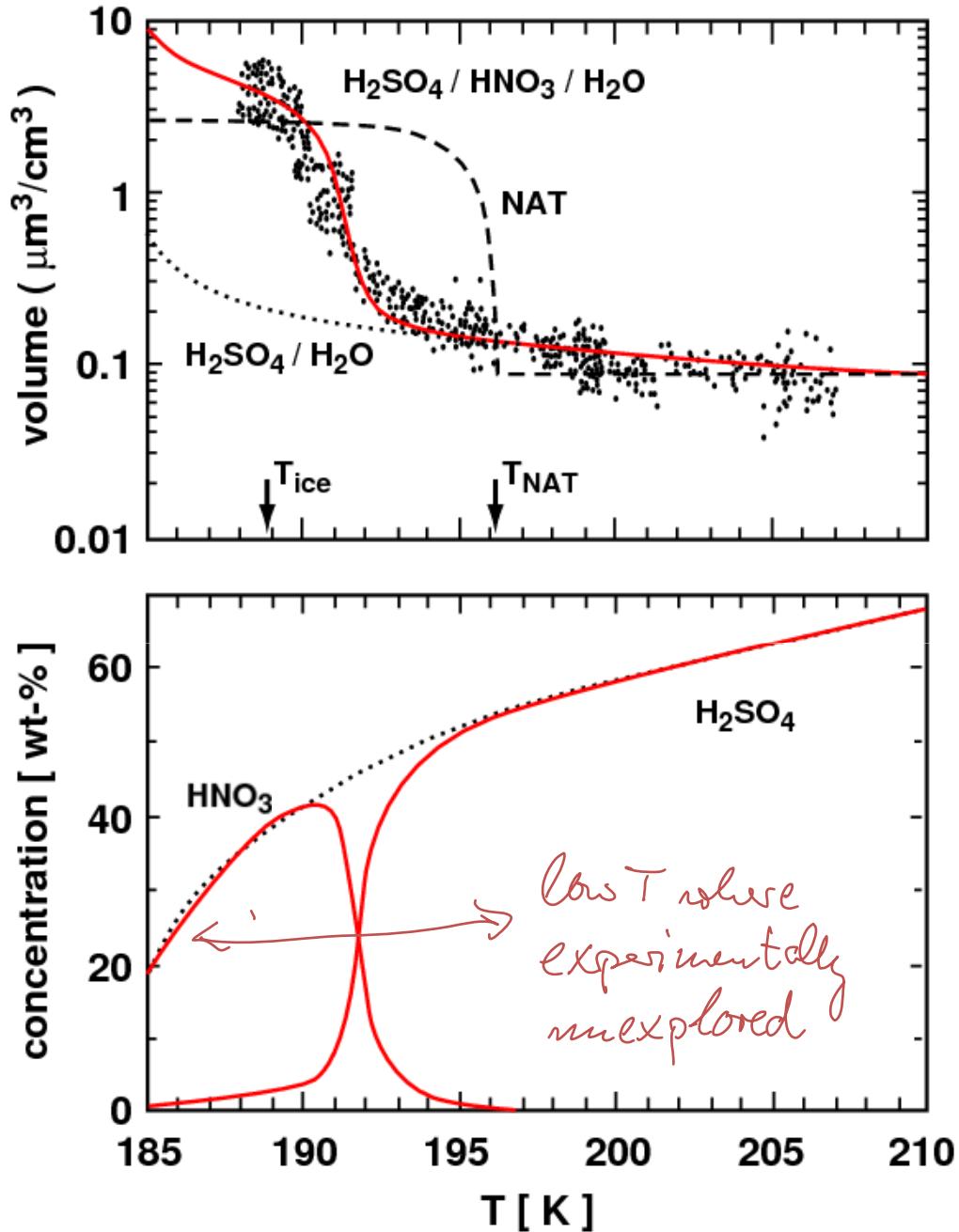
$$T_{\text{NAT}} \approx 195 \text{ K}$$



Carslaw et al. (1994):

Thermodynamic  
modeling of STS  
(supercooled ternary  
solutions,  
 $\text{H}_2\text{SO}_4/\text{HNO}_3/\text{H}_2\text{O}$ )

measurements  
ER-2  
Norway → North Pole



## **Thermodynamics of Electrolytes.**

### **I. Theoretical Basis and General Equations**

Kenneth S. Pitzer, J. Phys. Chem., 77, 268 - 277, 1973:

#### **General Equations**

Let us now set up a system of equations for the thermodynamic properties of pure or mixed electrolytes in rather general form. We will later choose the exact form for certain functions by comparison with experimental data. The total excess Gibbs energy for a solution containing  $n_w$  kg of solvent and  $n_i, n_j, \dots$  moles of solute species  $i, j, \dots$  is taken to be

$$\frac{G^{\text{ex}}}{RT} = n_w f(I) + \frac{1}{n_w} \sum_{ij} \lambda_{ij}(I) n_i n_j + \frac{1}{n_w^2} \sum_{i,j,k} \mu_{ijk} n_i n_j n_k \quad (21)$$

Here  $f(I)$  is a function of ionic strength (also temperature and solvent properties) expressing the effect of the long-range electrostatic forces;  $f(I)$  may have the form of the

## Pitzer Ion-Interaction Model:

$$\frac{G^{\text{ex}}}{RT} = n_w f(I) + \frac{1}{n_w} \sum_{ij} \lambda_{ij} n_i n_j + \frac{1}{n_w^2} \sum_{ijk} \mu_{ijk} n_i n_j n_k + \dots$$

long range ionic interaction potential ( $I$  = ion strength)

short range 2-body interactions of species ( $i, j, k, w$ )

short range 3-body interactions of species ( $i, j, k, w$ )

neglect higher order terms

Activities:  $\ln a_i = \frac{1}{RT} \times \frac{\partial G}{\partial n_i}$

Theoretical description for  $f(I)$ : Debye-Hückel theory (1928)

Data used to parameterize the interaction potentials  $\lambda_{ij}, \mu_{ijk}$ :

(1)  $p^{\text{vap}}$  measurements: for water  $p_w = p_w^0 \times a_w ; \quad \ln a_w = \frac{1}{RT} \times \frac{\partial G}{\partial n_w}$

for solutes,  
e.g.  $\text{HCl} \leftrightarrow \text{H}^+ + \text{Cl}^-$   $p_{\text{HCl}} = \frac{a_{\text{H}^+} a_{\text{Cl}^-}}{K_H} ; \quad \ln a_{\text{HCl}} = \frac{1}{RT} \times \frac{\partial G}{\partial n_i}$

(2) Electromotive force measurements:  $E = E_0 + \frac{F}{RT} \times \ln(a_{\text{H}^+} a_{\text{Cl}^-})$

(3) Enthalpy measurements:  $\Delta H = \frac{\partial(\Delta G/T)}{\partial(1/T)}$

(4) Measurements of heat capacities.

(5) Measurements of solubilities.

(6) Measurements of dissociation coefficients

## Pitzer Ion-Interaction Model:

$$\frac{G^{\text{ex}}}{RT} = n_w f(I) + \frac{1}{n_w} \sum_{ij} \lambda_{ij} n_i n_j + \frac{1}{n_w^2} \sum_{ijk} \mu_{ijk} n_i n_j n_k$$

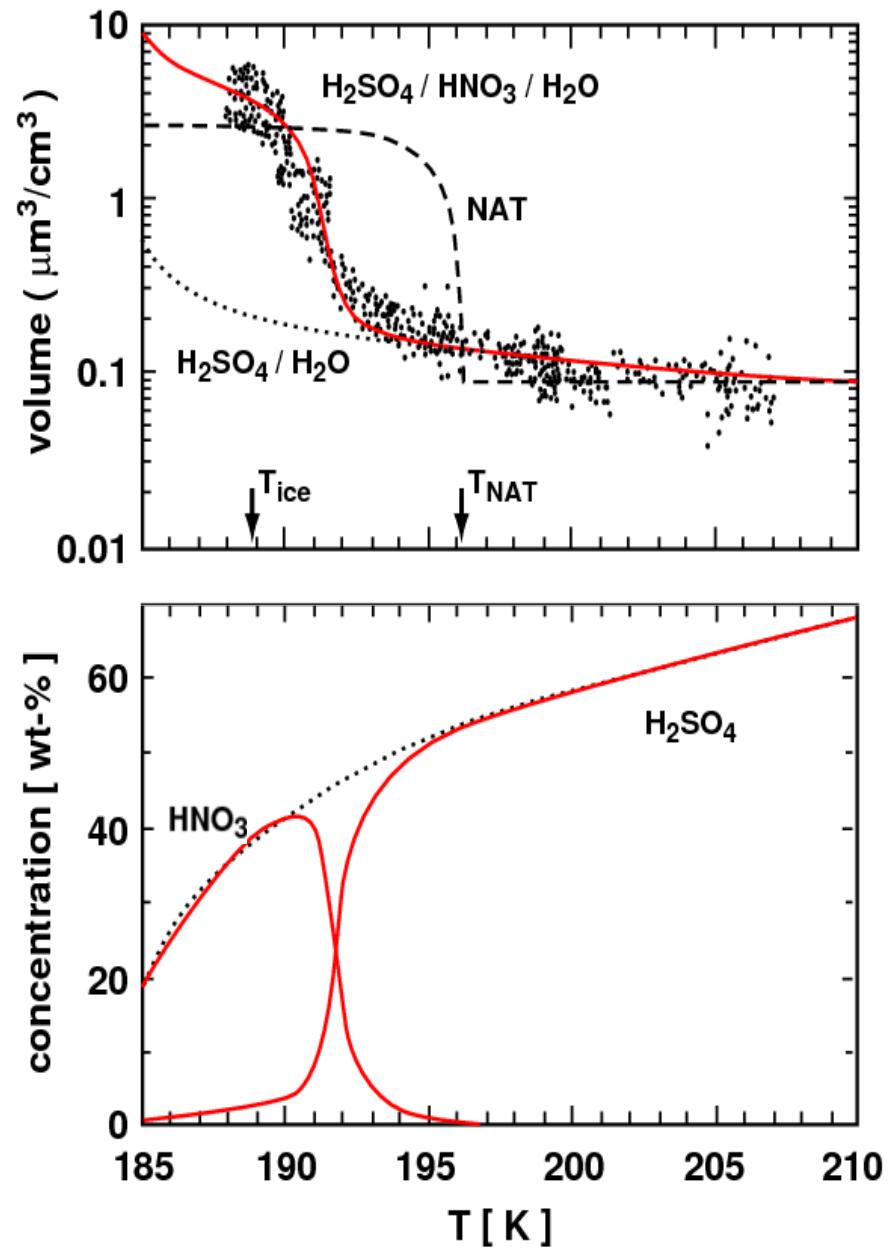
Activities:  $\ln a_i = \frac{1}{RT} \times \frac{\partial G}{\partial n_i}$

$p^{\text{vap}}$  for  $\text{H}_2\text{O}$

$$\rightarrow p_w = p_w^0 \times a_w ; \quad \ln a_w = \frac{1}{RT} \times \frac{\partial G}{\partial n_w}$$

$p^{\text{vap}}$  for  $\text{HNO}_3$

$$\rightarrow p_{\text{HNO}_3} = \frac{a_{\text{H}^+} a_{\text{NO}_3^-}}{K_H} ; \quad \ln a_{\text{HNO}_3^-} = \frac{1}{RT} \times \frac{\partial G}{\partial n_i}$$



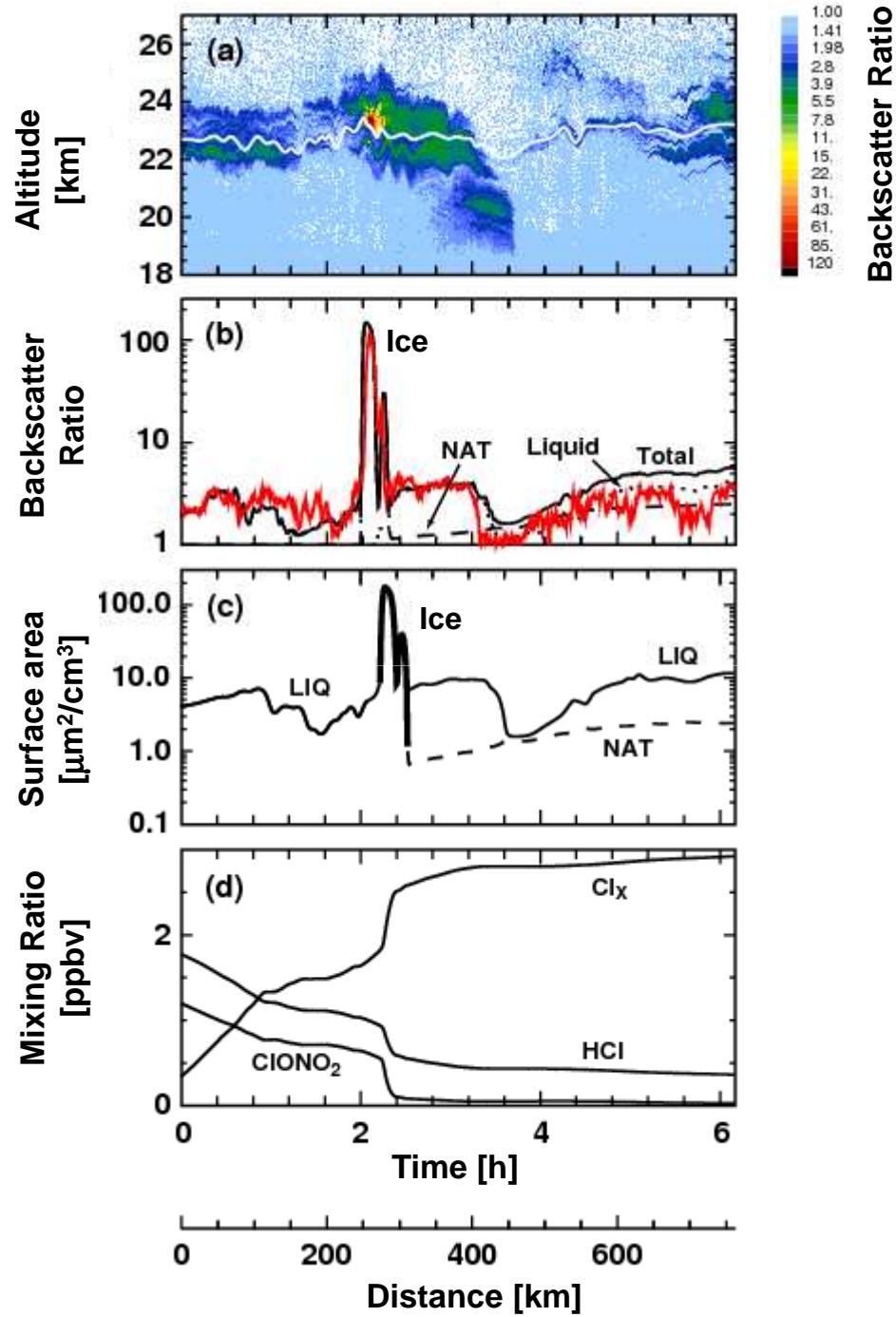
## Box modeling of PSCs

(a) Lidar backscatter ratio

(b) Backscatter along trajectory  
of ice, NAT and STS  
Red: measured, black: calc.

(c) Calculated surface area  
densities

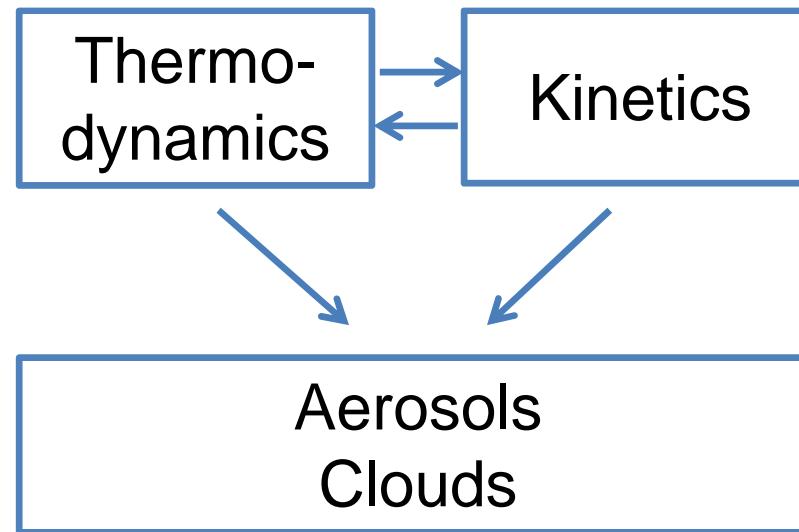
(d) Calculated chemical effects,  
mainly due to  
 $\text{HCl} + \text{ClONO}_2 \rightarrow \text{Cl}_2 + \text{HNO}_3$



**Formation of water clouds**

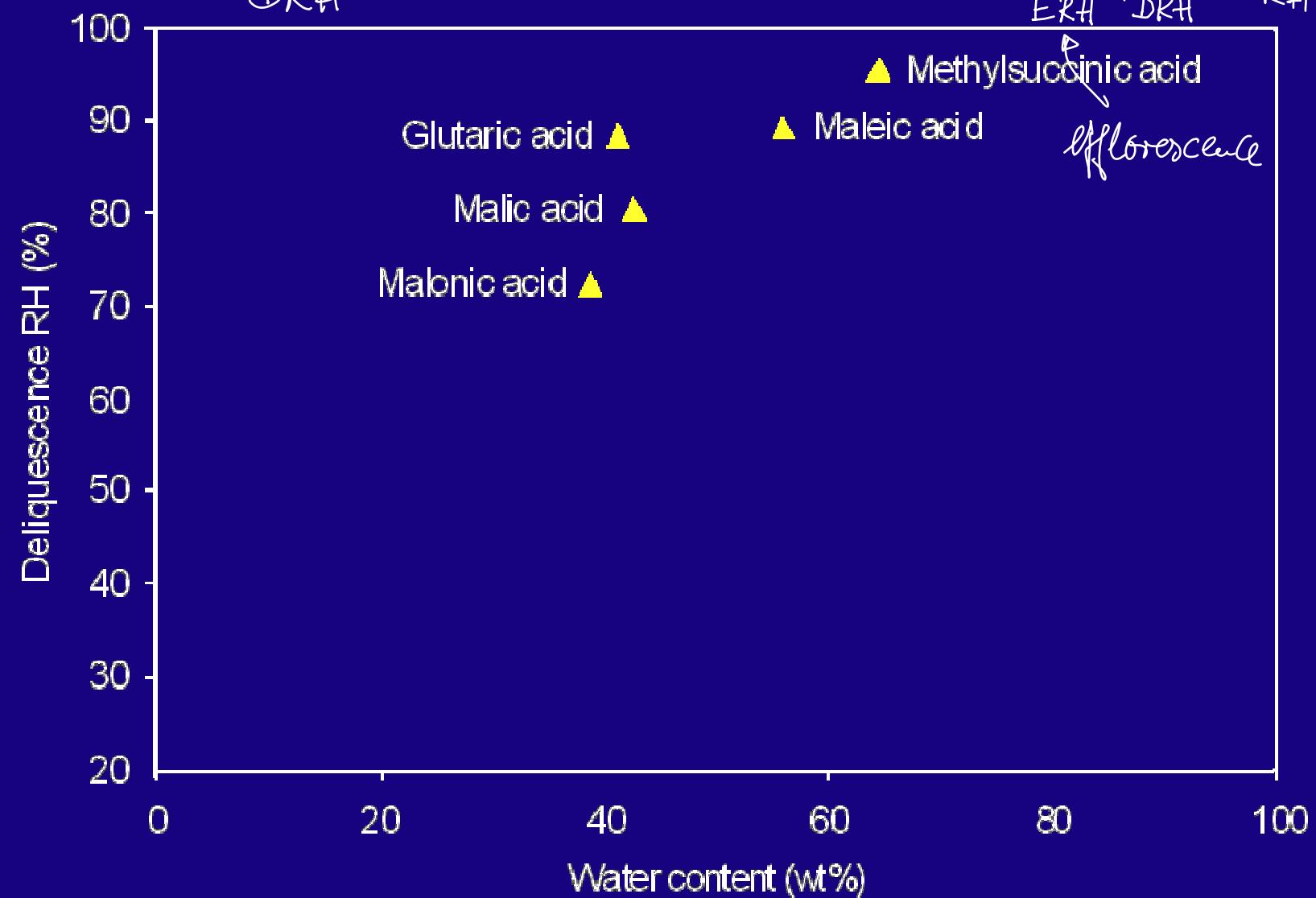
**Formation of Polar Stratospheric Clouds**

**Deliquescence of aerosols**



*How far do we get with thermodynamics in explaining cloud formation?*

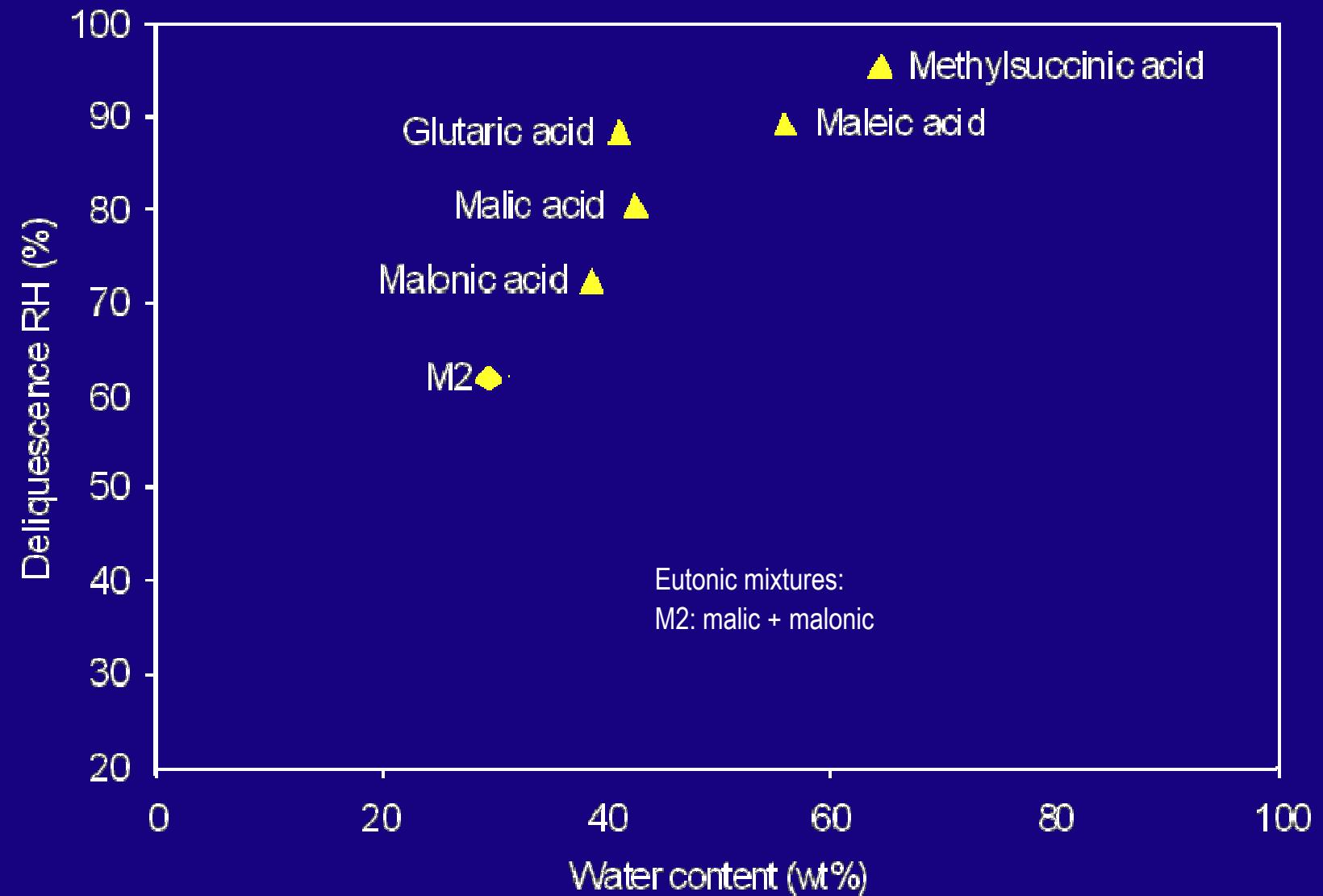
# Deliquescence RH of organic mixtures



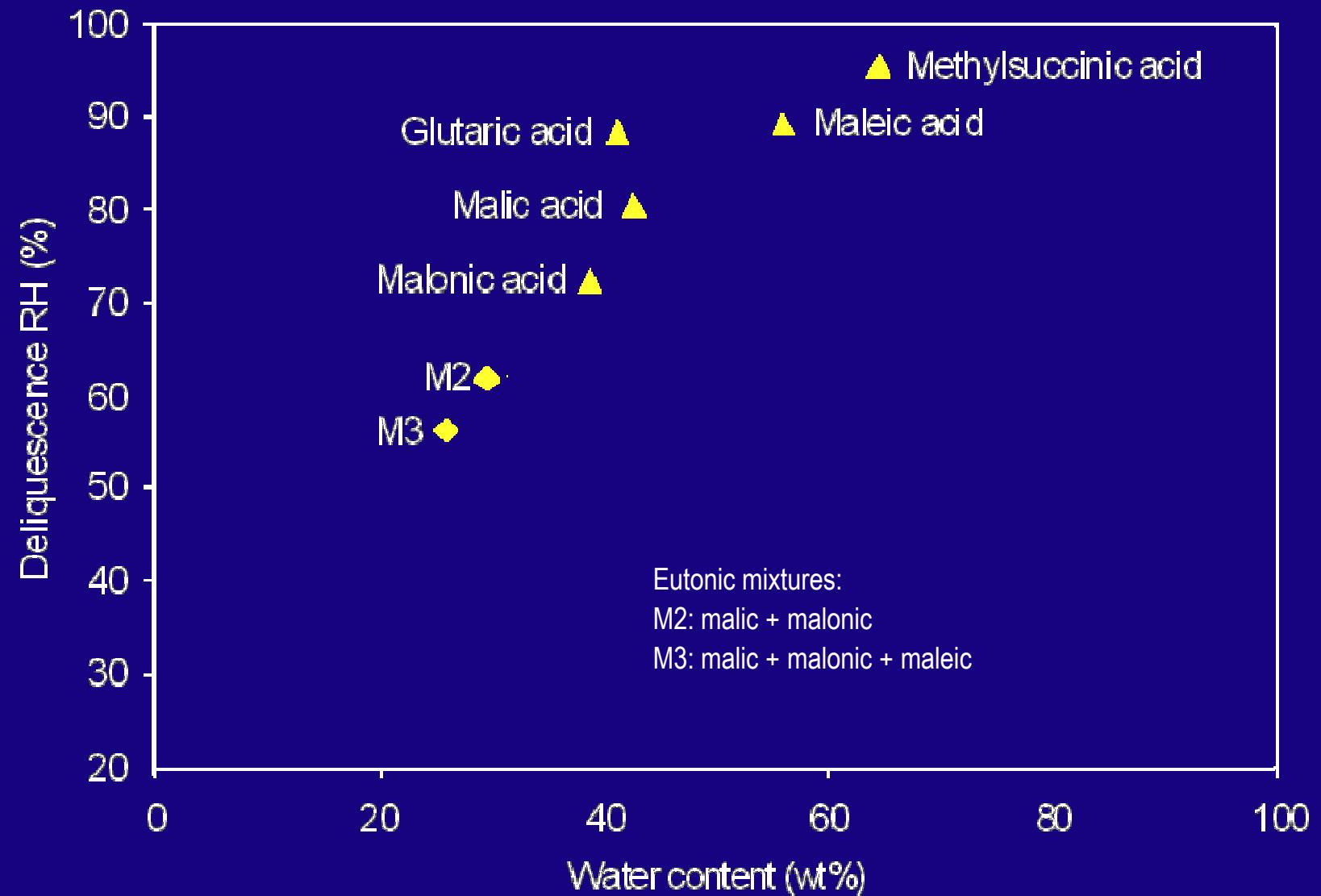
$T = 25^\circ\text{C}$

Marcolli et al. (2004)

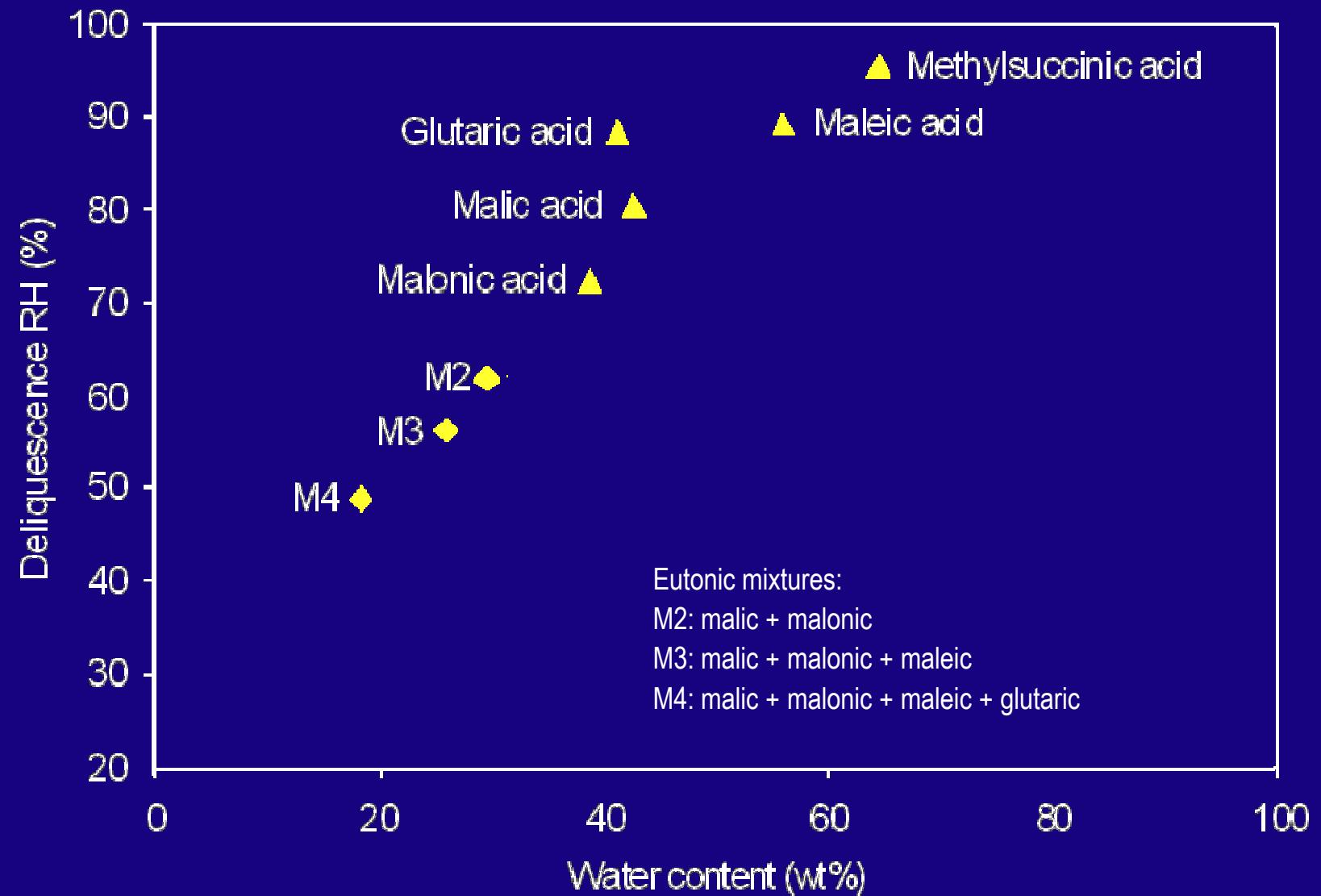
# Deliquescence RH of organic mixtures



# Deliquescence RH of organic mixtures



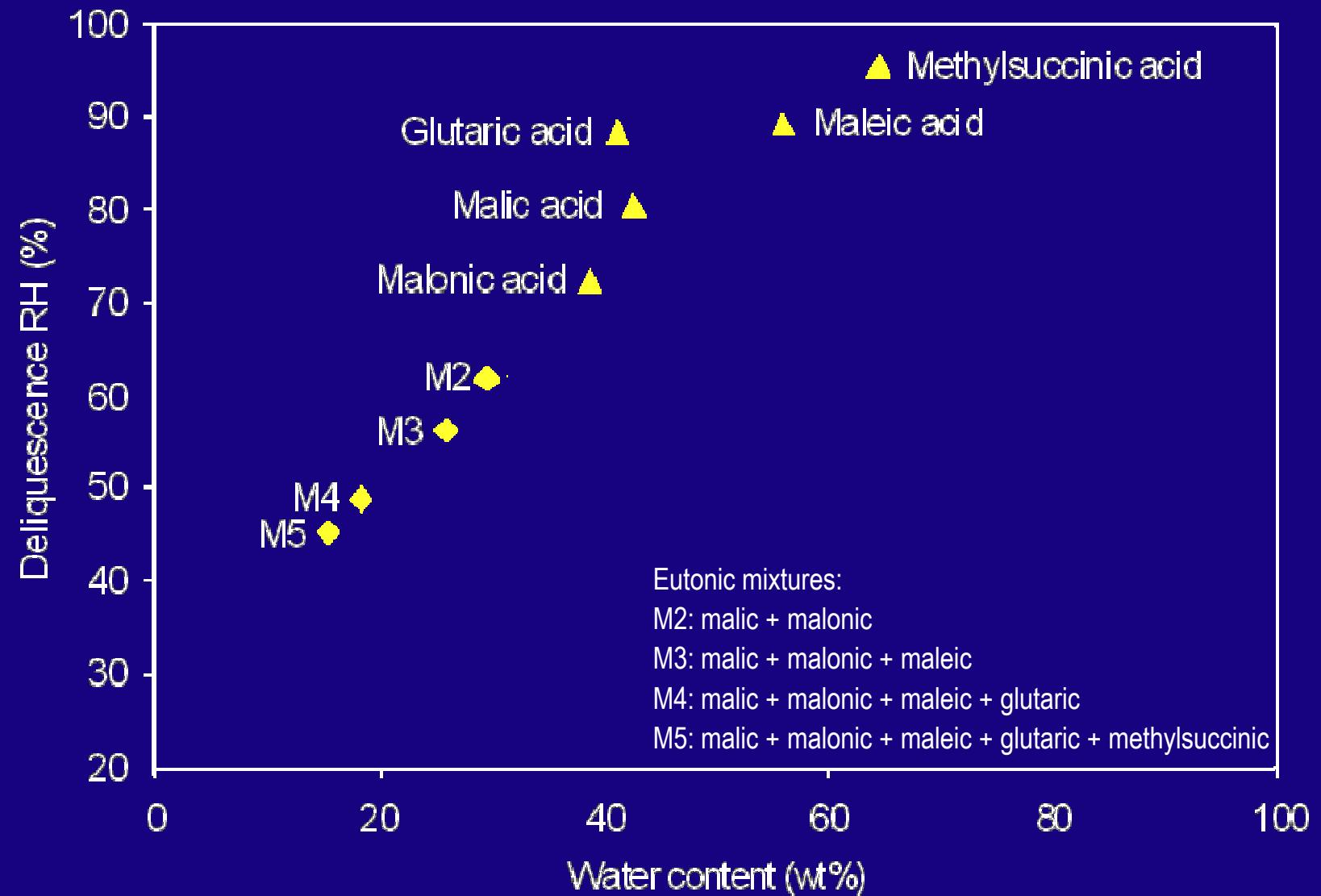
# Deliquescence RH of organic mixtures



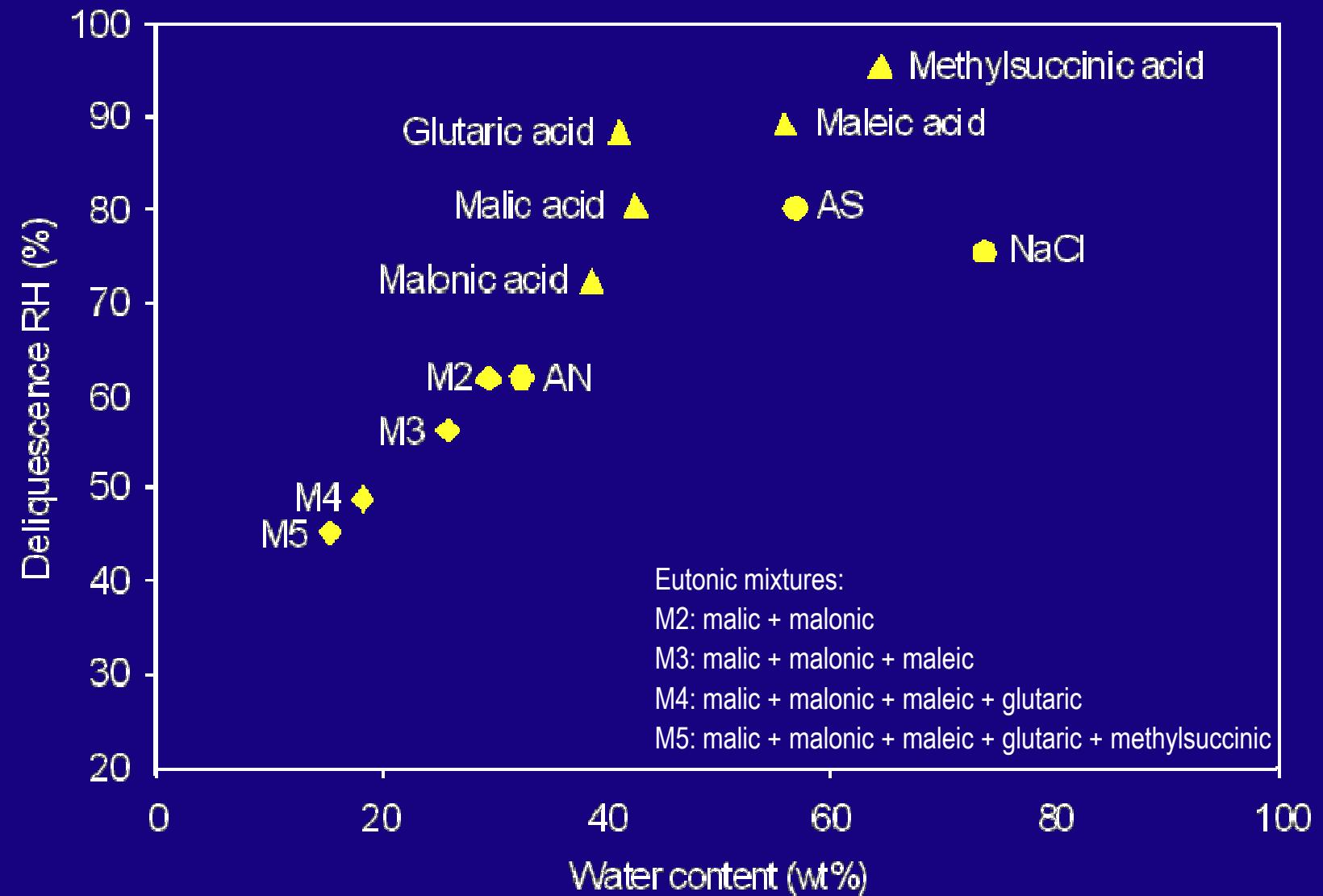
$T = 25^\circ\text{C}$

Marcolli et al. (2004)

# Deliquescence RH of organic mixtures



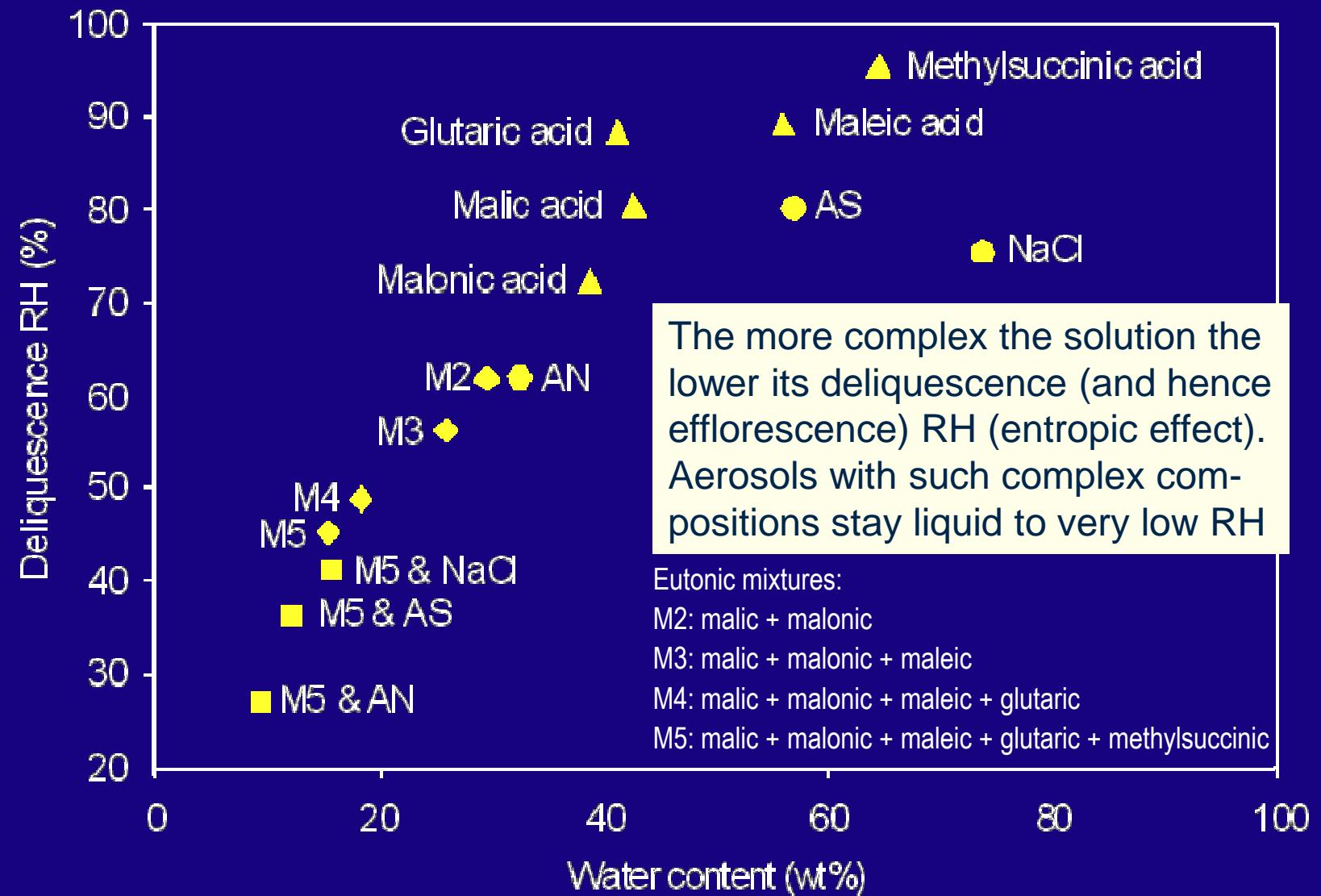
# Deliquescence RH of organic mixtures



$T = 25^\circ\text{C}$

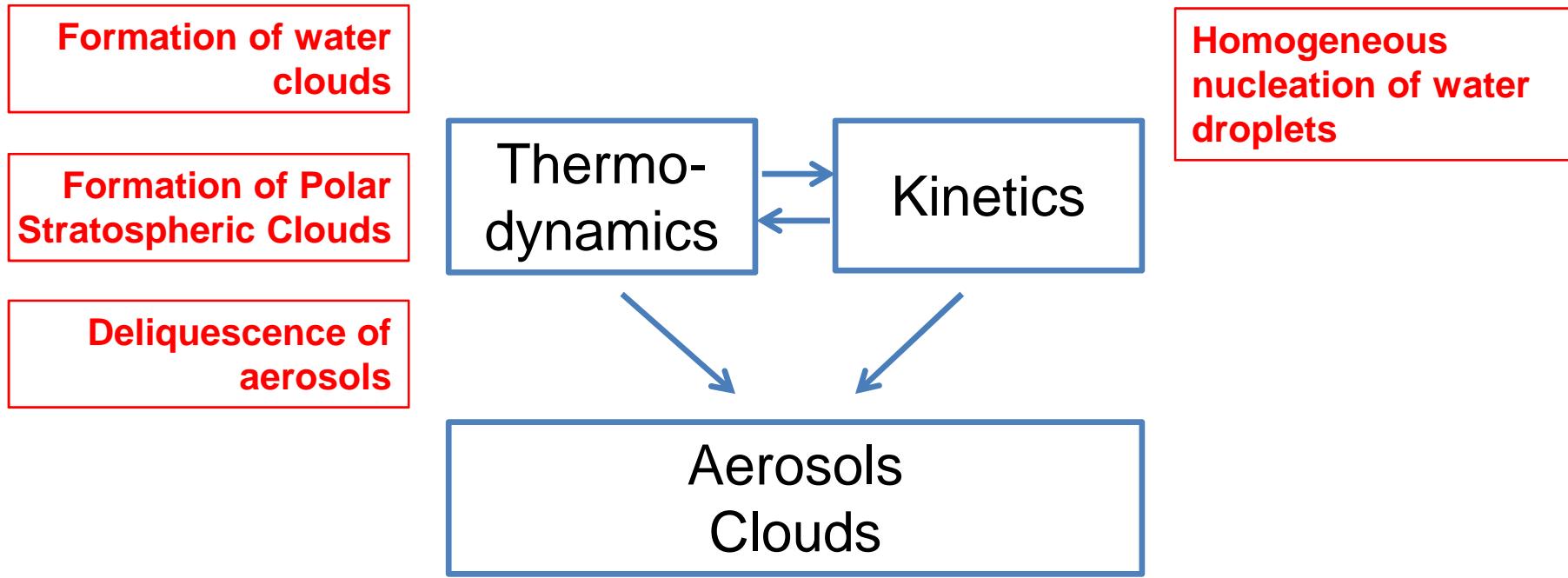
Marcolli et al. (2004)

# Deliquescence RH of organic mixtures



$T = 25^\circ\text{C}$

Marcolli et al. (2004)



*How far do we get with  
thermodynamics in explaining  
cloud formation?  
When do we need a kinetic  
treatment?*

# Nucleation

Formation of a critical cluster from a sequence of bimolecular additions:

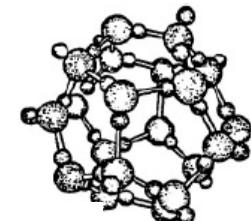


...

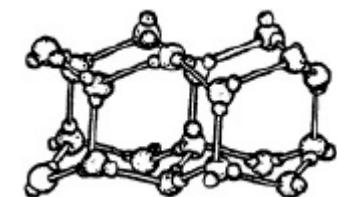


- supersaturation: necessary but not sufficient
- need to form new surface (Kelvin equation)
- need to overcome energy barrier by a critical cluster

molec  
dynami cs  
simulati on s



Clathrate structure



Ice -I<sub>h</sub> structure  
(Hale & Plummer, 1974)

**What energy is needed to form a critical cluster?**

**What is the size of the critical cluster?**

Excess free energy for cluster formation:  $\Delta G = \Delta G_S + \Delta G_V$

$\Delta G_S > 0 \rightarrow$  excess free energy required to form cluster surface (expense)

$\Delta G_V < 0 \rightarrow$  excess free energy released from volume transformation (gain)

# Nucleation: Classical Theory – a poor man's approach

$$\Delta G = \Delta G_s + \Delta G_v$$

$$= A\sigma - n\Delta\mu$$

$$= 4\pi r^2 \sigma - \frac{4\pi r^3}{3\nu_m} \Delta\mu$$

where

$$\Delta\mu = \mu_g - \mu_l = kT \ln \left( \frac{p}{p(\infty)} \right)$$

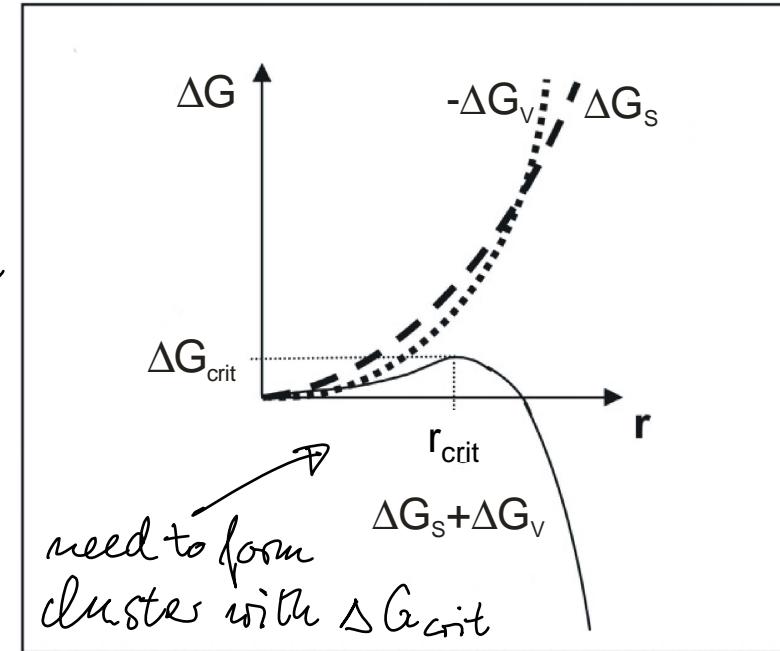
look for max ( $\Delta G$ )

→ Critical radius:

$$r_c = \frac{2\sigma\nu_m}{\Delta\mu}$$

→ Critical energy (barrier):

$$\begin{aligned} \Delta G_{crit} &= \frac{16\pi\sigma^3\nu_m^2}{(\Delta\mu)^2} - \frac{32\pi\sigma^3\nu_m^2}{3(\Delta\mu)^2} \\ &= \frac{16\pi\sigma^3\nu_m^2}{3(\Delta\mu)^2} = \frac{16\pi\sigma^3\nu_m^2}{3k^2T^2(\ln(p/p(\infty))^2)} \end{aligned}$$



Assumptions?

$\sigma$  = surface tension

$\nu_m$  = molar volume

$p(\infty)$  = flat surface vapor pressure

} from bulk

If we assume an **Arrhenius reaction velocity equation** commonly used for the rate of a thermally activated process, the rate of nucleation,  $J$ , is given as:

$$J = K \exp\left(-\frac{\Delta G_{crit}}{kT}\right) = K \exp\left(-\frac{16\pi\sigma^3 v_m^2}{3k^2 T^2 (\ln(p/p(\infty))^2)}\right)$$

Obtain prefactor  $K$  from kinetic collision frequency:

$$K = \left(\frac{2\sigma}{\pi m_m}\right)^{1/2} \frac{v_m N_v^2}{S}$$

$m_m$ : molecular mass  
 $N_v$ : vapor concentration

$1 \text{ \AA} = 0.1 \text{ nm}$

Example: critical radius, number, and nucleation rate for water droplets at 298 K

$p/p(\infty)$	$r_c (\text{\AA})$	$i_c = \frac{\# \text{ molec}}{\text{cluster}}$	$J (\text{cm}^{-3}\text{s}^{-1})$
1	$\infty$	$\infty$	$-\infty$
2	15.1	482	$1.3 \times 10^{-47}$
3	9.5	121	$8.9 \times 10^{-4}$
4	7.6	60	$6.4 \times 10^{+7}$
5	6.5	39	$3.8 \times 10^{+11}$

$\left. \begin{array}{l} \text{no nucleation} \\ \text{switch on mud.} \end{array} \right\}$

$$\sigma = 0.072 \text{ N/m}; v_m = 2.99 \times 10^{-29} \text{ m}^3; m_m = 2.99 \times 10^{-26} \text{ kg}$$

# Experiments on homogeneous nucleation from vapors by a nucleation pulse method

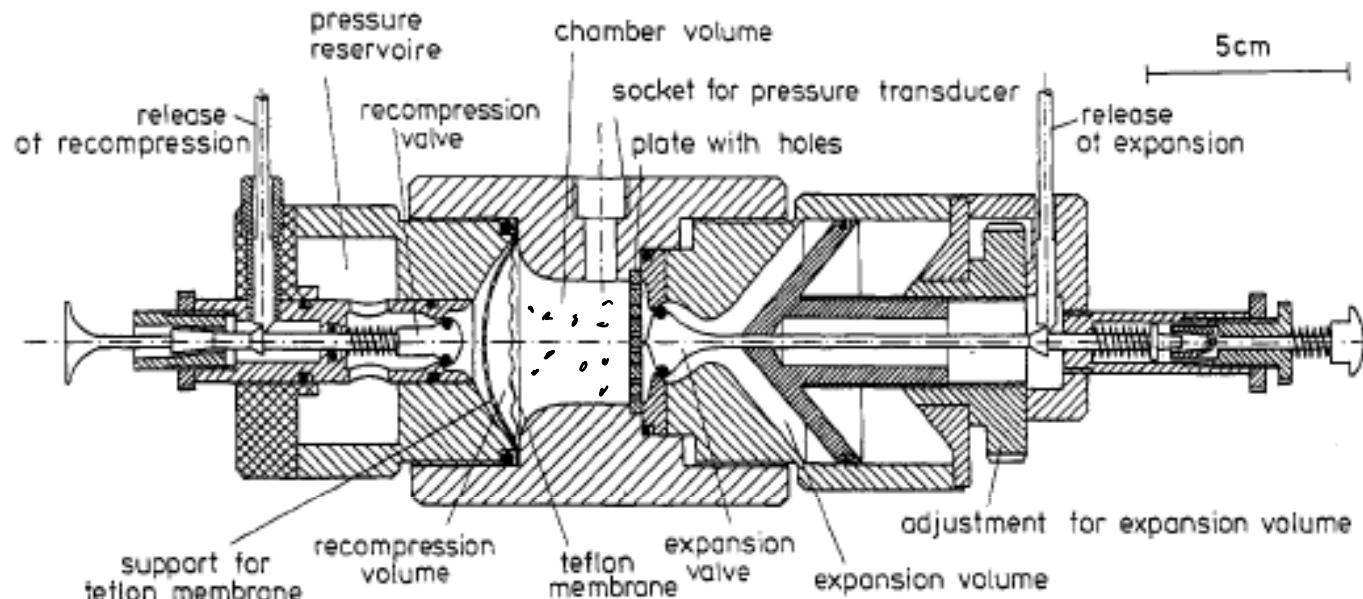
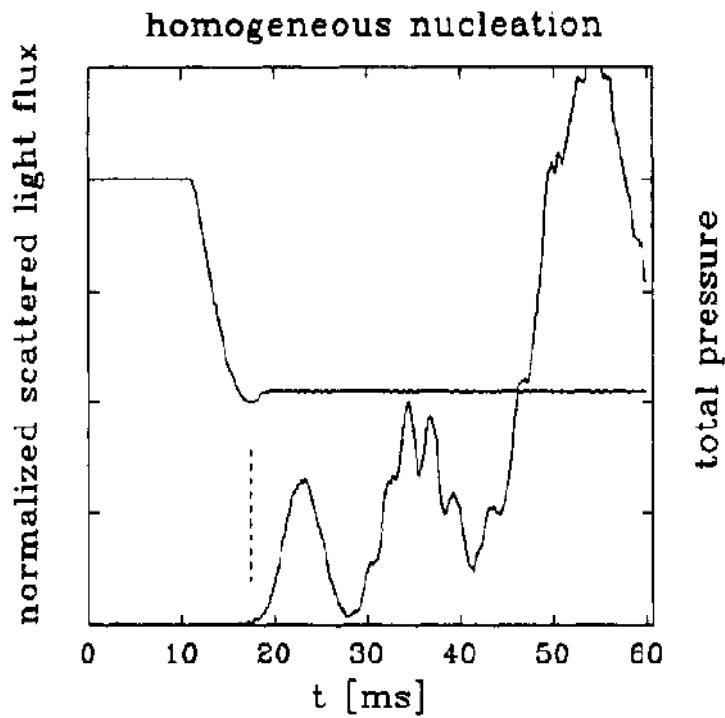


Figure 2. Cross section of the expansion chamber showing the main design features to scale. Expansion and recompression valve are released by a rotating-trigger unit in a well-defined time sequence.

- Premixed vapor and carrier gas (Xe, Kr, Ar, Ne or He)
- Expansion is held for  $t_{exp}$  (a few ms)
- Small recompression to quench further nucleation  
→ nuclei can grow into droplets of observable size ( $\mu\text{m}$ )
- Number density  $C$  of the droplets obtained from scattered light  
→  $J = C / t_{exp}$

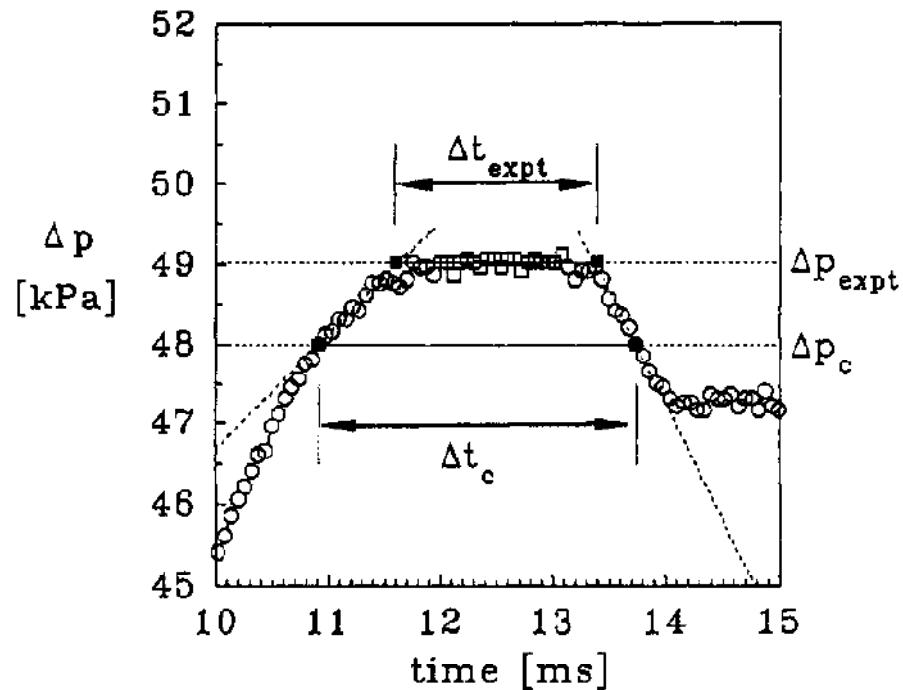
tiny particles  
not visible



### Homogeneous nucleation exp.:

$p_{tot}$  and scattered light flux,  $\theta = 15^\circ$

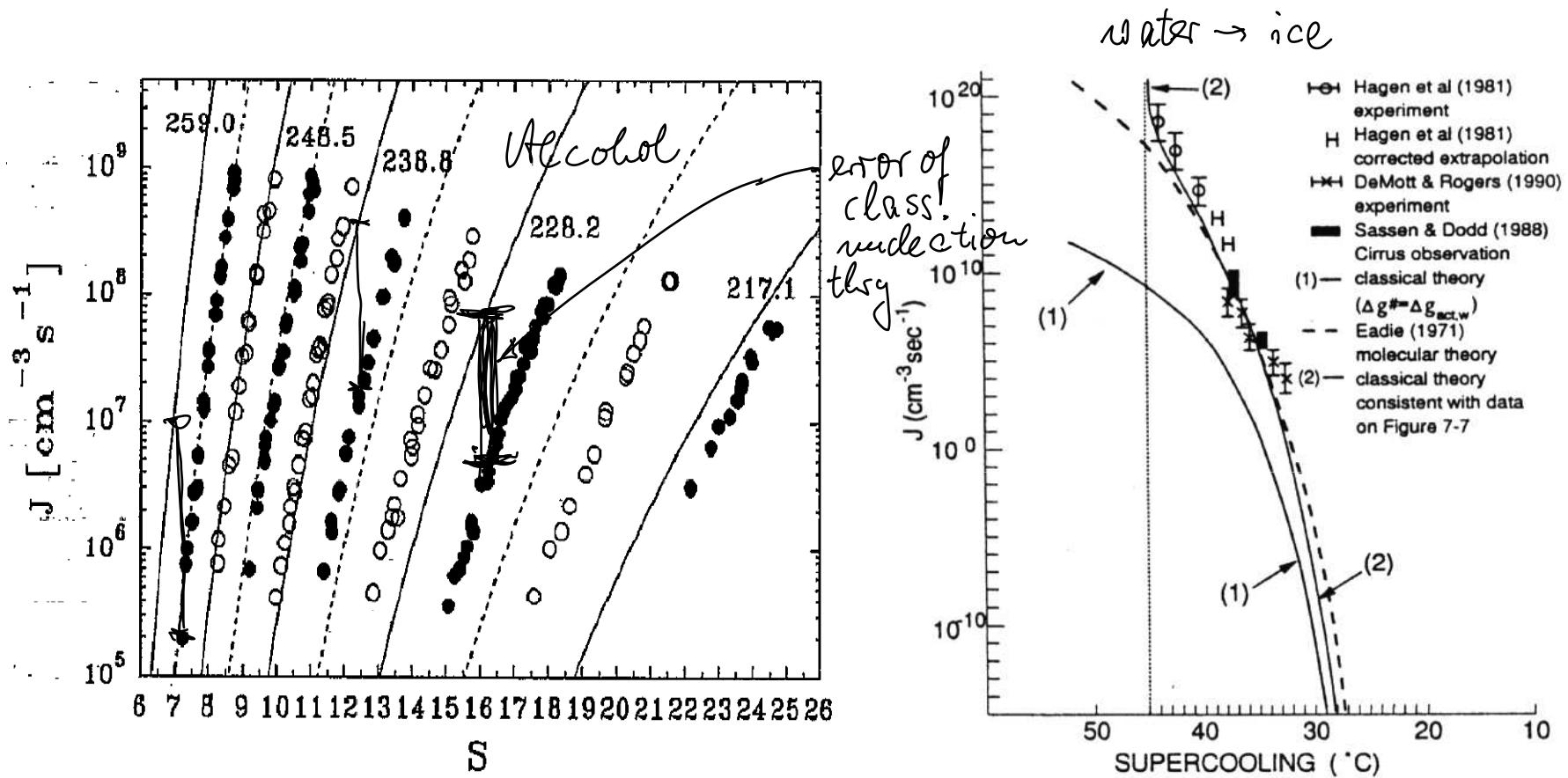
Significant light scattering occurs only **after** the nucleation pulse



### Nucleation pulse:

Obtain experimental pressure drop  $\Delta p_{expt}$  and duration  $\Delta t_{expt}$  of the nucleation pulse

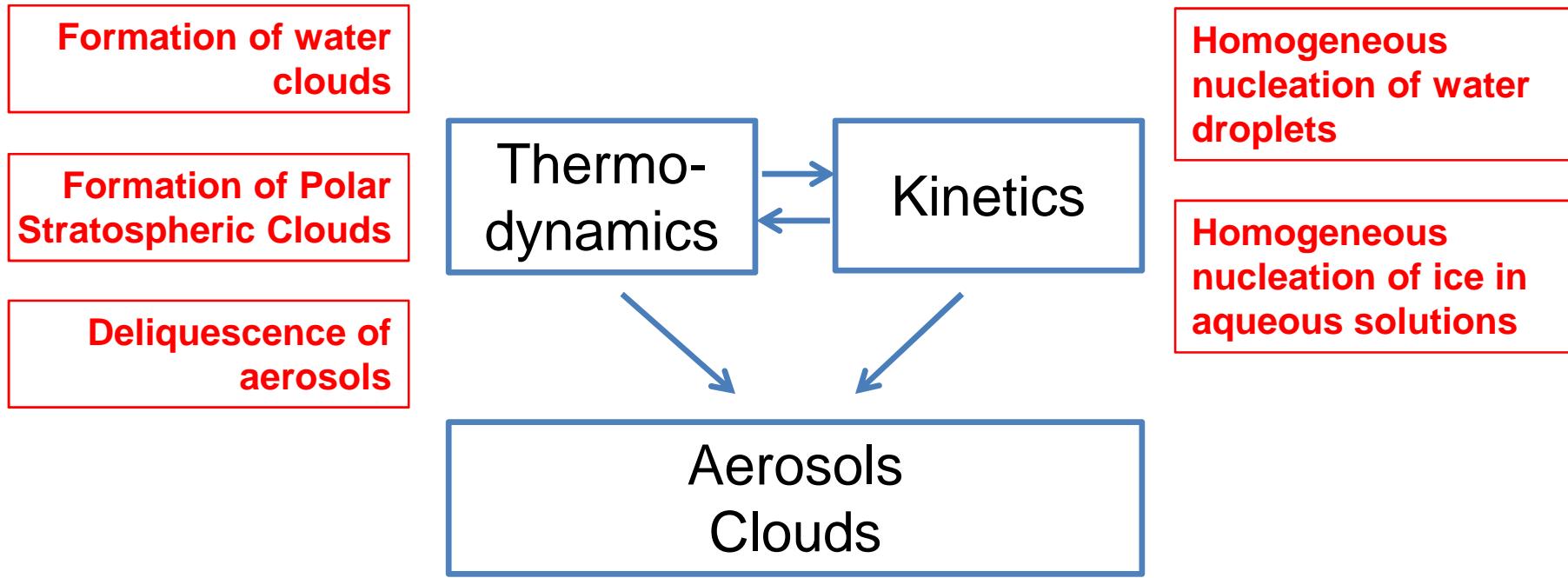
## Homogeneous nucleation rates for water: gas-to-liquid and liquid-to-solid



Nucleation rate measurements and classical (Becker-Döring) theory (Viisanen et al., J. Chem. Phys., 1993).

Solid lines belong to solid points.

Variation of the rate of homogeneous ice nucleation in supercooled water (from Pruppacher and Klett, Kluwer, 1997).



*How far do we get with  
thermodynamics in explaining  
cloud formation?  
When do we need a kinetic  
treatment?*

# Homogeneous ice nucleation

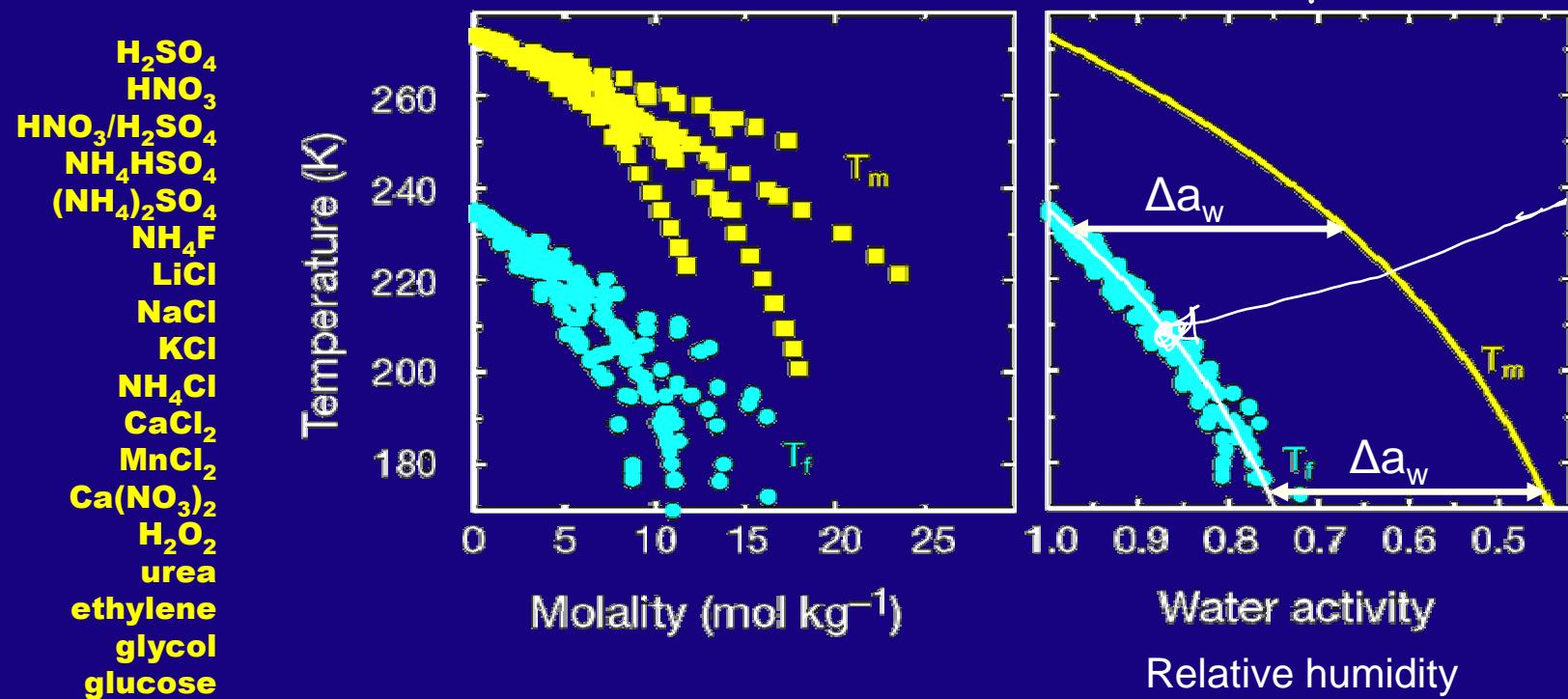
A quantitative thermodynamic ice freezing theory  
 Koop et al., Nature 2000

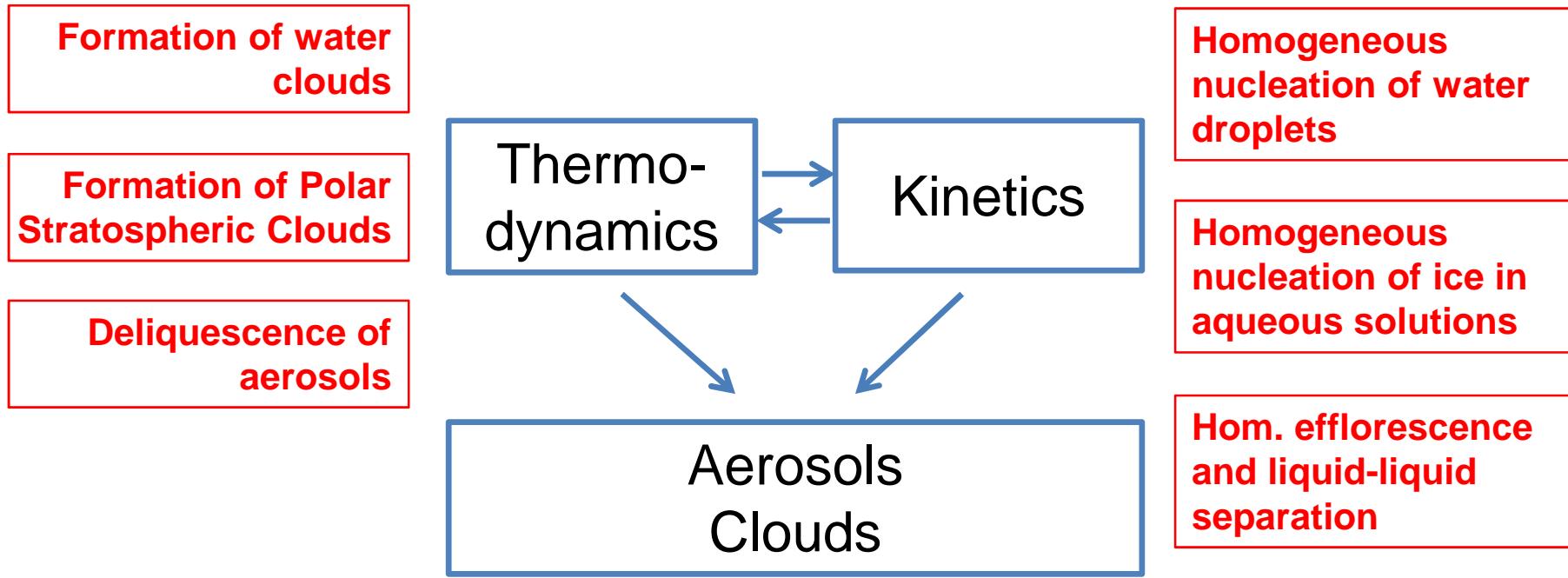
Unifies freezing nucleation temperatures and rates for  
 18 different aqueous solutions:

$$P_w = P_w^o a_w$$

$$a_w = \frac{1}{RT} \frac{\partial G}{\partial n_w}$$

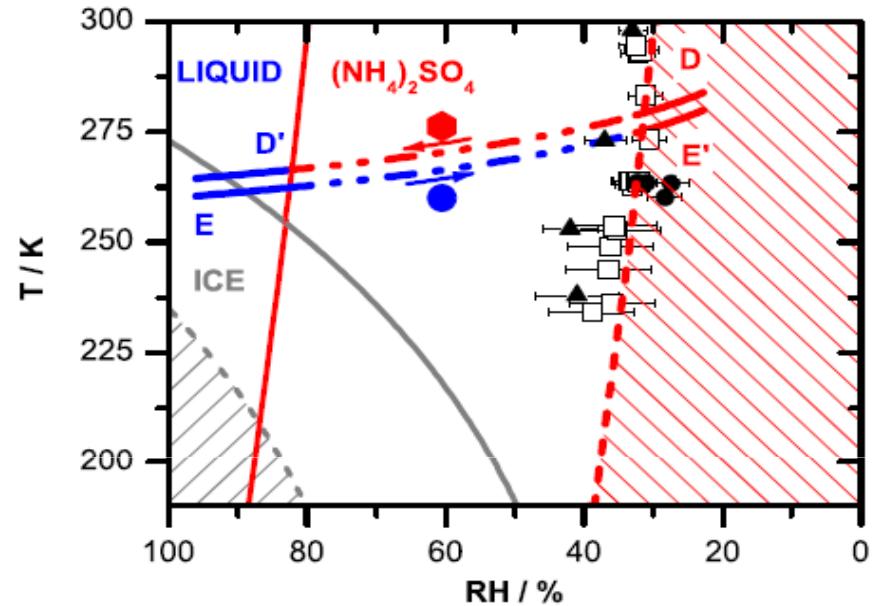
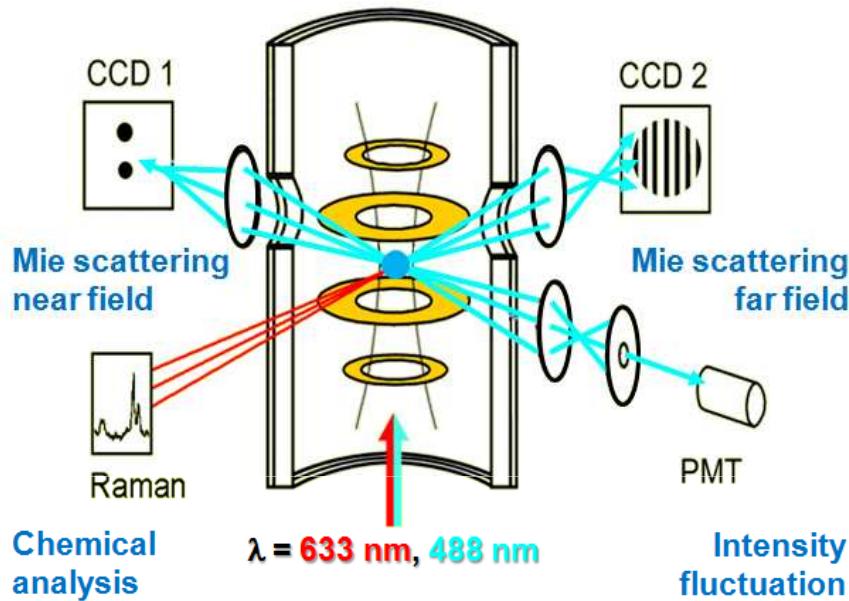
$$a_w^{\text{liq}} \approx \frac{P_w}{P_w^o} \stackrel{\Sigma q}{=} R \Delta H_{f,i,s}$$





*How far do we get with thermodynamics in explaining cloud formation?  
When do we need a kinetic treatment?*

# Deliquescence/efflorescence of aerosol particles

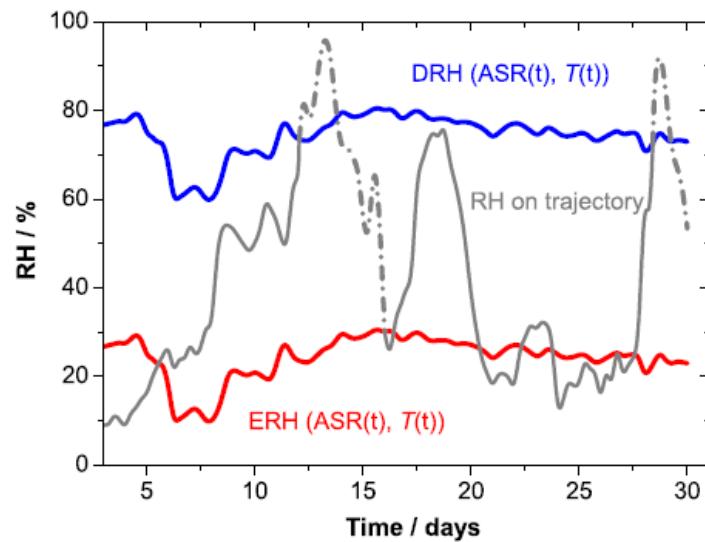


## Electrodynamic particle trap

- store single micron-sized particle
- air flow with controlled RH (5-95 %)
- air flow with controlled  $T$  (160-310 K)
- multiple spectroscopic analysis methods

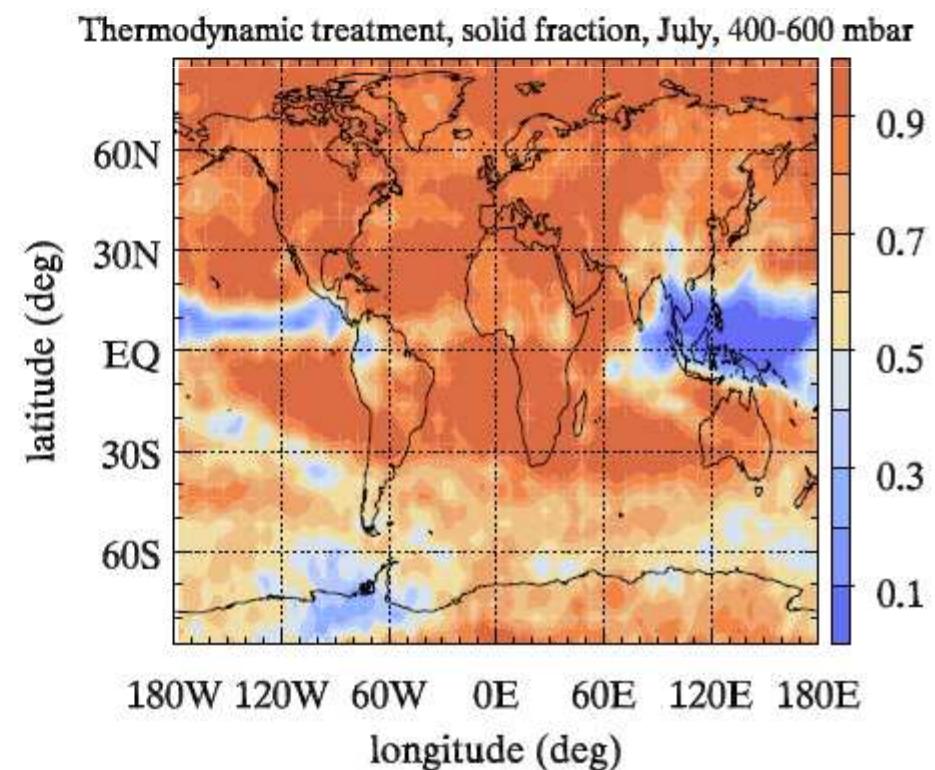
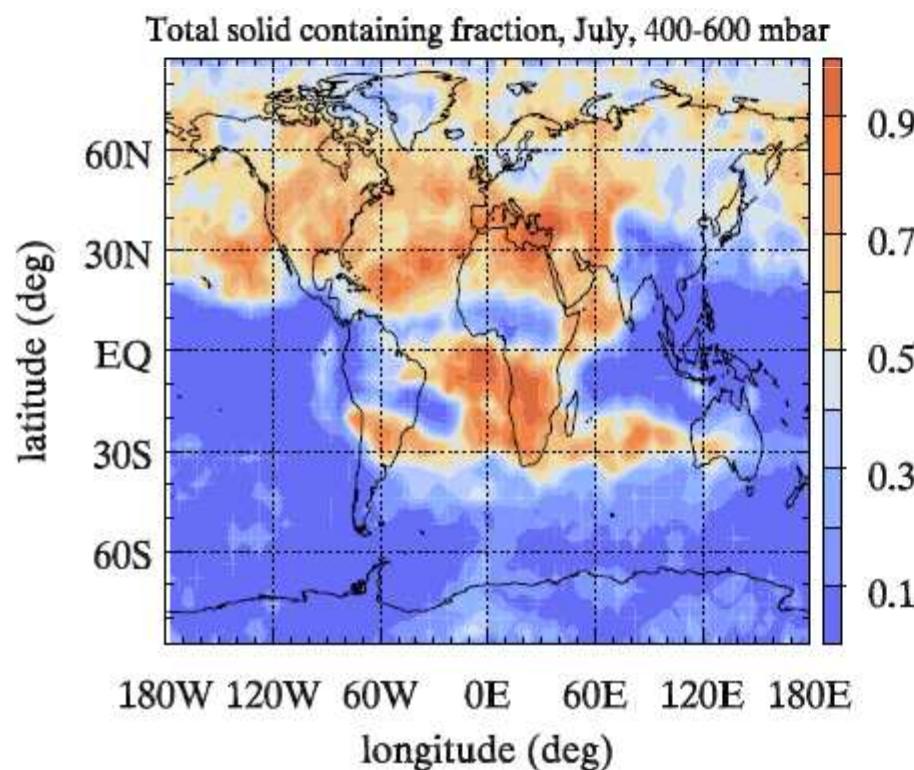
## Efflorescence measurements

- here (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> (sulfate) particle
- also NH<sub>4</sub>HSO<sub>4</sub> (bisulfate)
- and (NH<sub>4</sub>)<sub>3</sub>H(SO<sub>4</sub>)<sub>2</sub> (letovicite)



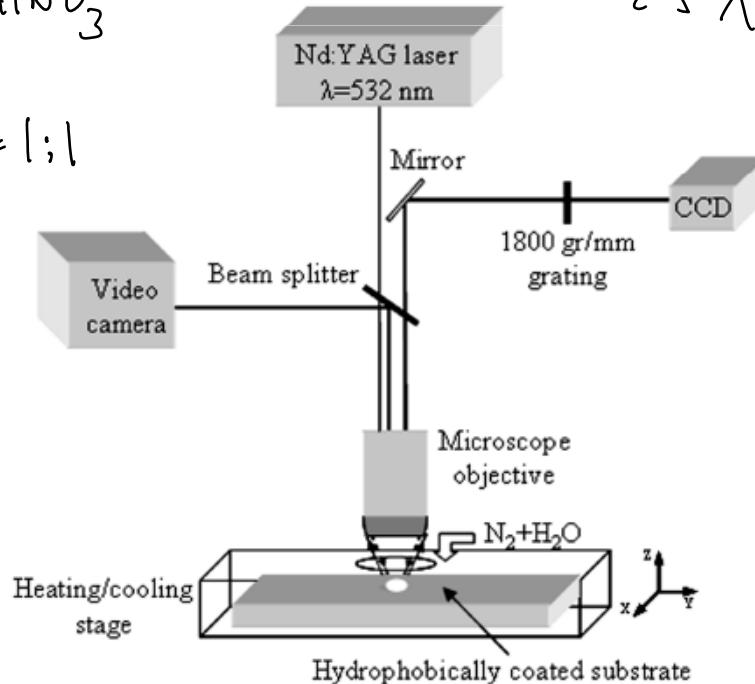
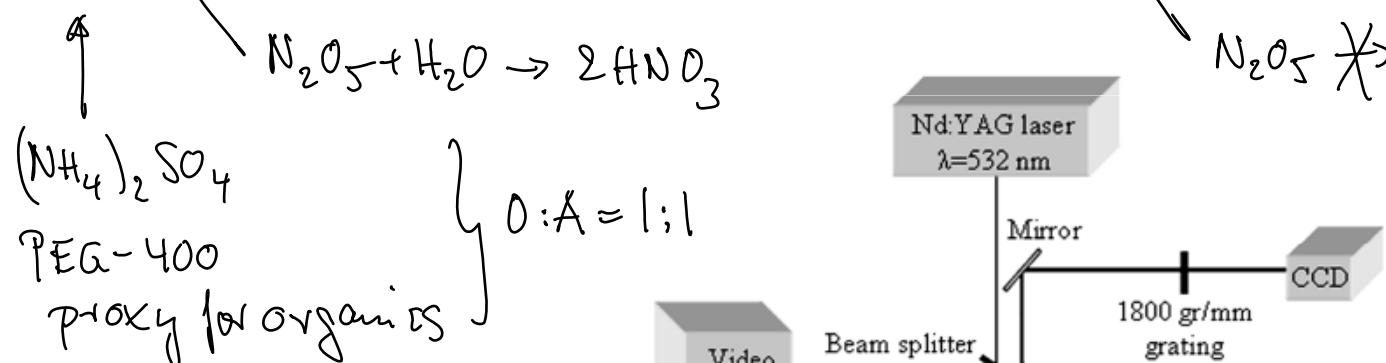
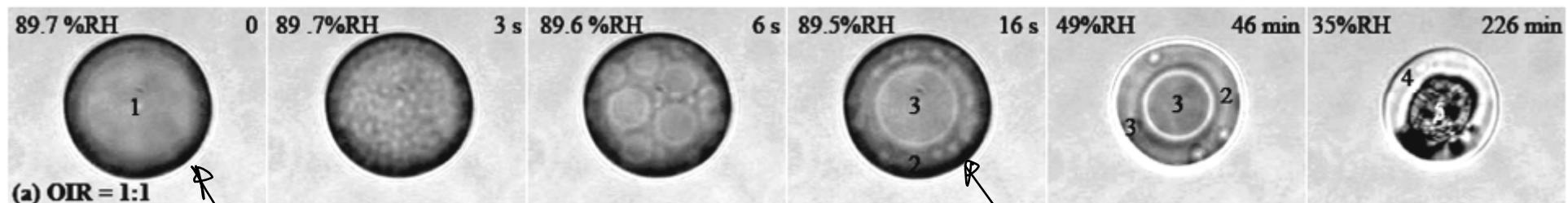
## $\text{NH}_4^+/\text{HSO}_4^-/\text{SO}_4^{2-}/\text{H}_2\text{O}$ hysteresis (measured in trap)

Trajectory-based global analysis  
(Colberg et al., 2003):  
left: full account for hysteresis  
right: allow efflorescence w/o supersaturation



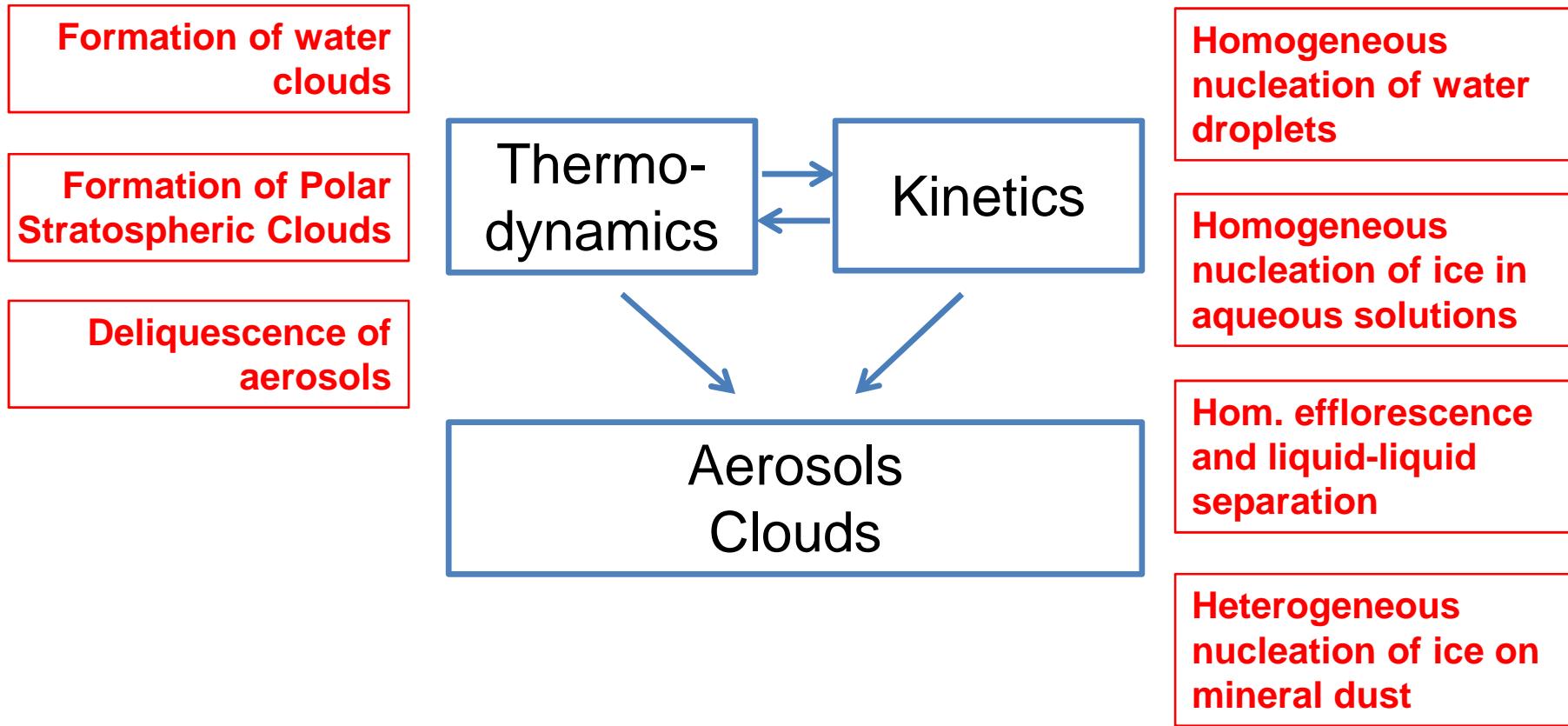
# Thermodynamic properties of aerosols

- evidence for prevalence of liquid organic aerosols
- evidence for liquid-liquid phase separations



Raman microscope:

Ciołkun  
et al.  
JPC 2009

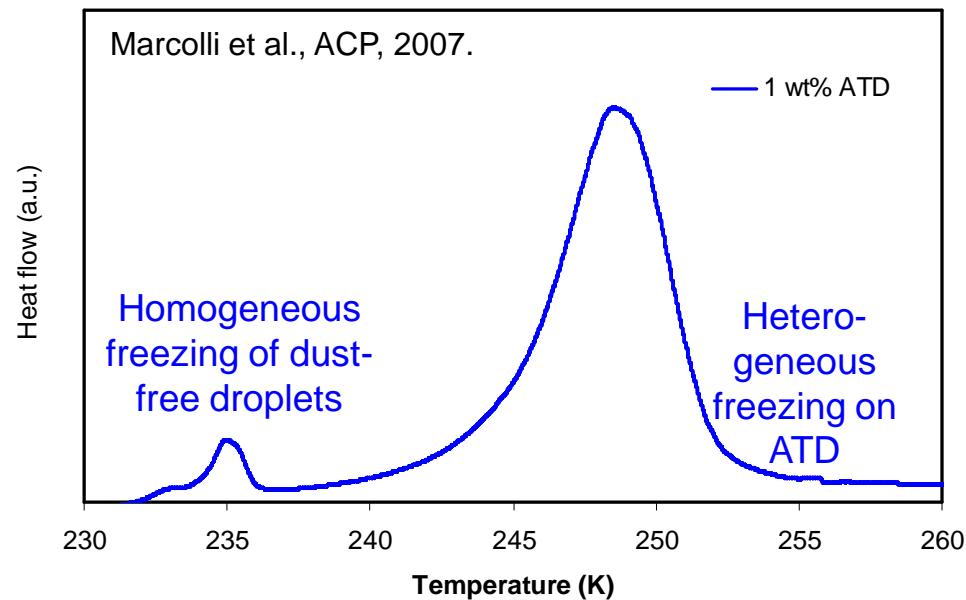


*How far do we get with  
thermodynamics in explaining  
cloud formation?*

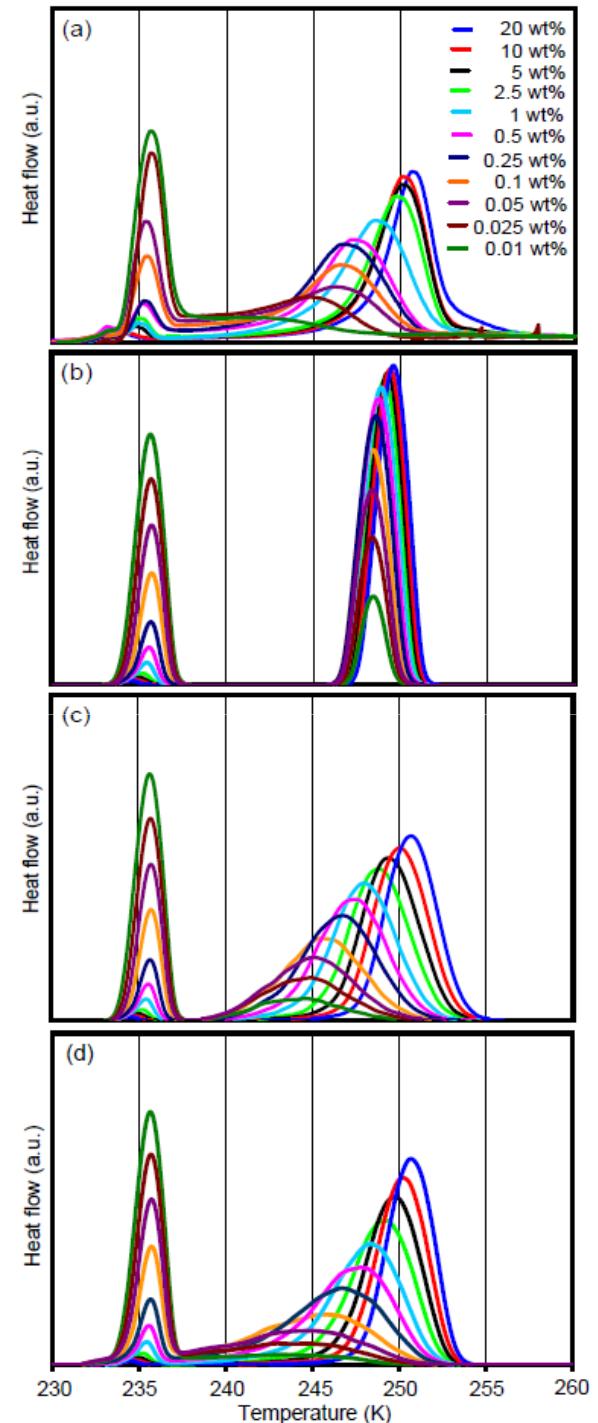
*When do we need a kinetic  
treatment?*

# Heterogeneous nucleation on Arizona test dust (ATD): A first active-site-attribution approach

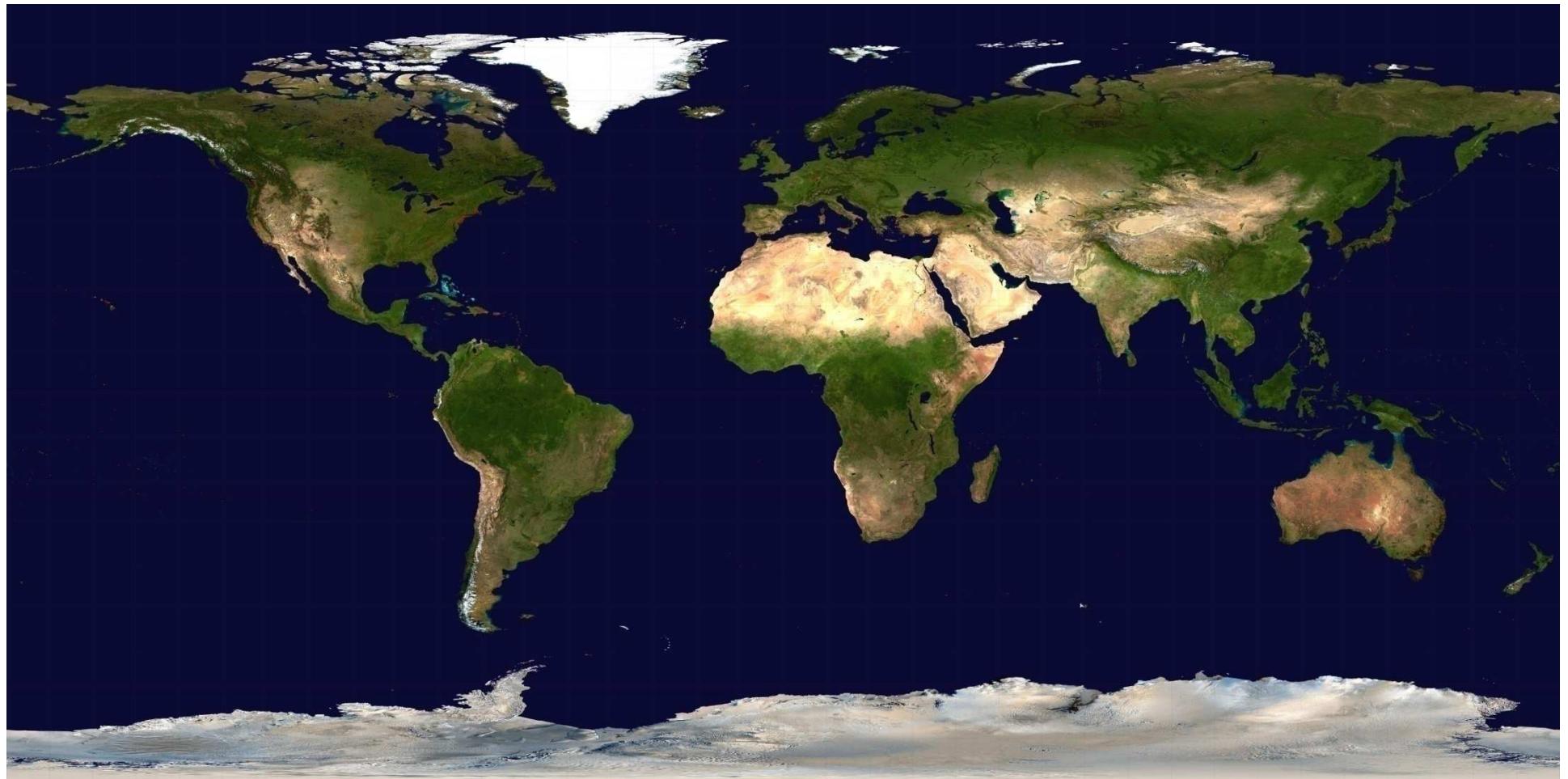
→ Differential Scanning Spectroscopy  
DSC expt on emulsified aqueous suspension of ATD (1 wt%)



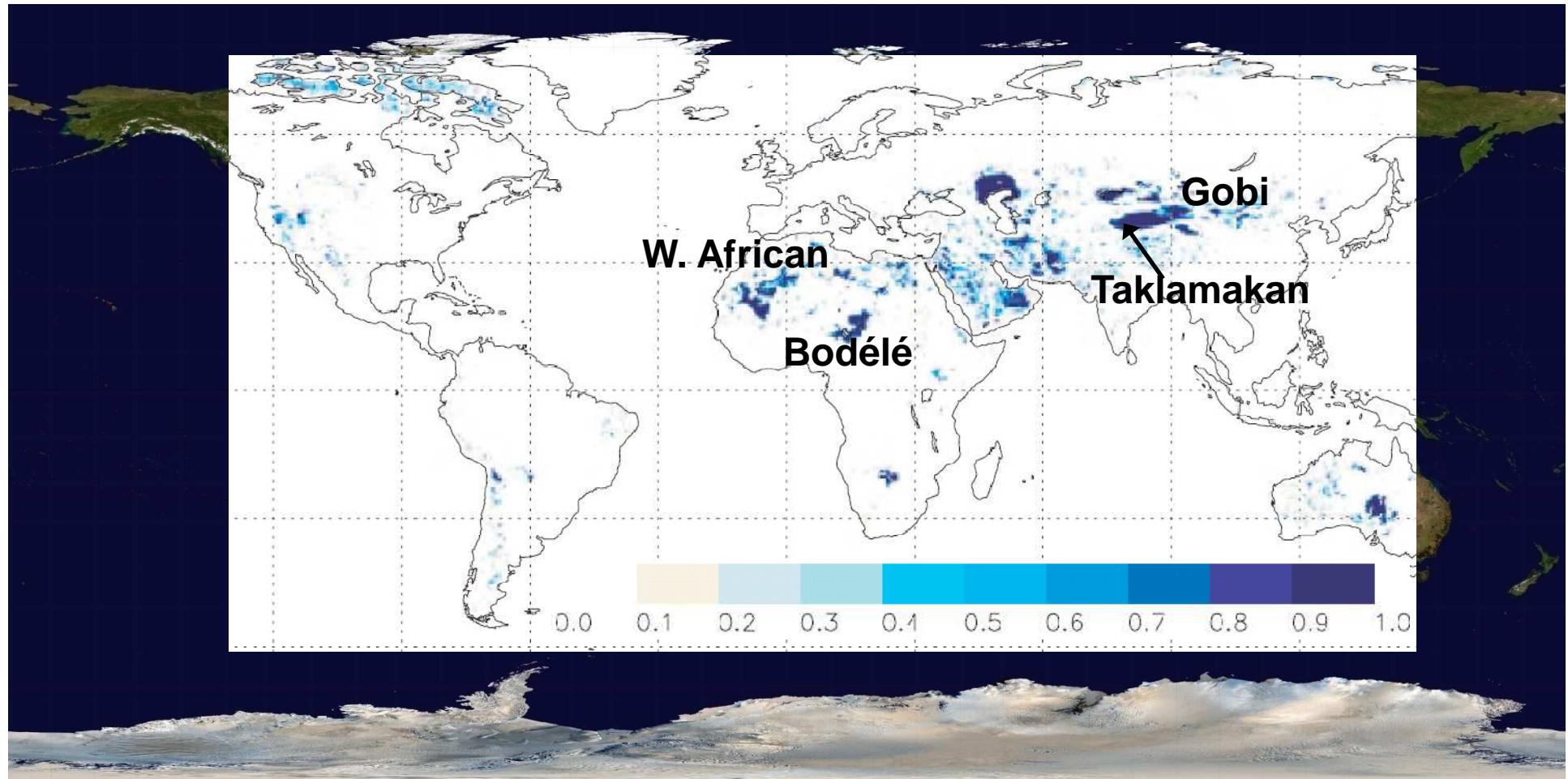
- (a) DSC experiments on an emulsified ATD suspension →
  - (b) Assuming all ATD particles to have the same active site
  - (c) Attributing stochastically a single active site per ATD ptcl
  - (d) Active site distribution on each ATD particle
- More realistic dusts than ATD: Pinti et al.



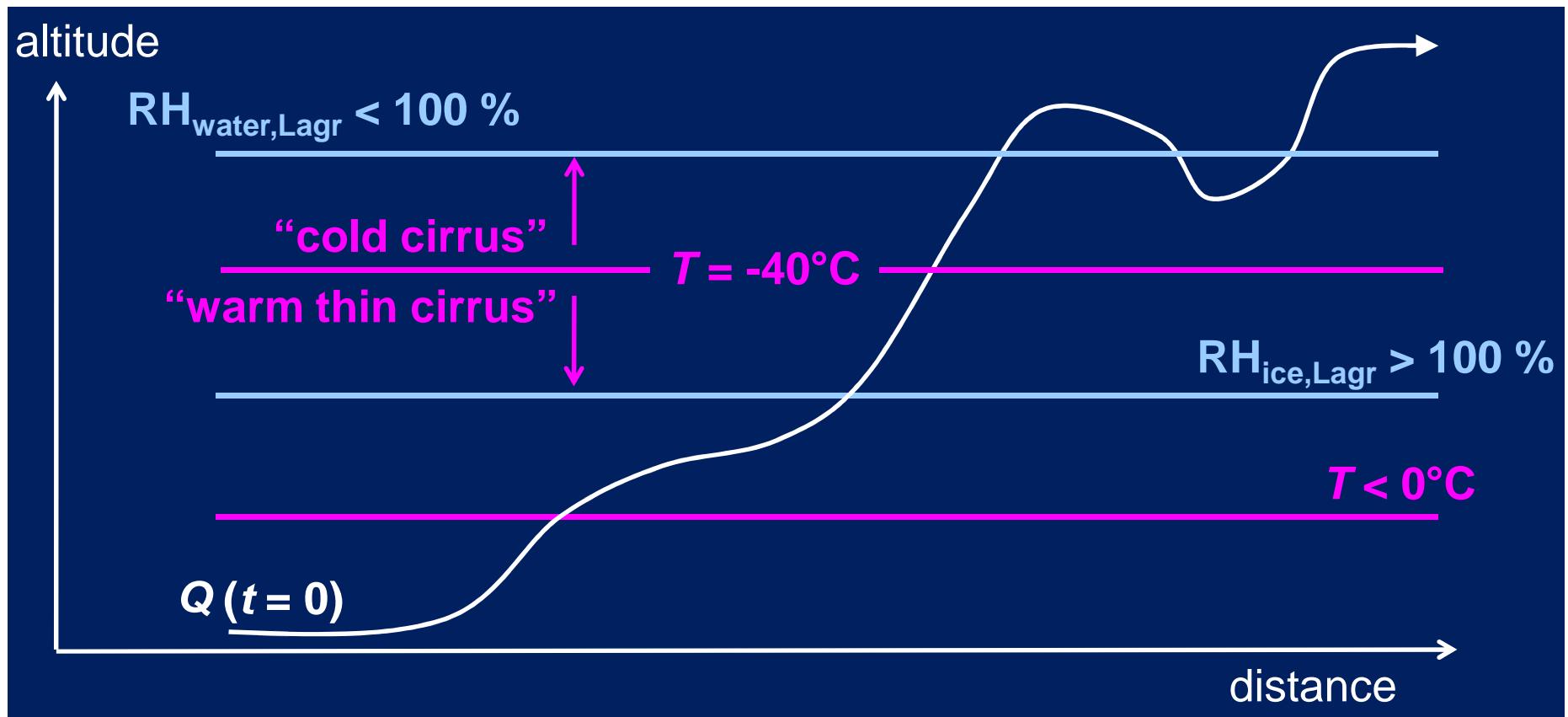
# Where does mineral dust come from?



# Location of preferential dust sources

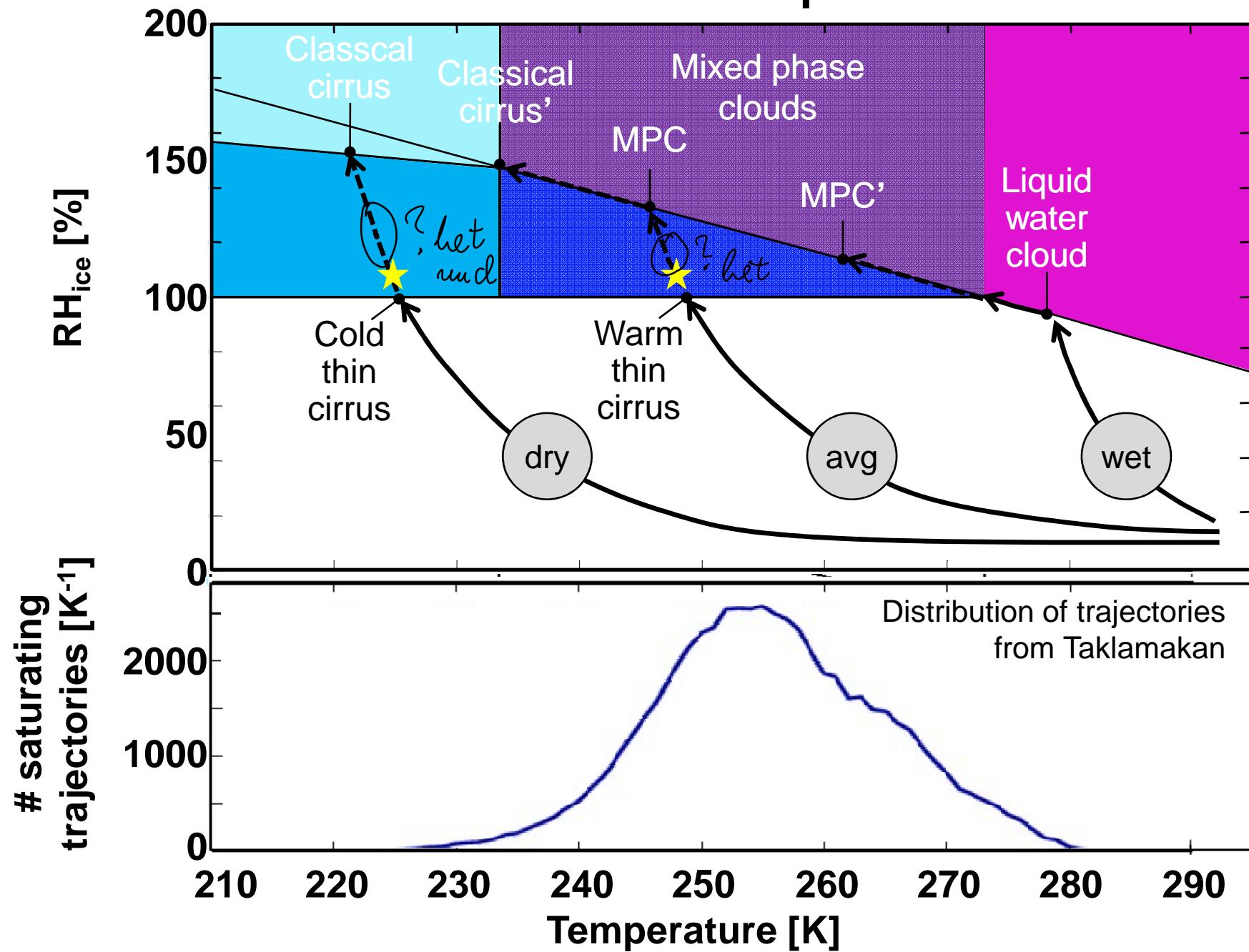


# Lagrangian tracing of $\text{RH}_{\text{ice}}$

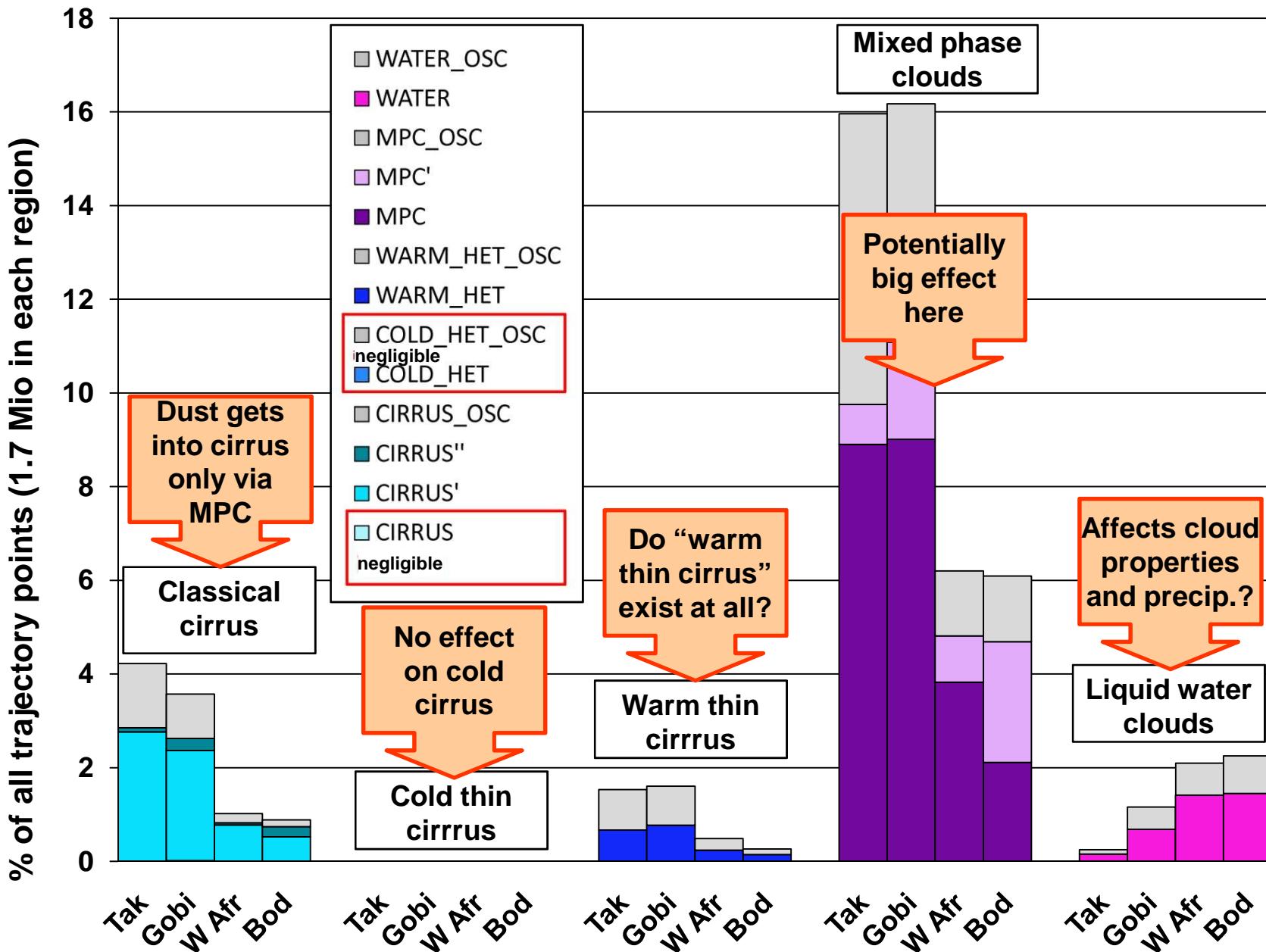


Transported specific humidity ( $Q$ ) at beginning of each trajectory ( $t = 0$ )  
No condensation and mixing → trace  $Q$  only up to  $\text{RH}_w \leq 100\%$   
Checked ECMWF's  $T(t = 0)$  and  $Q(t = 0)$  are realistic

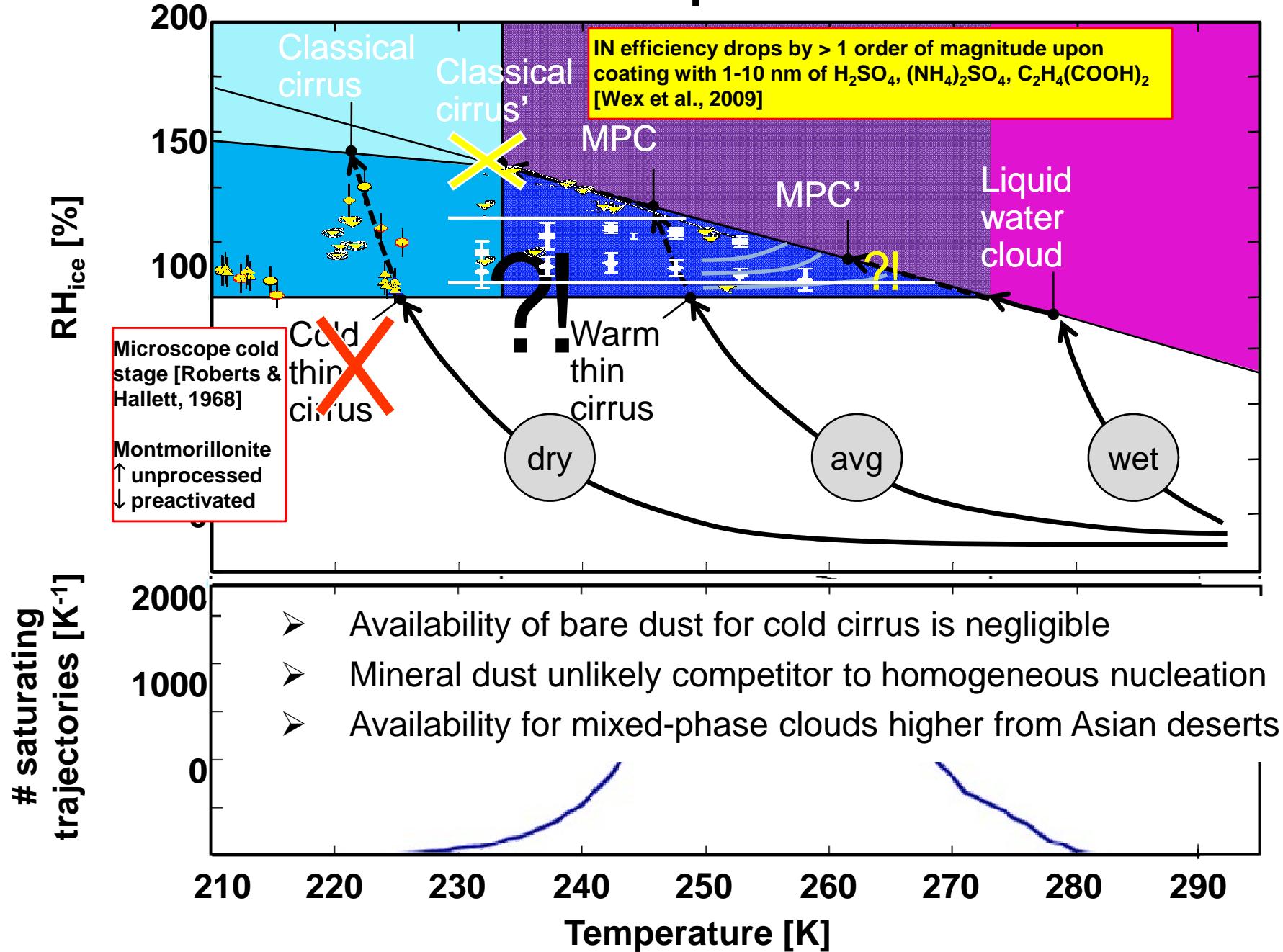
# Cloud formation processes

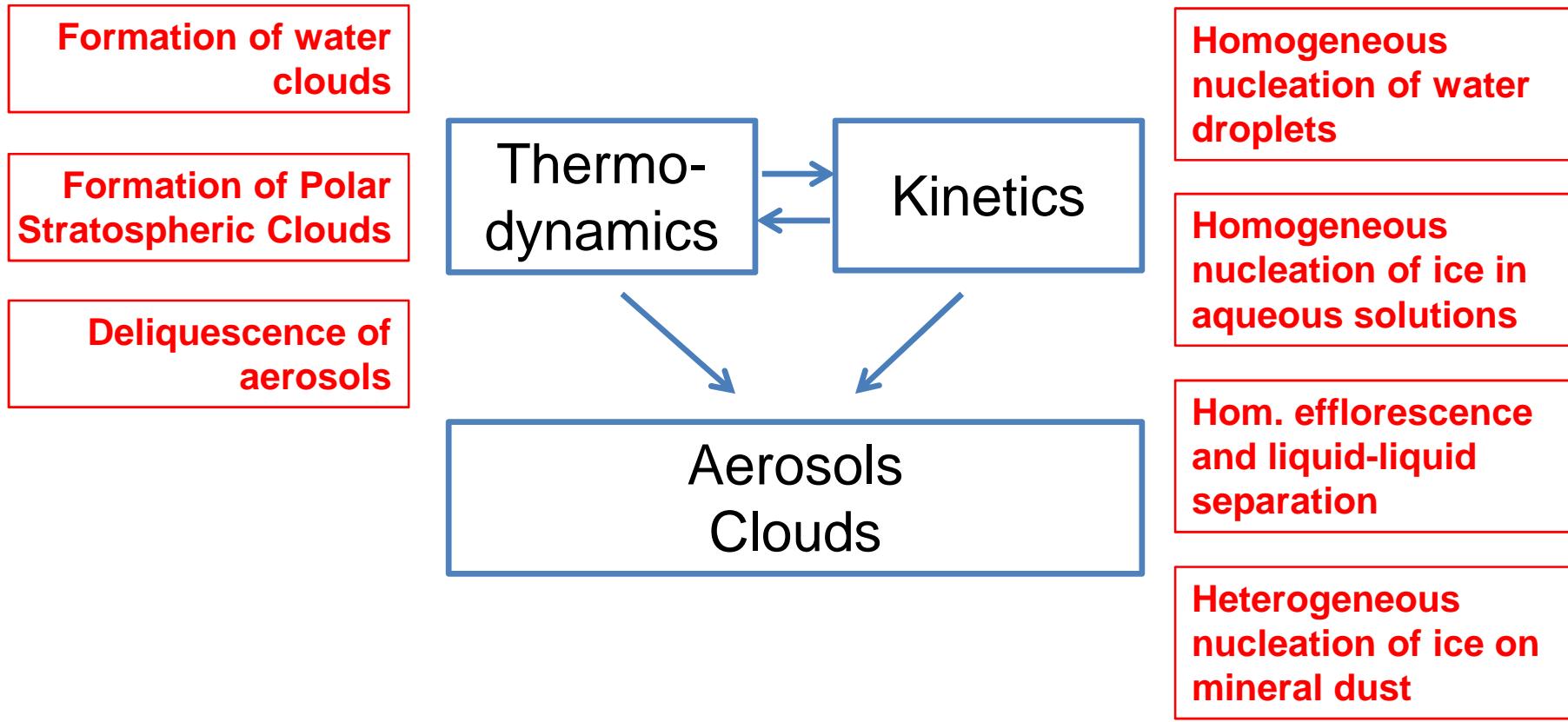


# Results by Cloud Type



# Cloud formation processes





*How far do we get with  
thermodynamics in explaining  
cloud formation?*

*When do we need a kinetic  
treatment?*

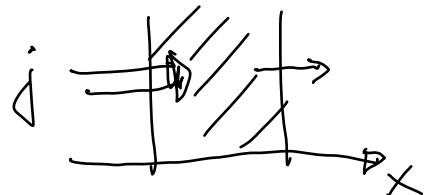
# Diffusion Growth of Flat Surface or Water Droplet

1-D

## (1) Continuity equation

$n = \text{H}_2\text{O}$  molecule number density (in the gas phase)

$j = \text{molecules per area per time} = \text{molecular flux}$



$$\frac{\partial n(x,t)}{\partial t} = - \frac{\partial j(x,t)}{\partial x}$$

3-D

$$\nabla = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right)$$

$$\frac{\partial n}{\partial t} = - \nabla \cdot j$$

## (2) Fick's Law

Diffusive flux of molecules is a result of number density gradients:

(diffusion coefficient  $[D] = \text{cm}^2 \text{ s}^{-1}$ )

$$j = -D \frac{\partial n}{\partial x}$$

$$\vec{j} = -D \nabla n$$

## (3) Diffusion Equation

Combine (1) and (2) :

$$\frac{\partial n}{\partial t} = D \frac{\partial^2 n}{\partial x^2}$$

$$\frac{\partial n}{\partial t} = D \nabla^2 n$$

## The droplet growth problem:

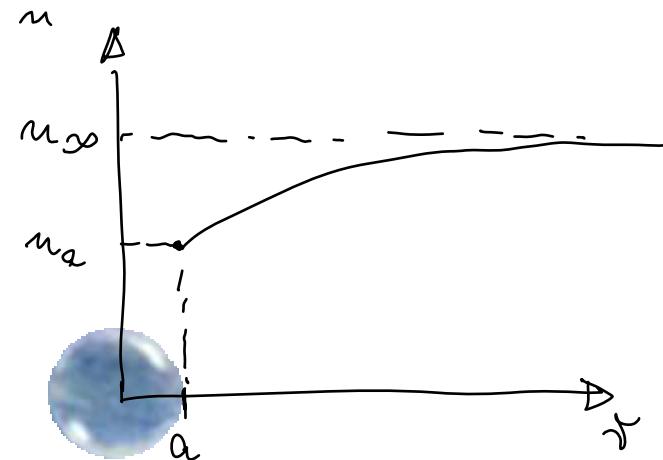
$r$  = radial coordinate

$a$  = droplet radius

$n$  = number density of H<sub>2</sub>O molecules

$n_\infty$  = number density far from droplet

$n_a$  = number density just above  
droplet surface



## Transform from Cartesian coordinates to spherical coordinates:

$$\nabla^2 \psi = \frac{1}{r} \frac{\partial^2}{\partial r^2} (r \psi) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2}$$

(e.g. formulae in Jackson's book on electrodynamics)

*= 0 for spherical symmetry*

The droplet growth problem is in good approximation spherically symmetric. Therefore, the diffusion of H<sub>2</sub>O molecules towards a small water droplet of radius  $a$  can be described by the radial diffusion equation:

$$\frac{\partial n}{\partial t} = D_g \nabla^2 n = D_g \frac{1}{r} \times \frac{\partial^2}{\partial r^2} (r n)$$

where  $D_g$  is the diffusion constant of H<sub>2</sub>O molecules in air.

$$\frac{\partial n}{\partial t} = D_g \nabla^2 n = D_g \frac{1}{r} \times \frac{\partial^2}{\partial r^2} (r n)$$

Task: For stationary conditions ( $\underline{\partial/\partial t = 0}$ ), derive  $n$  from this equation.

Need two boundary conditions:

$$\begin{cases} n(r \rightarrow \infty) = n_{\infty} = \text{const} & \text{far away} \\ n(r \rightarrow a) = n_a = \text{const} & \text{above droplet surface.} \end{cases}$$

$$D = \frac{d^2}{dr^2} (\tau u)$$

$$\tau u = A + B r$$

$$\text{Boundary conditions: } n_{\infty} = B, \quad n_a = \frac{A}{a} + B$$

$$n(r) = (n_a - n_{\infty}) \frac{a}{r} + n_{\infty} \quad \text{and} \quad j(r) = -D_g \frac{\partial n}{\partial r} = D_g (n_a - n_{\infty}) \frac{a}{r^2}$$

## Interpretation:

- $p_\infty = n_\infty kT$  is the H<sub>2</sub>O partial pressure.
- $p_a = n_a kT$  is the H<sub>2</sub>O vapor pressure.
- $(n_a - n_\infty) < 0 \rightarrow$  water uptake
- $(n_a - n_\infty) > 0 \rightarrow$  water loss
- $(n_a - n_\infty) = 0 \rightarrow$  equilibrium

## Droplet growth:

$$\oint \vec{j} \cdot d\vec{S} = \oint \vec{j} \cdot \vec{e}_r dS = -\frac{dN}{dt} = -\frac{1}{V_m} \frac{dV}{dt} = -\frac{1}{V_m} 4\pi a^2 \frac{da}{dt}$$

$S$  = droplet surface area

$N$  = # H<sub>2</sub>O molecules in droplet

$V$  = droplet volume

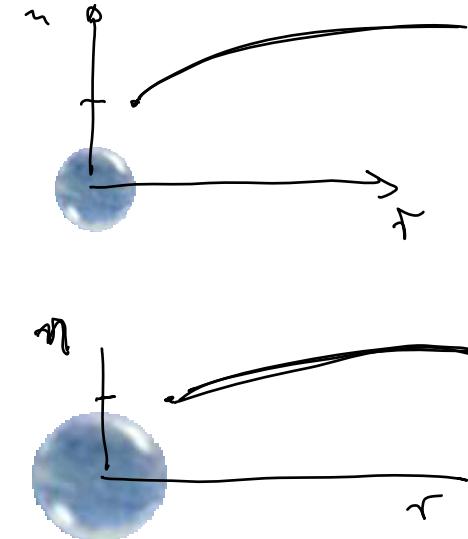
$V_m$  = H<sub>2</sub>O molecular volume

$$\oint \vec{j} \cdot d\vec{S} = \int j dS = 4\pi a^2 j(a) \approx 4\pi a^2 \left[ -D_g \frac{\partial u}{\partial r} \right]_a = 4\pi a D_g (n_a - n_\infty)$$

## Growth/evaporation law for a droplet

$$\Rightarrow \frac{da}{dt} = -V_m \frac{D_g}{a} (n_a - n_\infty)$$

$p_a = n_a kT$  is the H<sub>2</sub>O vapor pressure



***But there is a serious problem with our solution:***

$\Rightarrow$  Violation of flux limitation

This result diverges for  $a \rightarrow 0$ . But this is physical non-sense!

The flux cannot become arbitrarily large but is limited by molecular bombardment.

**Continuum Theory**  
diffusion equation

**Molecular Theory**  
statistical thermodynamics



Boltzmann

In mathematical terms, we need to change our boundary condition:

**Need a flux boundary condition, not a concentration boundary condition!**

Molecular bombardment on surface:

$$j = \frac{1}{4} \bar{v} n$$

( $\bar{v}$  = mean molecular thermal velocity)

$$\Rightarrow j(a) = D_g (n_a - n_\infty) \frac{1}{a} = \frac{\alpha}{4} \bar{v} (n_{vap} - n_a)$$

Hertz-Knudsen Equation

$\bar{v}$  = mean molecular thermal velocity

$\alpha$  = mass accommodation coefficient

→  $1 - \alpha$  is the fraction of colliding molecules that is reflected by surface

From this equation determine  $n_a$ :

$$n_a \left( \frac{D_g}{a} + \frac{\alpha \bar{v}}{4} \right) = \frac{\alpha}{4} \bar{v} n_{vap} - \frac{D_g}{a} n_\infty \Rightarrow n_a = \frac{n_{vap} + \frac{4 D_g n_\infty}{\alpha \bar{v} a}}{1 + \frac{4 D_g}{\alpha \bar{v} a}}$$

$$\frac{da}{dt} = -V_m \frac{D_g}{a} \times \frac{n_{vap} - n_\infty}{1 + (4D_g/\alpha a V)}$$

No divergence!  
Finite growth and evaporation rates!

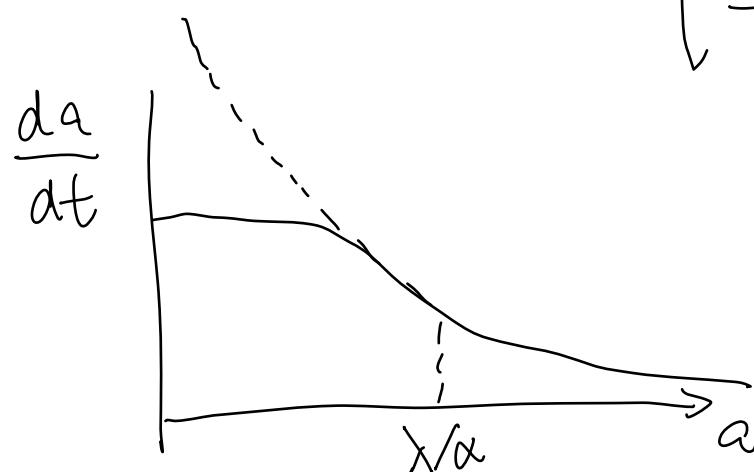
$$D_g = \frac{\bar{V} \lambda}{4}, \quad \lambda = \text{mean free collisional path}$$

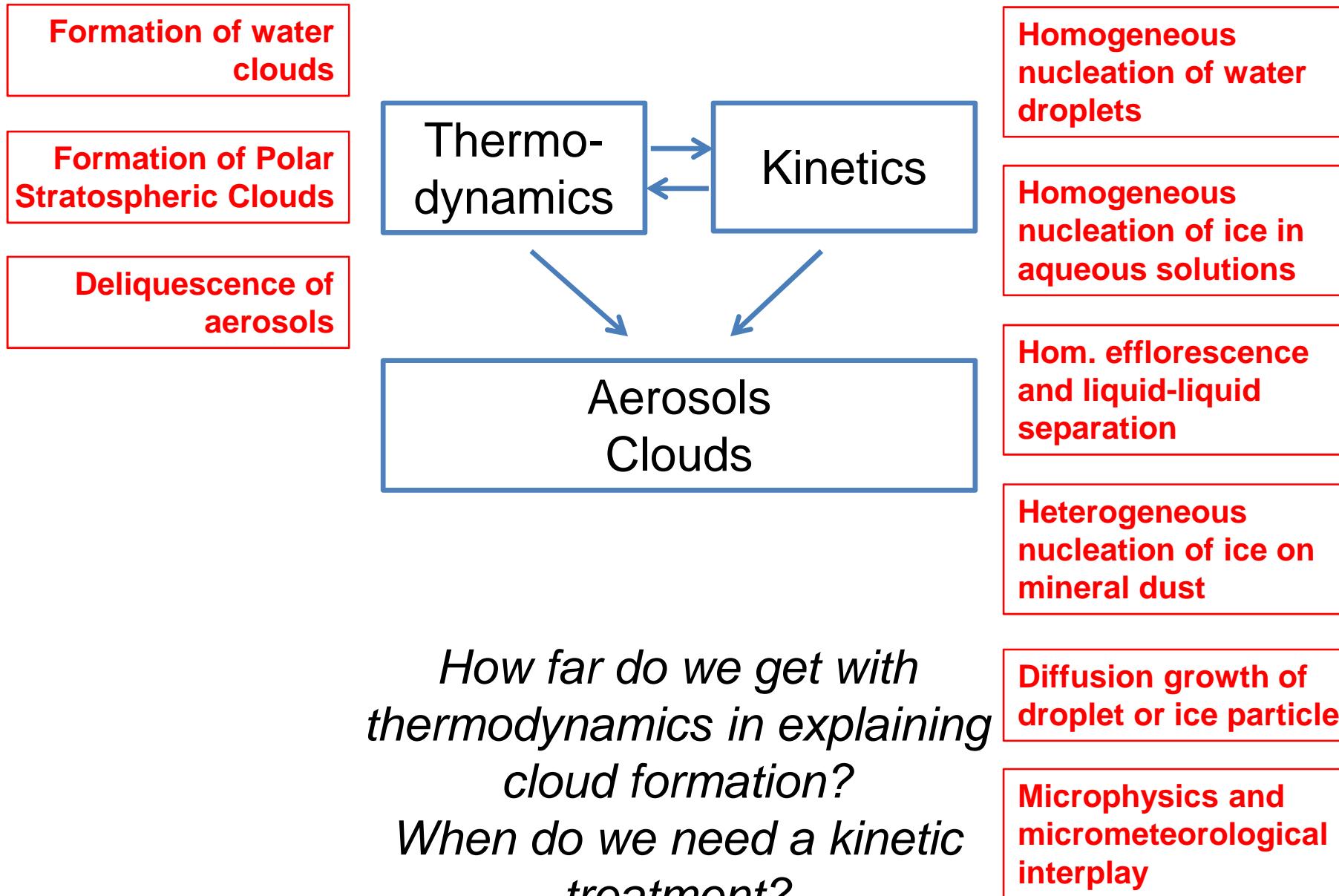
$$\frac{da}{dt} = -V_m \frac{D_g}{a} \times \frac{n_{vap} - n_\infty}{1 + \lambda/\alpha a} =$$

$$\left\{ \begin{array}{l} - \frac{V_m D_g}{a} (n_{vap} - n_\infty), \quad a \gg \lambda/\alpha \\ - V_m \frac{\lambda \bar{V}}{4} (n_{vap} - n_\infty), \quad a \ll \lambda/\alpha \end{array} \right.$$

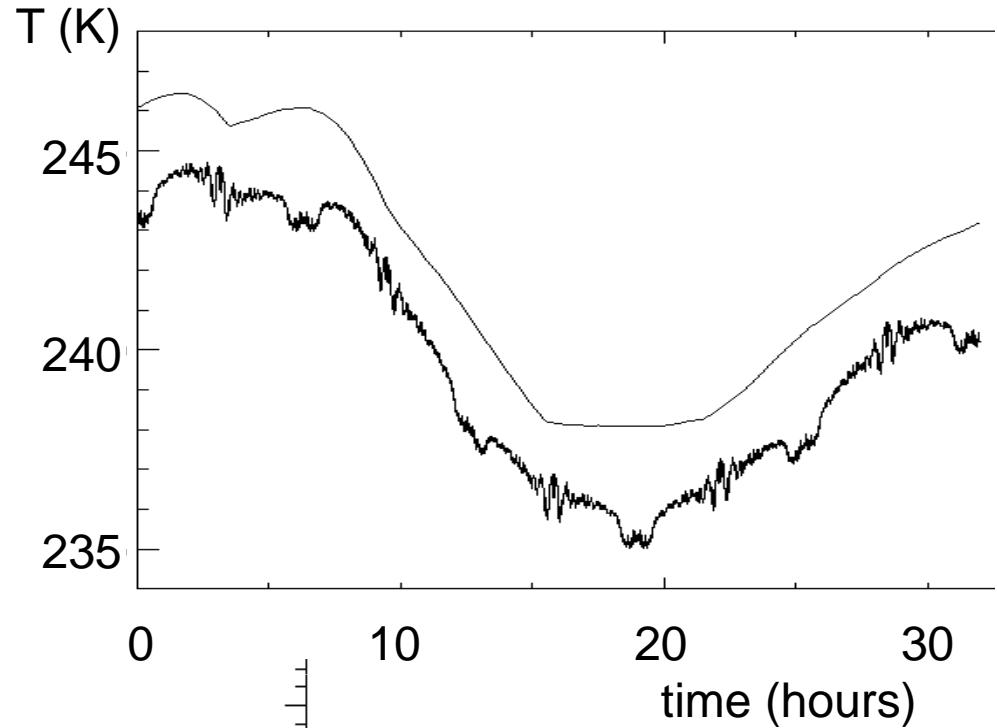
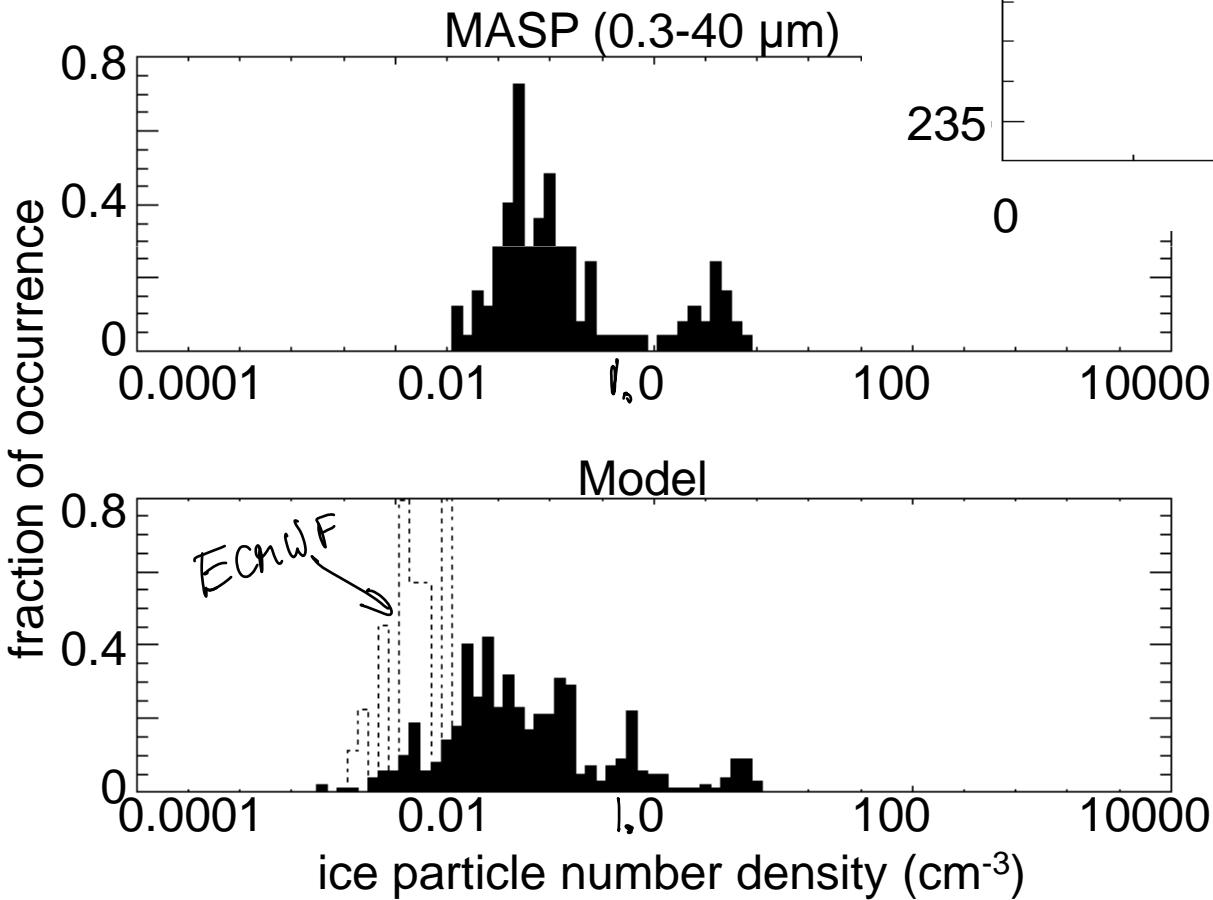
Continuum regime  
 $a \gg \lambda/\alpha$

Knudsen regime  
 $a \ll \lambda/\alpha$





# Importance of meso-scale temperature fluctuations for ice nucleation



SUCCESS  
campaign, cirrus cloud at  
~ 7 km  
altitude

**Formation of water clouds**

**Formation of Polar Stratospheric Clouds**

**Deliquescence of aerosols**

**Thermo-dynamics**

**Kinetics**

**Aerosols  
Clouds**

**Homogeneous nucleation of water droplets**

**Homogeneous nucleation of ice in aqueous solutions**

**Hom. efflorescence and liquid-liquid separation**

**Heterogeneous nucleation of ice on mineral dust**

**Diffusion growth of droplet or ice particle**

**Microphysics and micrometeorological interplay**

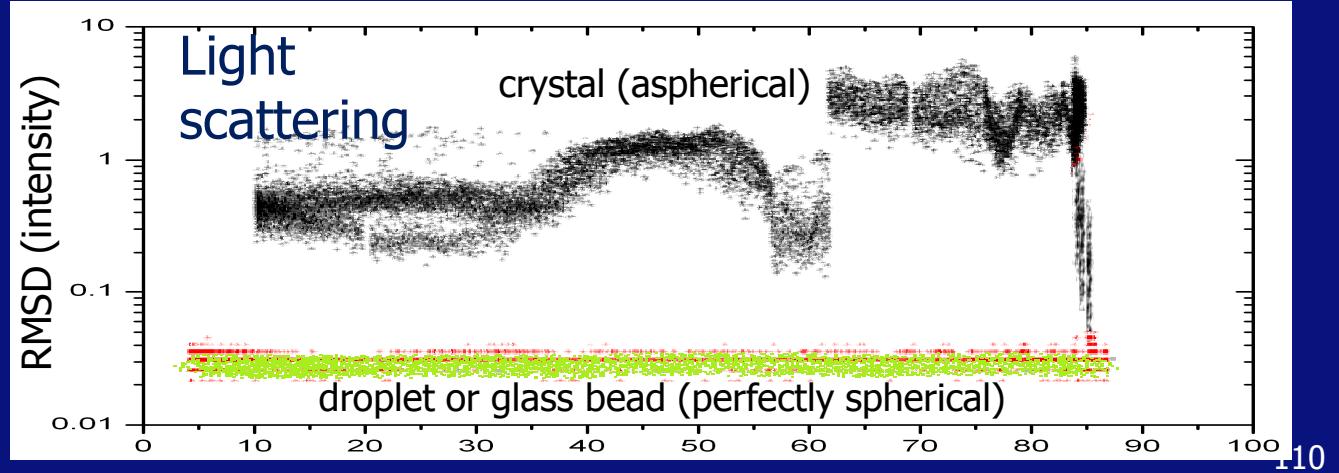
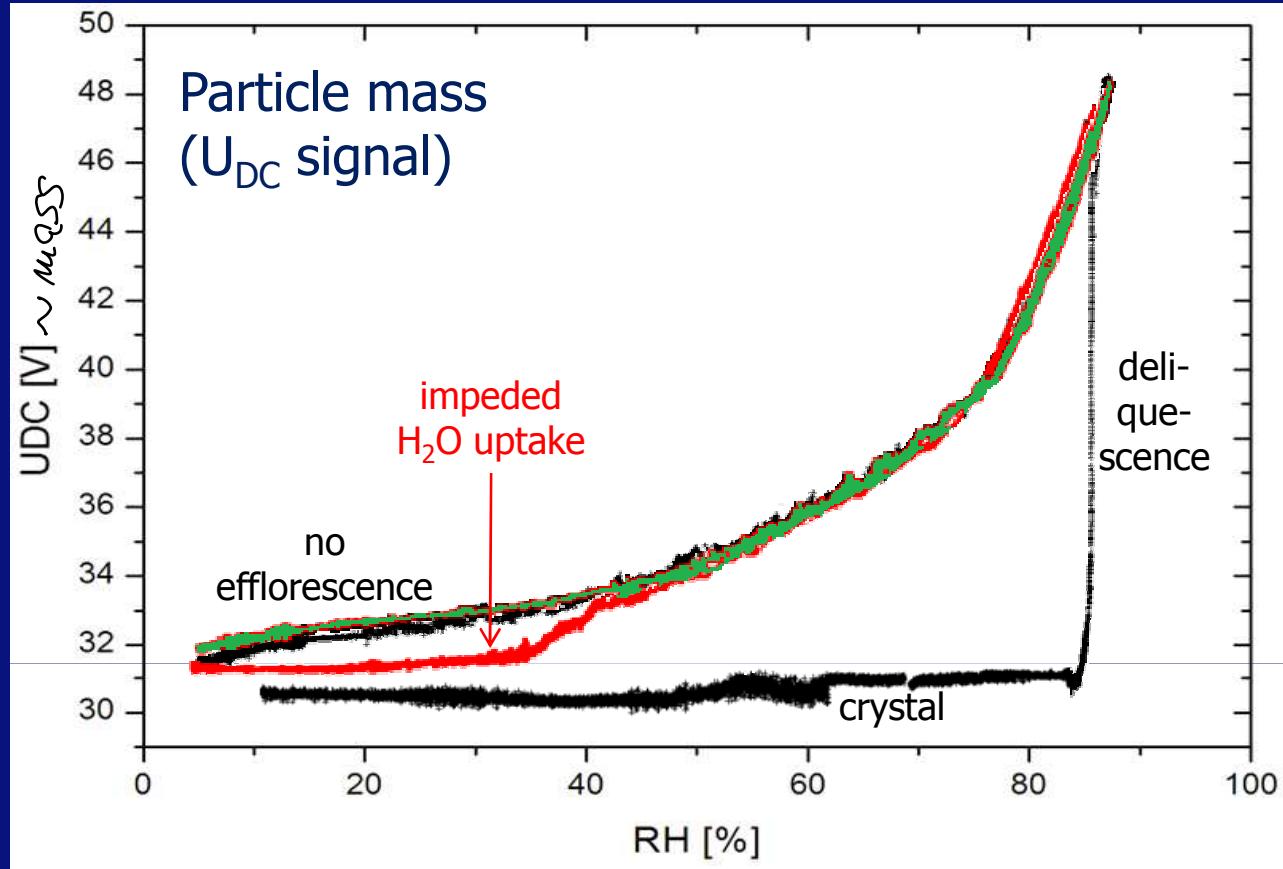
**Glass formation**

*How far do we get with thermodynamics in explaining cloud formation?  
When do we need a kinetic treatment?*

## Example:

$\text{H}_2\text{O}$  uptake  
impedance  
of glassy  
aerosols:  
sucrose  
particle  
at 291 K

(5-day  
experiment,  
each leg  
~ 1 day)



Formation of water clouds

Formation of Polar Stratospheric Clouds

Deliquescence of aerosols

Thermo-dynamics

Kinetics

Aerosols  
Clouds

Combined frost point / backscatter measurements

*How far do we get with thermodynamics in explaining cloud formation?  
When do we need a kinetic treatment?*

Homogeneous nucleation of water droplets

Homogeneous nucleation of ice in aqueous solutions

Hom. efflorescence and liquid-liquid separation

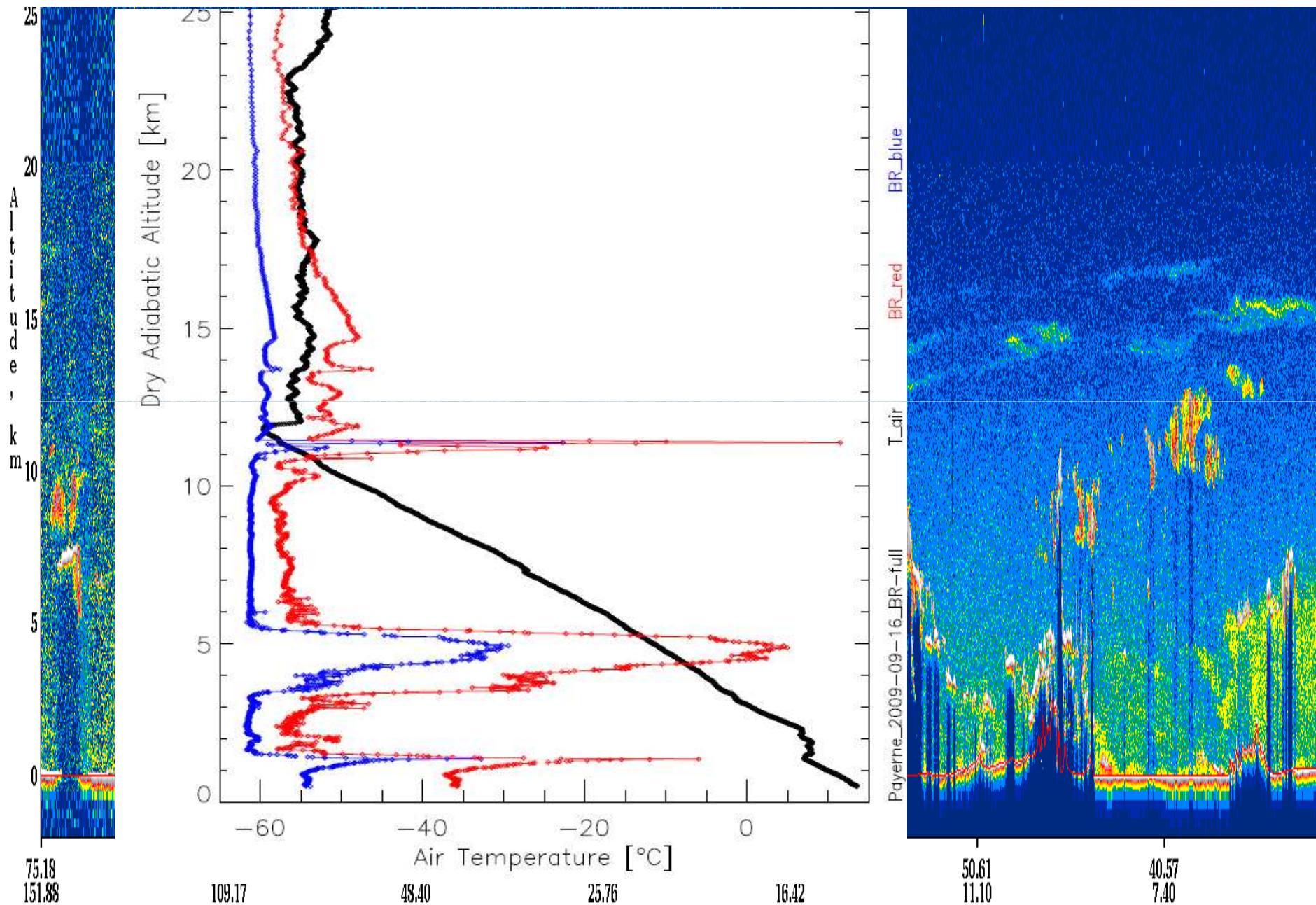
Heterogeneous nucleation of ice on mineral dust

Diffusion growth of droplet or ice particle

Microphysics and micrometeorological interplay

Glass formation

# Low clouds, cirrus and stratospheric aerosol above Zurich, 16 September 2009

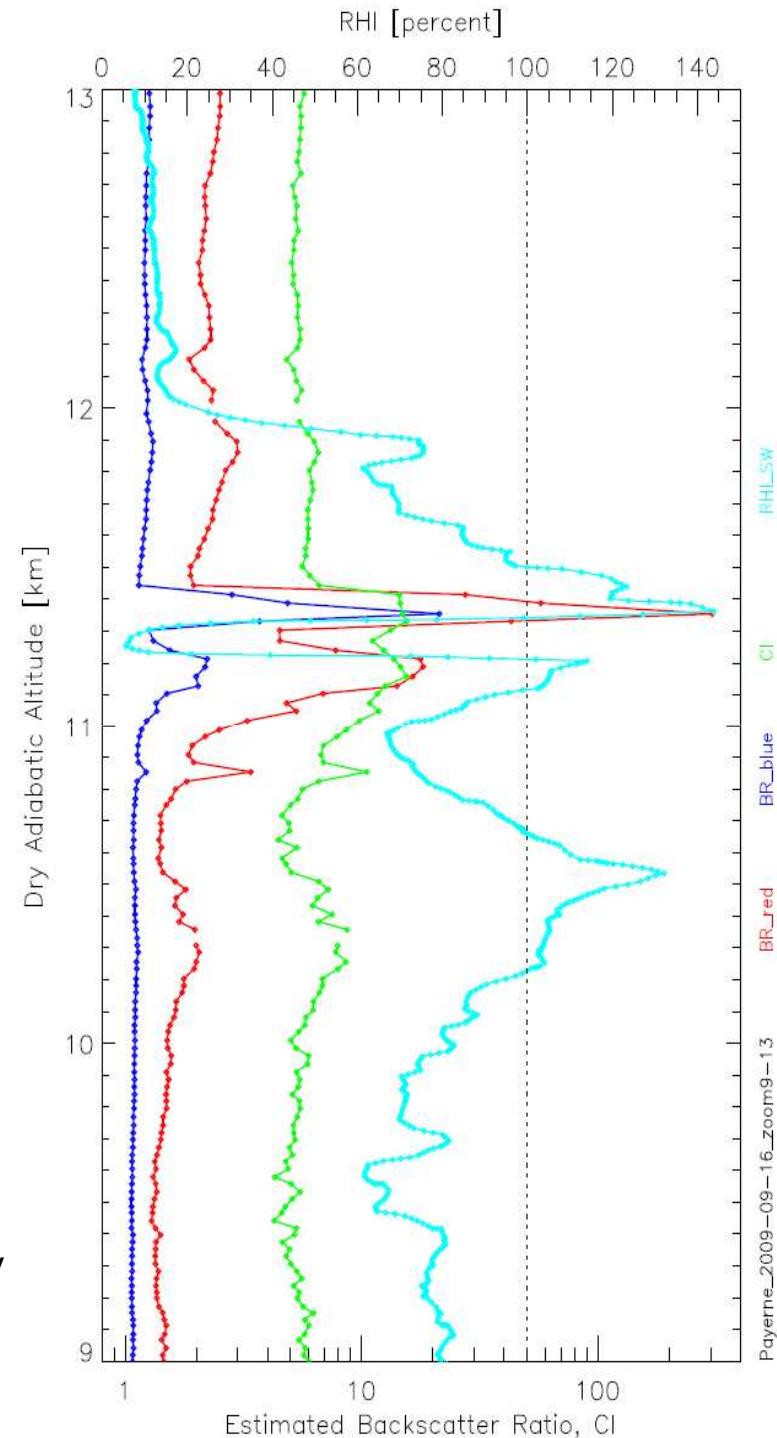


**Highlight:**  
New Instrument development

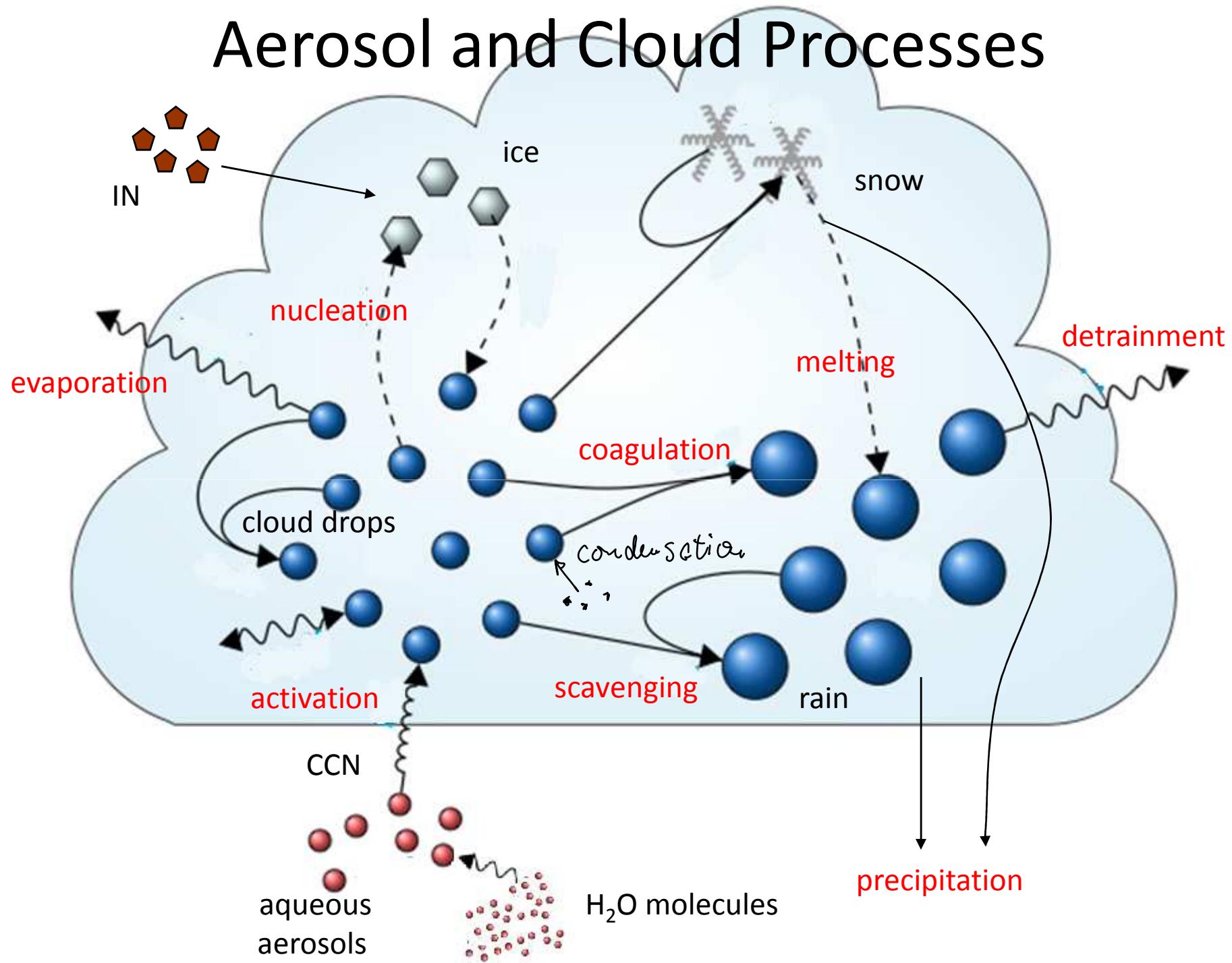
## COBALD Lightweight Backscatter Sonde

Feature	Specification	Remark
wavelengths	455 nm & 870 nm	color index 1-15
Backscatter dynamic range	$10^4$	from unperturbed stratosph. aerosol to thick anvil outflow
time resolution	1 s 0.05-3 s selectable	
dimensions	$17 \times 14 \times 12 \text{ cm}^3$	incl. 3 cm insulation
total weight	540 g	suited for piggyback
power supply	$8 \times \text{LR61}$ (1.5V AA) $2 \times \text{6LR61}$ (9V)	for > 3 h of operation
data interface	19.2 kbit/s, logic level RS232	settings for SRS-C34, adaptable to telemetry
altitude range	ground to > 30 km	cp. weather sondes

More on this: Cirisan et al., future work



# Aerosol and Cloud Processes



Thanks!

## Last slide:

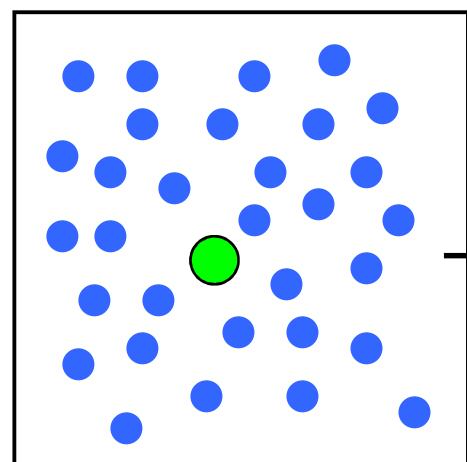
The differential particle size distribution

$$\frac{dn}{d\log r}(\vec{x}, r, t) \equiv r n_r(\vec{x}, r, t)$$

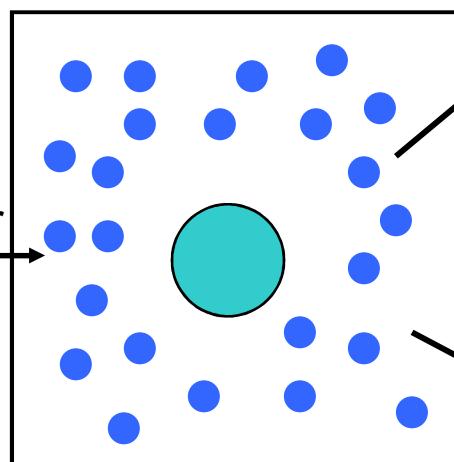
and its corresponding transport equation:

$$\begin{aligned} & \frac{\partial n_r}{\partial t}(\vec{x}, r, t) + \vec{v} \cdot \nabla n_r(\vec{x}, r, t) + v_s \frac{\partial n_r}{\partial z}(\vec{x}, r, t) + \frac{\partial v_r n_r}{\partial r}(\vec{x}, r, t) + D_r \nabla^2 n_r(\vec{x}, r, t) \\ &= J_{nuc}(\vec{x}, r, t) \\ & - \int_0^\infty dr' K(r, r') n_r(\vec{x}, r, t) n_r(\vec{x}, r', t) \\ & + \int_0^r dr' K(r', (r^3 - r'^3)^{1/3}) n_r(\vec{x}, r', t) n_r(\vec{x}, (r^3 - r'^3)^{1/3}, t) \end{aligned}$$

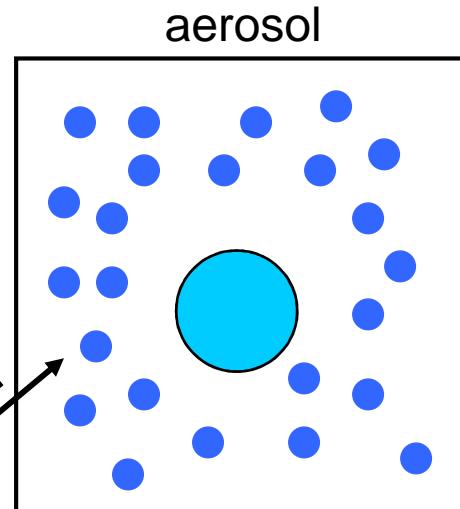
- water molecule
- aerosol particle (e.g.  $\text{NH}_4^+/\text{SO}_4^{2-}/\text{H}_2\text{O}$  solution)
- diluted aerosol particle
- cloud droplet



moister

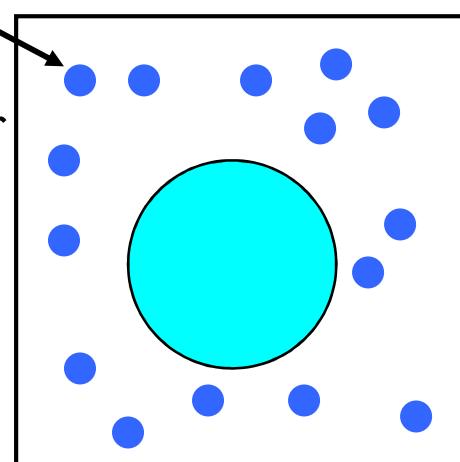


even  
moister



What decides whether the aerosol particle stays an aerosol particle or becomes a cloud droplet?  
→ Köhler Theory

even  
moister

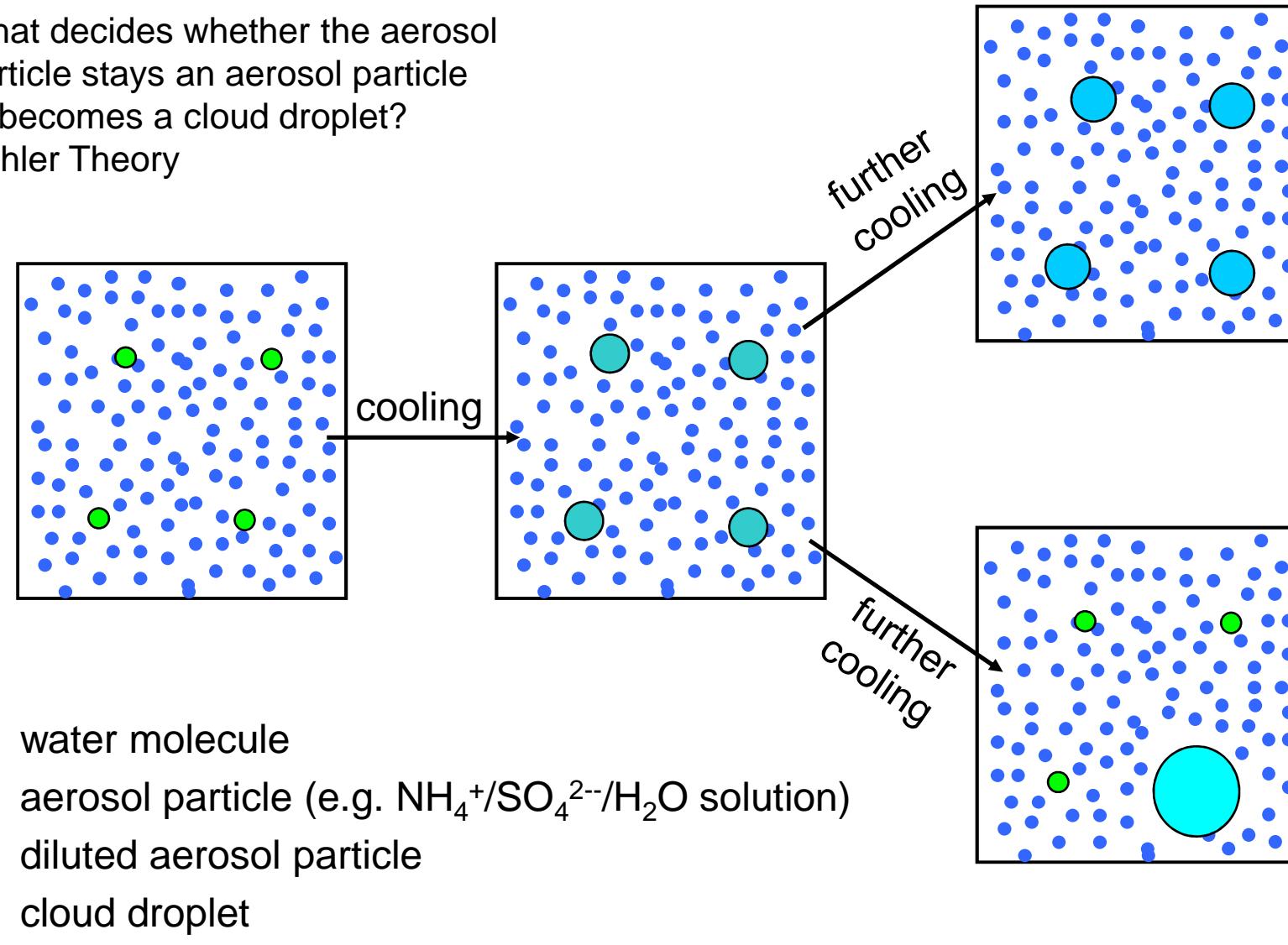


# Cloud droplet formation

A fierce competition without which precipitation would be massively impeded!

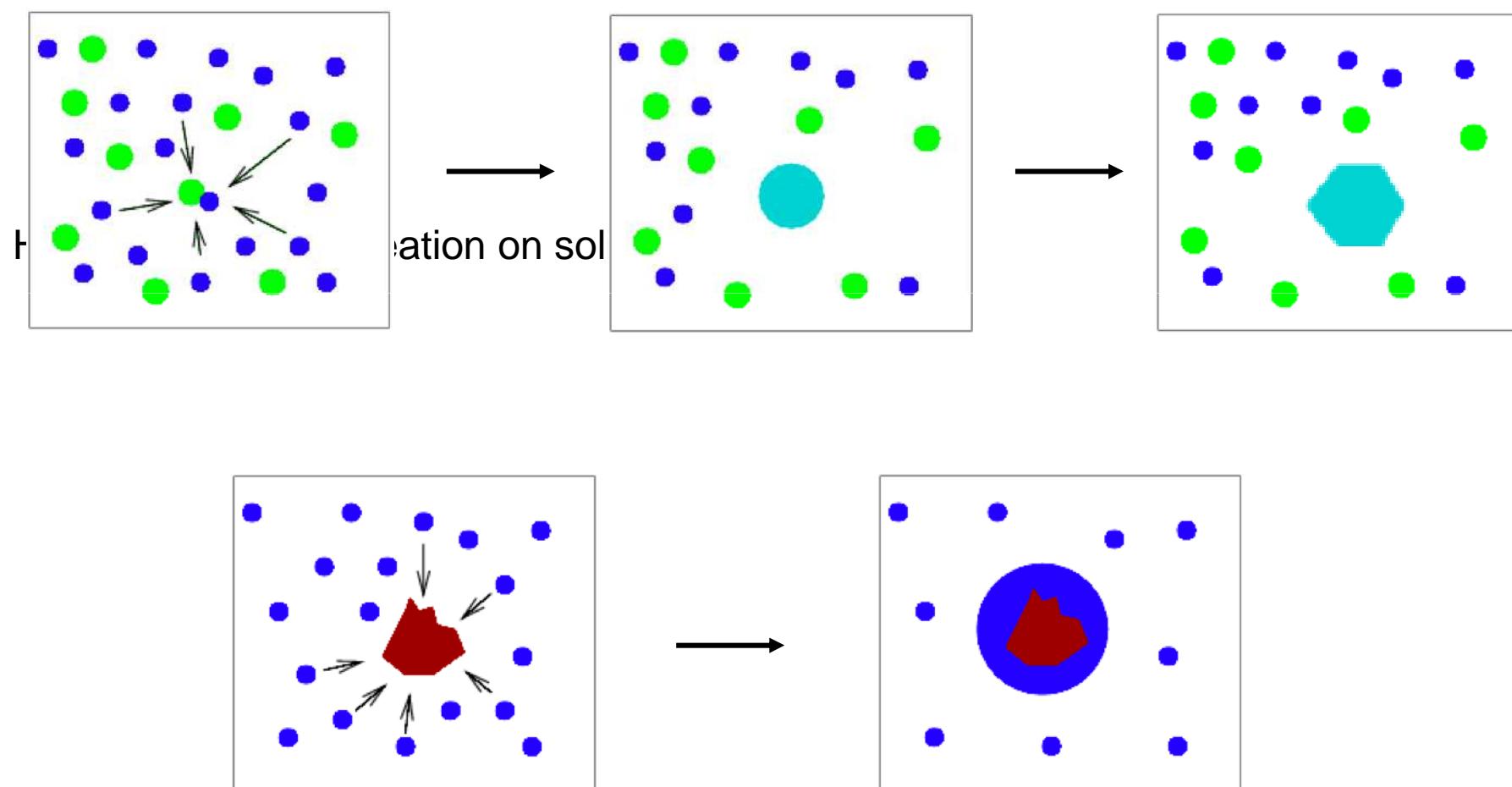
What decides whether the aerosol particle stays an aerosol particle or becomes a cloud droplet?

Köhler Theory

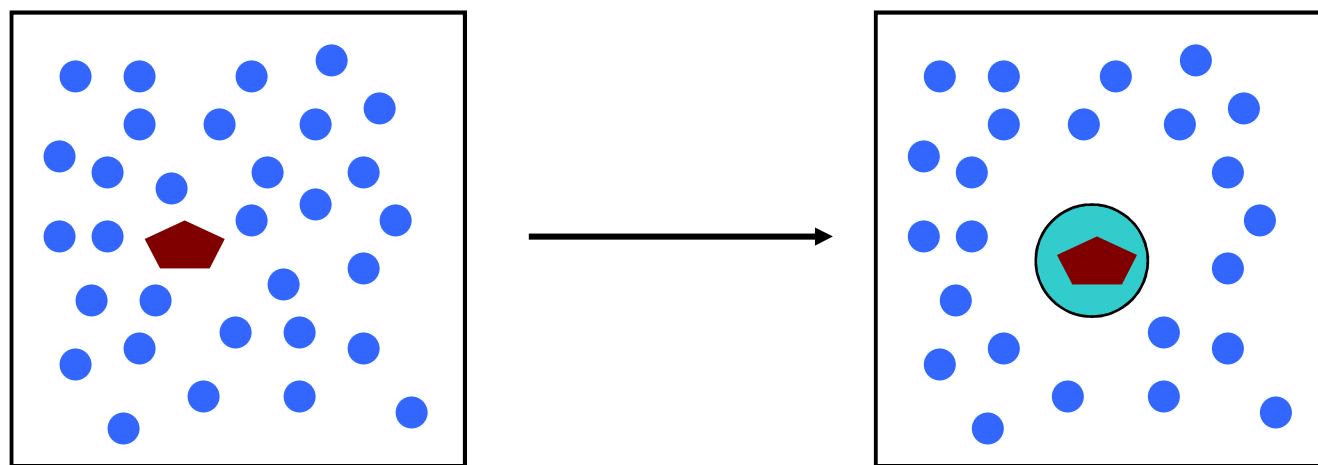


Different pathways for ice nucleation, e.g.:

Homogeneous nucleation of solution droplets



Cloud condensation nuclei  
insoluble aerosol



Depending on surface, composition,  
temperature, relative humidity ...

Hier Colberg

Hoyle paper

Do we need a kinetic  
treatment for H<sub>2</sub>O transport  
in strat?

Raoult lived when?

Snowwhite / Cobald